

#### WHP Cruise Summary Information

WOCE section designation	SR03
Expedition designation (EXPOCODE)	09AR9501_1; 09AR9604_1 ; 09AR9601_1
Chief Scientist(s) and their affiliation	Nathan Bindoff, Antarctic CRC (9501)
	Nathan Bindoff, Antarctic CRC (9604)
	Stephen Rintoul, CSIRO (9601)
Dates	1995.07.17 - 1995.09.02 (9501)
	1996.01.19 - 1996.03.31 (9604)
	1996.08.22 - 1996.09.22 (9601)
Ship	
Ports of call	Davis; Casey; Macquarie Island (9604)
	Macquarie Island (9601)
Number of stations	208 (9501); 147 (9604); 71 (9601)
Geographic boundaries of the stations	43°59.86 S
09AR9501_1	139°44.93 E 146°20.32 E
	65°30.64 S
	44°00.01 S
09AR9601_1	139°49.38 E 152°18.29 E
	65°44.59 S
004 50004 4	44°7.02 S
09AR9604_1	76°1.96 E 150°1.03 E
	68°8.43 S
Floats and drifters deployed	8 deployed (9604)
Moorings deployed or recovered	1 recovered (9604)
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## COOPERATIVE RESEARCH CENTRE FOR THE ANTARCTIC AND SOUTHERN OCEAN ENVIRONMENT (ANTARCTIC CRC)

Aurora Australis Marine Science Cruises AU9501, AU9604 and AU9601 - Oceanographic Field Measurements and Analysis, Inter-cruise Comparisons and Data Quality Notes

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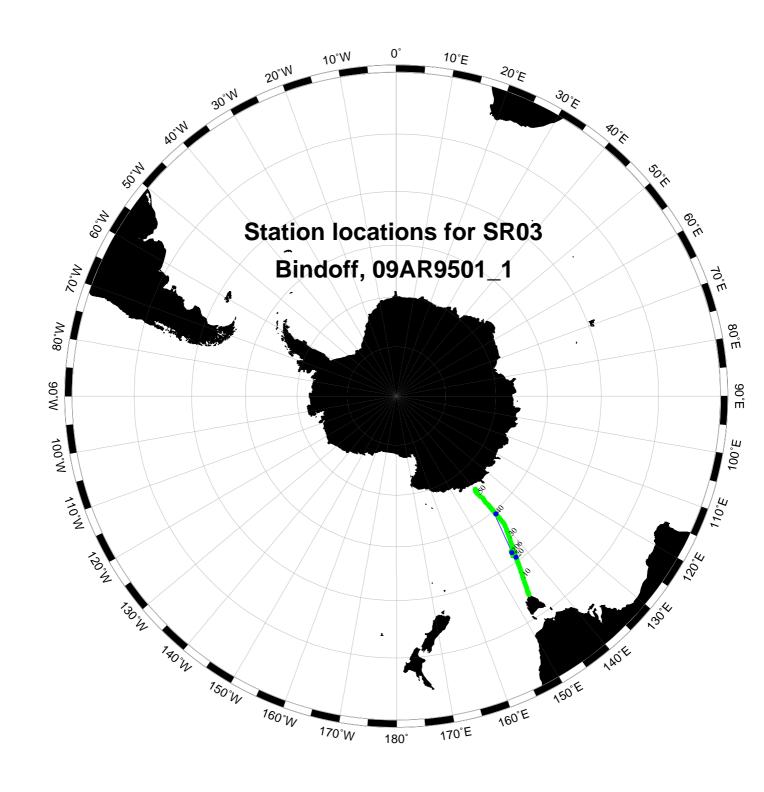
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### Part 1 Aurora Australis Marine Science Cruise AU9501 - Oceanographic Field Measurements and Analysis

#### **ABSTRACT**

Oceanographic measurements were conducted along WOCE Southern Ocean meridional section SR3 between Tasmania and Antarctica, and around the boundary of a square-plan test volume south of the Antarctic Divergence, from July to September 1995. A total of 208 CTD vertical profile stations were taken, 64 of those to near bottom, and the remaining 144 to a depth of 500 m. Over 2300 Niskin bottle water samples were collected for the measurement of salinity, dissolved oxygen, nutrients, dissolved organic and inorganic carbon, iodate/iodide, primary productivity, and biological parameters, using both a 24 and 12 bottle rosette sampler. Near surface current data were collected using a ship mounted ADCP. Measurement and data processing techniques are summarised, and a summary of the data is presented in graphical and tabular form.

#### 1.1 INTRODUCTION

Marine science cruise AU9501, the fourth oceanographic cruise of the Cooperative Research Centre for the Antarctic and Southern Ocean Environment (Antarctic CRC), was conducted aboard the Australian Antarctic Division vessel RSV Aurora Australis from July to September 1995. The first major constituent of the cruise was the collection of oceanographic data relevant to the Australian Southern Ocean WOCE Hydrographic Program, along WOCE section SR3 (Figure 1.1a). The primary scientific objectives of this program are summarised in Rosenberg et al. (1995a). This was the sixth occupation of section SR3, and the first during a southern winter. Previous occupations of SR3 by the Aurora Australis were in the spring of 1991 (Rintoul and Bullister, submitted), in the autumn of 1993 (Rosenberg et al., 1995a), and in the summers of 1993/94 and 1994/95 (Rosenberg et al., 1995b and 1996). The northern half of the SR3 section was occupied by the SCRIPPS ship R.V. Melville in the autumn of 1994 (principal investigators R.Watts, S. Rintoul, J. Richman, B. Petit, D. Luther, J. Filloux, J. Church, A. Chave).

The second major constituent of the cruise was the dual oceanographic and sea ice experiments FORMEX (Formation Experiment: water mass formation near the Antarctic Continental slope) and HIHO-HIHO (Harmonious Ice and Hydrographic Observations - Halide In, Heat Out: sea ice formation processes; Worby et al., 1996). The primary objectives of FORMEX are:

- 1. to obtain quantitative estimates of the rate of formation of Antarctic surface waters in the ice pack during winter;
- 2. to obtain quantitative estimates of the transfer of heat between the ocean and atmosphere and the role of advection of surface and circumpolar deep water on these transfers;
- 3. to investigate processes and mechanisms involved in the mixing of Polar Zone waters with "Complex Zone" waters near the Antarctic shelf.

FORMEX CTD measurements were collected to a depth of 500 m every 5 nautical miles around the perimeter of a closed 60x60 nautical mile area within the pack ice (Figure 1.1b). The closed volume was sampled clockwise 3 times over a 21 day period, with 48 CTD/ADCP profile stations sampled on each of the 3 completed circuits.

This report describes the collection of oceanographic data from the SR3 transect and FORMEX, and summarises the chemical analysis and data processing methods employed. All information required for use of the data set is presented in tabular and graphical form.

#### 1.2 CRUISE ITINERARY

The cruise commenced with a north to south traverse of section SR3, with a typical station spacing of 30 nautical miles. Station spacing between 49.5°S and 52°S was decreased to less than 20 nautical miles (Table 1.2) to include CTD casts over current meter and inverted echo sounder moorings (Table 1.4), thereby increasing meridional resolution in the vicinity of the Subantarctic Front. The mooring array had been deployed in the autumn of 1995 by the R.V. Melville (principal investigators R.Watts, S. Rintoul, J. Richman, B. Petit, D. Luther, J. Filloux, J. Church, A. Chave). South of ~55°S, periods of very calm conditions were encountered, with winds close to zero and the ocean surface glassy. ADCP measurements from this period will be useful for an examination of ADCP data in the absence of noise created by rolling and pitching of the ship. CTD data from this period will allow closer examination of CTD data quality in the absence of pressure reversals caused by a heaving vessel. The section was interrupted at ~65.1°S, due to thick sea ice and rising northerly winds.

The first lap around the FORMEX area was commenced 3 days after the interruption of the SR3 transect, and took 4 days to complete. The ship then travelled south as far as ~65.5°S, with further progress prevented by sea ice conditions. The SR3 section was recommenced at the southernmost latitude, and 3 stations were completed from south to north (Table 1.2). Note that the southermost station was over the continental slope, in a water depth of 1761 m.

Back at the FORMEX site, 2 test casts were taken inside the FORMEX area, both to trial a protective cover against cold air for the CTD sensors, and to investigate sensor performance on CTD serial 1193. FORMEX lap 2 then commenced, 6 days after the completion of lap 1, and taking 4.5 days to complete. Lap 3 commenced 1.5 days after the completion of lap 2, and took 3.5 days to complete. The time before and after each FORMEX lap was dedicated to sea ice experiments.

The ship then returned to the SR3 section, and CTD measurements at stations 44, 43 and 42 were repeated, owing to conductivity sensor malfunction during the earlier occupation. Before returning to Hobart, a further 4 stations were completed over inverted echo sounder moorings along the SR3 transect in the vicinity of the Subantarctic Front (Table 1.4). No measurements could be taken at the remaining 3 inverted echo sounder locations (mooring numbers I3, I5 and I7) due to rough weather conditions encountered on the northward leg.

#### **Table 1.1:** Summary of cruise itinerary.

Expedition Designation
Cruise AU9501 (cruise acronym ABSTAIN), encompassing WOCE section SR3, and FORMEX

Chief Scientists
Nathan Bindoff, Antarctic CRC
Ian Allison, Antarctic Division

*Ship* RSV Aurora Australis

Ports of Call

Cruise Dates
July 17 to September 2 1995

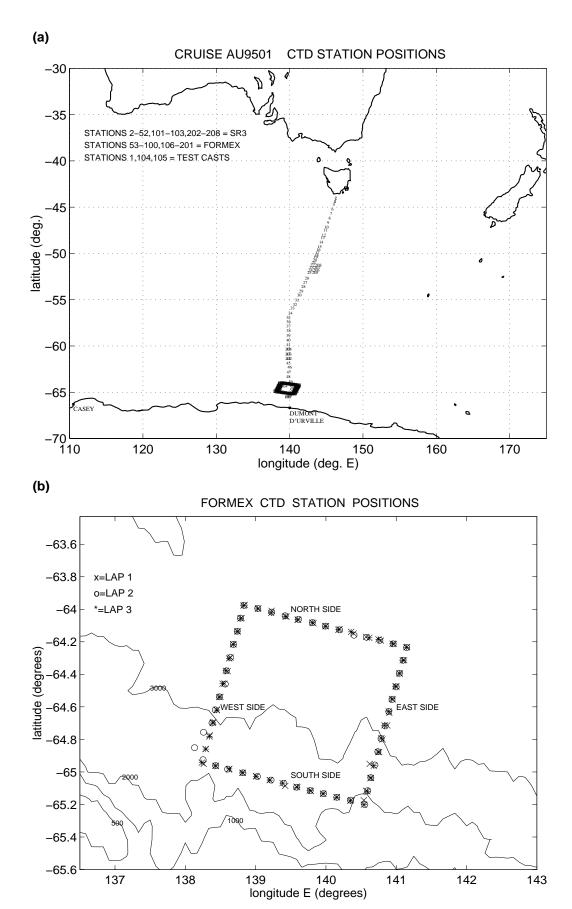


Figure 1.1a and b: CTD station positions for RSV Aurora Australis cruise AU9501 along WOCE transect SR3, and around FORMEX area.

#### 1.3 CRUISE SUMMARY

#### 1.3.1 CTD casts and water samples

In the course of the cruise, 61 CTD casts were completed along the SR3 section (Figure 1.1a), with most casts reaching to within 17 m of the sea floor (Table 1.2); 144 CTD casts to a depth of 500 m were completed on the 3 FORMEX laps; and 3 additional full depth test casts were completed at various locations. Over 2300 Niskin bottle water samples were collected for the measurement of salinity, dissolved oxygen, nutrients (orthophosphate, nitrate plus nitrite, and reactive silicate), dissolved organic and inorganic carbon, iodate/iodide, primary productivity, and biological parameters, using a 24 bottle rosette sampler for the SR3 section, and a 12 bottle system (with 6 bottles mounted) for FORMEX. Table 1.3 provides a summary of samples drawn at each station. Principal investigators for the various water sampling programmes are listed in Table 1.5a. For all stations, the different samples were drawn in a fixed sequence (see Rosenberg et al., 1996, for more details, including descriptions of methods for drawing samples).

#### 1.3.2 Principal investigators

The principal investigators for the CTD and water sample measurements are listed in Table 1.5a. Cruise participants are listed in Table 1.5b.

Table 1.2 (following 6 pages): Summary of station information for RSV Aurora Australis cruise AU9501. The information shown includes time, date, position and ocean depth for the start of the cast, at the bottom of the cast, and for the end of the cast. The maximum pressure reached for each cast, and the altimeter reading at the bottom of each SR3 cast (i.e. elevation above the sea bed) are also included. Missing ocean depth values are due to noise from the ship's bow thrusters interfering with the echo sounder. For casts which do not reach to within 100 m of the bed (i.e. the altimeter range), or for which the altimeter was not functioning, there is no altimeter value. For station names, TEST is a test cast, and Fx.y is cast number y on FORMEX lap x (Figure 1.1b). Note that all times are UTC (i.e. GMT). CTD unit 7 (serial no. 1103) was used for stations 1 to 29, 45 to 103, and 106 to 208; CTD unit 5 (serial no. 1193) was used for stations 30 to 44, and 104 to 105.

station			STAR	T	maxP		BOT	ТОМ				EN	D	
number	time	date	latitude	longitude depth(m)	(dbar)	time	latitude	longitude	depth(m	) altimeter	time	latitude	longitude	depth(m)
1 TEST	2227 1	7-JUL-95	44:22.85S	146:10.75E 2387	2306	2345	44:22.66S	146:11.34E	2392	58.4	0046	44:22.50S	146:11.50E	2393
2 SR3	0315 1	8-JUL-95	43:59.86S	146:19.20E 240	174	0330	43:59.88S	146:19.62E	-	14.0	0358	43:59.97S	146:20.32E	210
3 SR3	0538 1	8-JUL-95	44:07.38S	146:13.72E 1076	1106	0612	44:07.59S	146:14.85E	-	16.0	0658	44:07.59S	146:15.67E	-
4 SR3	1000 1	8-JUL-95	44:22.72S	146:10.59E 2407	2348	1103	44:22.65S	146:10.77E	-	15.6	1224	44:22.62S	146:10.90E	-
5 SR3	1610 1	8-JUL-95	44:43.18S	146:02.80E 3225	3230	1736	44:43.24S	146:03.31E	3225	17.6	1916	44:43.30S	146:03.67E	3123
6 SR3	0020 1	9-JUL-95	45:12.82S	145:51.22E 2866	2890	0155	45:12.72S	145:51.11E	-	18.0	0317	45:12.66S	145:52.36E	2764
7 SR3	1729 1	9-JUL-95	45:41.88S	145:39.45E 2017	2056	1838	45:41.88S	145:38.57E	2068	17.6	2005	45:41.66S	145:37.75E	2068
8 SR3	0027 2	0-JUL-95	46:10.36S	145:27.57E 2744	2748	0148	46:10.18S	145:27.58E	2740	18.1	0311	46:09.89S	145:27.63E	2764
9 SR3	0710 2	0-JUL-95	46:39.14S	145:15.03E 3348	3392	0835	46:38.93S	145:14.68E	-	16.8	1019	46:38.40S	145:14.63E	3368
10 SR3	1413 2	0-JUL-95	47:08.72S	145:03.10E 3593	3910	1545	47:08.28S	145:04.02E	-	15.1	1721	47:07.67S	145:04.28E	-
11 SR3	2001 2	0-JUL-95	47:28.20S	144:54.33E 4300	4344	2145	47:27.01S	144:55.48E	-	17.9	2336	47:26.85S	144:56.04E	4068
12 SR3	0318 2	1-JUL-95	47:59.90S	144:40.57E 4064	4144	0458	47:59.08S	144:40.79E	-	5.0	0633	47:58.53S	144:40.99E	-
13 SR3	0852 2	1-JUL-95	48:19.03S	144:31.56E 4003	4170	1040	48:18.35S	144:31.13E	-	15.0	1242	48:18.12S	144:31.58E	3936
14 SR3	1525 2	1-JUL-95	48:46.60S	144:18.95E 4177	4134	1706	48:45.73S	144:19.15E	-	16.5	1850	48:44.91S	144:19.14E	4045
15 SR3	2152 2	1-JUL-95	49:16.19S	144:05.63E 4218	4254	2341	49:15.28S	144:05.86E	4350	11.1	0133	49:14.49S	144:06.13E	-
16 SR3	0338 2	2-JUL-95	49:36.61S	143:56.13E 3686	3836	0518	49:35.98S	143:57.07E	-	-	0659	49:35.37S	143:57.97E	-
17 SR3	0849 2	2-JUL-95	49:53.24S	143:48.21E 3788	3864	1037	49:52.30S	143:49.92E	-	16.0	1215	49:52.06S	143:50.73E	-
18 SR3	1414 2	2-JUL-95	50:09.62S	143:40.72E 3711	3818	1555	50:09.45S	143:41.91E	-	17.3			143:42.88E	
19 SR3	1908 2	2-JUL-95	50:23.92S	143:33.66E 3583	3656	2056	50:24.03S	143:35.08E	-	16.7	2241	50:23.60S	143:36.13E	3573
20 SR3				143:26.96E 3655	3556			143:27.26E		19.9			143:27.22E	
21 SR3				143:17.77E 3808	3880			143:17.62E		19.8			143:17.39E	
22 SR3				143:07.69E 3706	3876			143:08.06E		15.0			143:08.68E	
23 SR3				142:59.21E 3778	3788			143:00.10E		17.0			143:00.77E	
24 SR3				142:50.80E 3757	3674			142:52.80E		17.4			142:53.60E	
25 SR3				142:42.01E 3512	3514			142:44.15E		19.5	-		142:45.42E	
26 SR3				142:22.85E 3348	3470			142:23.97E		12.0			142:24.57E	
27 SR3				142:08.25E 3133	3134	-		142:08.16E		15.0			142:07.92E	
28 SR3				141:51.81E 2508	2508			141:52.23E		13.0			141:52.65E	
29 SR3				141:35.63E 2662	2656			141:35.57E		15.6			141:35.70E	
30 SR3	0620 2	25-JUL-95	54:31.72S	141:19.42E 2815	2844	0730	54:31.48S	141:19.86E	-	12.0	0843	54:31.12S	141:19.75E	-
31 SR3				141:00.79E 3348	3300			141:00.34E		15.2			141:00.74E	
32 SR3				140:43.48E 3993	4140	_		140:43.15E		15.0			140:43.08E	
33 SR3				140:23.88E 3583	3638	0440	55:55.57S	140:24.37E	-	15.5			140:25.04E	
34 SR3				140:06.09E 3890	4162			140:06.07E		15.0			140:05.98E	
35 SR3				139:50.88E 4075	4180			139:51.85E		14.3			139:52.18E	-
36 SR3	0024 2	7-JUL-95	57:22.25S	139:51.04E 4075	4058	0212	57:22.17S	139:49.72E	-	11.4	0404	57:22.58S	139:48.79E	-

station			STAR	T.	maxP		ВОТ	TOM				EN	1D	
number	time	date	latitude	longitude depth(m)	(dbar)	time	latitude	longitude	depth(m	n) altimeter	time	latitude	longitude	depth(m)
37 SR3	0650 2	7-JUL-95	57:51.42S	139:51.42E 4095	4182	0831	57:51.31S	139:51.89E	-	15.0	1000	57:51.398	139:52.72E	-
38 SR3	1524 2	7-JUL-95	58:20.62S	139:51.08E 3993	4044	1703	58:20.59S	139:51.57E	-	12.8	1846	58:20.965	139:51.62E	3993
39 SR3	2236 2	7-JUL-95	58:51.45S	139:50.49E 3942	4046	0031	58:51.76S	139:50.71E	-	15.9	0215	58:51.728	139:50.53E	-
40 SR3	0539 2	8-JUL-95	59:21.04S	139:50.89E 4218	4220	0720	59:21.33S	139:51.23E	-	15.8	0850	59:21.648	139:51.76E	-
41 SR3	1428 2	8-JUL-95	59:51.30S	139:50.94E 4587	4540	1632	59:50.248	139:51.31E	-	13.8	1829	59:49.578	139:52.13E	4587
42 SR3	2320 2	8-JUL-95	60:21.27S	139:50.24E 4443	4506	0128	60:21.548	139:49.95E	4443	9.9	0328	60:21.875	139:49.61E	-
43 SR3	0611 2	9-JUL-95	60:51.27S	139:50.17E 4402	4466	0747	60:51.80S	139:49.52E	-	11.3	0928	60:52.308	139:49.72E	-
44 SR3	1431 2	9-JUL-95	61:21.06S	139:51.01E 4351	4410	1649	61:22.098	139:50.41E	4351	13.6	1847	61:22.398	139:50.64E	4351
45 SR3	2326 2	9-JUL-95	61:50.05S	139:51.60E 4300	3348	0125	61:49.87S	139:54.95E	4300	-	0255	61:50.585	139:57.90E	-
46 SR3	0622 3	0-JUL-95	62:15.68S	140:00.46E 4054	4082	0758	62:15.84\$	140:01.21E	4054	16.4	0936	62:16.325	140:02.14E	-
47 SR3	1424 3	0-JUL-95	62:49.70S	139:53.68E 3235	3262	1601	62:50.56S	139:54.91E	3275	13.5	1728	62:51.638	139:55.29E	3255
48 SR3	2112 3	0-JUL-95	63:17.16S	139:50.37E 3819	3830	2241	63:18.37S	139:49.53E	3819	25.5	0036	63:20.658	139:47.19E	3819
49 SR3	0450 3	1-JUL-95	63:49.89S	140:07.79E 3716	3746	0625	63:49.72S	140:11.10E	3716	16.0	0751	63:49.805	140:14.37E	3716
50 SR3	1733 3	1-JUL-95	64:26.58S	140:20.49E 3481	3476	1908	64:26.59S	140:20.04E	3471	13.7	2027	64:26.468	140:19.64E	3471
51 SR3	0318 1	1-AUG-95	64:46.74S	140:20.35E 3327	3274	0441	64:47.33S	140:18.40E	-	16.2	0614	64:48.178	140:16.84E	-
52 SR3	1046 1	1-AUG-95	65:07.28S	140:19.45E 2583	2582	1201	65:07.55S	140:18.91E	-	14.9	1321	65:07.968	140:18.24E	2563
53 F1.1	1706 4	4-AUG-95	64:57.01S	140:37.39E 2701	496	1726	64:56.98\$	140:36.97E	2713	-	1739	64:56.968	140:36.63E	2723
54 F1.2	1939 4	4-AUG-95	65:02.29S	140:37.98E 2598	496	1952	65:02.26S	140:37.62E	2608	-	2011	65:02.228	140:37.09E	2518
55 F1.3	2213 4	4-AUG-95	65:06.95S	140:34.41E 2471	500	2231	65:06.91S	140:34.00E	2471	-	2248	65:06.908	140:33.66E	2501
56 F1.4	0021 5	5-AUG-95	65:10.43S	140:32.34E 2217	496	0042	65:10.40S	140:31.93E	2232	-	0056	65:10.418	140:31.67E	2252
57 F1.5	0250 5	5-AUG-95	65:10.33S	140:21.43E 2383	496	0306	65:10.33S	140:21.26E	-	-	0318	65:10.338	140:20.98E	2406
58 F1.6	0454 5	5-AUG-95	65:09.28S	140:09.12E 2569	496	0510	65:09.30S	140:08.93E	-	-	0523	65:09.298	140:08.75E	2569
59 F1.7				139:57.79E 2746	498	0651	65:08.03S	139:57.66E	-	-	0707	65:07.998	139:57.50E	2774
60 F1.8	0757 5	5-AUG-95	65:07.04S	139:47.20E 2538	496	0814	65:06.98S	139:47.10E	2544	-	0830	65:06.958	139:46.83E	2508
61 F1.9	0953 5	5-AUG-95	65:05.44S	139:34.91E 2537	496	1008	65:05.45S	139:34.86E	-	-	1018	65:05.448	139:34.83E	2539
62 F1.10	1159 5	5-AUG-95	65:05.16S	139:25.27E 2688	498	1212	65:05.15S	139:25.16E	2703	-	1227	65:05.148	139:25.13E	2698
63 F1.11	1508 5	5-AUG-95	65:03.01S	139:12.11E 2911	496	1523	65:03.02S	139:12.06E	2911	-	1534	65:03.008	139:12.03E	2911
64 F1.12	1733 5	5-AUG-95	65:01.59S	139:00.64E 2595	496	1748	65:01.59S	139:00.56E	2595	-	1802	65:01.585	139:00.52E	2589
65 F1.13	1934 5	5-AUG-95	65:00.31S	138:48.70E 2314	498	1948	65:00.30S	138:48.65E	2314	-	2002	65:00.278	138:48.67E	2314
66 F1.14	2255 5	5-AUG-95	64:59.08S	138:37.25E 2524	496	2311	64:59.10S	138:37.16E	-	-	2331	64:59.098	138:37.09E	2524
67 F1.15	0348 6	6-AUG-95	64:57.75S	138:26.05E 2205	498	0402	64:57.75S	138:25.99E	2201	-	0423	64:57.778	138:25.92E	2201
68 F1.16	0620 6	6-AUG-95	64:57.01S	138:15.69E 2498	498	0632	64:57.03S	138:15.69E	2500	-	0646	64:57.068	138:15.60E	2500
69 F1.17	1058 6	6-AUG-95	64:51.54S	138:17.32E 2630	498	1110	64:51.54S	138:17.57E	2683	-	1128	64:51.538	138:17.68E	2611
70 F1.18	1500 6	6-AUG-95	64:46.44S	138:20.80E 2858	498	1512	64:46.41S	138:21.00E	2838	-	1528	64:46.305	138:21.08E	-
71 F1.19	1634 6	6-AUG-95	64:41.61S	138:23.81E 2858	496	1651	64:41.52S	138:23.88E	2867	-	1708	64:41.418	138:24.18E	2867
72 F1.20	1805 6	6-AUG-95	64:37.03S	138:26.85E 2853	496	1820	64:36.98S	138:26.97E	2843	-	1838	64:36.898	138:27.03E	2843

station	START						BOT	ГОМ				END			
number	time	date	latitude	longitude depth(m)	(dbar)	time	latitude	longitude	depth(m	) altimeter	time	latitude	longitude	depth(m)	
73 F1.21	1925	6-AUG-95	64:32.33S	138:30.00E 3086	498	1940	64:32.25S	138:30.00E	3096	-	1959	64:32.22S	138:30.05E	3096	
74 F1.22	2107	6-AUG-95	64:27.42S	138:33.24E 3188	498	2123	64:27.42S	138:33.27E	3183	-	2139	64:27.35S	138:33.25E	3183	
75 F1.23	2235	6-AUG-95	64:22.86S	138:36.08E 3287	496	2252	64:22.85S	138:36.13E	3287	-	2306	64:22.83S	138:36.24E	3287	
76 F1.24	0002	7-AUG-95	64:17.79S	138:38.57E 3392	496	0015	64:17.82S	138:38.79E	3402	-	0028	64:17.82S	138:38.98E	3402	
77 F1.25	0121	7-AUG-95	64:12.81S	138:40.75E 3480	500	0132	64:12.83S	138:40.83E	3480	-	0151	64:12.79S	138:41.23E	3480	
78 F1.26	0322	7-AUG-95	64:08.17S	138:44.91E 3564	498	0337	64:08.13S	138:45.25E	3564	-	0358	64:08.04S	138:45.64E	3571	
79 F1.27	0446	7-AUG-95	64:03.24S	138:48.02E 3677	498	0458	64:03.20S	138:48.31E	-	-	0516	64:03.21S	138:48.61E	-	
80 F1.28	0553	7-AUG-95	63:58.39S	138:50.63E 3706	500	0610	63:58.50S	138:51.34E	-	-	0627	63:58.34S	138:52.12E	3737	
81 F1.29	0715	7-AUG-95	63:59.61S	139:02.32E 3699	498	0727	63:59.59S	139:02.66E	3700	-	0746	63:59.52S	139:03.19E	3700	
82 F1.30	0847	7-AUG-95	64:00.56S	139:13.69E 3618	496	0900	64:00.48S	139:13.91E	3620	-	0915	64:00.54S	139:14.46E	3621	
83 F1.31	1027	7-AUG-95	64:02.70S	139:26.35E 3629	498	1038	64:02.67S	139:26.59E	3629	-	1057	64:02.74S	139:26.97E	-	
84 F1.32	1147	7-AUG-95	64:03.85S	139:36.33E 3614	498	1158	64:03.76S	139:36.71E	-	-	1209	64:03.67S	139:37.09E	3604	
85 F1.33	1306	7-AUG-95	64:05.16S	139:49.29E 3631	498	1319	64:05.06S	139:49.57E	-	-	1335	64:04.90S	139:49.94E	3635	
86 F1.34	1431	7-AUG-95	64:06.24S	139:59.92E 3655	498	1445	64:06.07S	140:00.27E	-	-	1503	64:05.97S	140:00.56E	-	
87 F1.35	1539	7-AUG-95	64:07.34S	140:11.71E 3610	500	1552	64:07.24S	140:12.03E	-	-	1611	64:07.13S	140:12.49E	-	
88 F1.36	1649	7-AUG-95	64:08.93S	140:23.59E 3612	496	1659	64:08.89S	140:23.77E	-	-	1712	64:08.76S	140:24.00E	3612	
89 F1.37	1740	7-AUG-95	64:10.22S	140:34.32E 3610	496	1753	64:10.21S	140:34.24E	3610	-	1808	64:10.06S	140:34.20E	3610	
90 F1.38	1900	7-AUG-95	64:11.54S	140:46.92E 3594	496	1915	64:11.59S	140:46.86E	-	-	1929	64:11.67S	140:46.75E	3589	
91 F1.39	2009	7-AUG-95	64:12.76S	140:58.08E 3597	498	2022	64:12.82S	140:58.11E	3597	-	2042	64:12.93S	140:58.41E	3592	
92 F1.40	2117	7-AUG-95	64:13.92S	141:09.21E 3623	498	2130	64:13.87S	141:09.42E	3518	-	2147	64:13.93S	141:09.47E	3518	
93 F1.41	2312	7-AUG-95	64:18.78S	141:06.73E 3550	498	2324	64:18.78S	141:06.79E	3550	-	2338	64:18.70S	141:06.75E	3550	
94 F1.42	-			141:03.08E 3467	498	0133	64:23.74S	141:03.34E	3472	-	0145	64:23.71S	141:03.51E	3472	
95 F1.43				141:00.15E 3365	496			141:00.26E		-		64:28.37S			
96 F1.44	0536	8-AUG-95	64:33.28S	140:57.15E 3264	508	0548	64:33.28S	140:57.25E	-	-	0606	64:33.25S	140:57.55E	3268	
97 F1.45	0827	8-AUG-95	64:38.23S	140:54.08E 3100	498	0839	64:38.20S	140:54.09E	-	-	0902	64:38.18S	140:54.19E	3106	
98 F1.46	0957	8-AUG-95	64:42.84S	140:52.30E 2881	496	1008	64:42.83S	140:52.24E	2881	-	1021	64:42.84S	140:52.17E	2880	
99 F1.47	1153	8-AUG-95	64:48.04S	140:48.28E 2699	498	1203	64:48.00S	140:48.15E	2696	-		64:47.97S			
100 F1.48	1308	8-AUG-95	64:52.68S	140:45.46E 2602	498	1317	64:52.59S	140:45.33E	2611	-	1332	64:52.57S	140:45.07E	2620	
101 SR3	1709	9-AUG-95	65:30.64S	139:44.93E 1761	1736	1757	65:30.63S	139:45.07E	1761	10.7	1850	65:30.64S	139:45.07E	1759	
102 SR3	2015	9-AUG-95	65:27.61S	139:47.82E 2074	2072	2114	65:27.66S	139:47.67E	2069	11.6	2213	65:27.71S	139:47.62E	2069	
103 SR3	2318	9-AUG-95	65:21.79S	139:56.58E 2551	2538	0010	65:21.80S	139:56.44E	2561	12.8	0104	65:21.80S	139:56.31E	2561	
104 TEST	1041	12-AUG-95	64:21.328	139:16.75E 3583	3582	1154	64:21.39S	139:15.34E	-	16.7	1259	64:21.58S	139:13.36E	-	
105 TEST	1726	12-AUG-95	64:40.888	3 138:31.57E 2701	2706	1848	64:40.68S	138:30.29E	2721	11.1	2001	64:40.48S	138:29.10E	2721	
106 F2.19	1734	14-AUG-95	64:41.958	138:22.80E 2767	500	1752	64:41.91S	138:22.49E	2780	-	1811	64:41.88S	138:22.18E	2780	
107 F2.20	1945	14-AUG-95	64:37.118	138:25.50E 2865	496	2005	64:37.08S	138:25.29E	-	-	_	64:37.03S			
108 F2.21	2217	14-AUG-95	64:32.288	138:29.28E 3043	498	2230	64:32.23S	138:29.10E	3037		2244	64:32.20S	138:28.95E	3036	

station	START						BOT	ГОМ				EN	D	
number	time	date	latitude	longitude depth(m)	(dbar)	time	latitude	longitude	depth(m	) altimeter	time	latitude	longitude	depth(m)
109 F2.22	2346 1	14-AUG-95	64:27.59S	138:34.14E 3225	498	2357	64:27.60S	138:34.00E	3225	-	0019	64:27.59S	138:33.54E	3225
110 F2.23	0320 1	15-AUG-95	64:22.69S	138:35.08E 3276	498	0337	64:22.67S	138:34.84E	3297	-	0402	64:22.61S	138:34.21E	3328
111 F2.24	0458 1	15-AUG-95	64:17.74S	138:38.63E 3419	498	0525	64:17.62S	138:37.98E	3409	-	0541	64:17.54S	138:37.54E	3429
112 F2.25	0705 1	15-AUG-95	64:12.96S	138:41.11E 3471	498	0717	64:12.91S	138:40.82E	-	-	0734	64:12.87S	138:40.31E	-
113 F2.26	0830 1	15-AUG-95	64:08.07S	138:44.31E 3583	498	0843	64:08.04S	138:44.04E	-	-	0903	64:07.96S	138:43.53E	3573
114 F2.27	1016 1	15-AUG-95	64:03.25S	138:47.02E 3686	498	1027	64:03.22S	138:46.87E	-	-	1041	64:03.21S	138:46.49E	3676
115 F2.28	1151 1	15-AUG-95	63:58.55S	138:50.14E 3716	498	1201	63:58.54S	138:49.92E	-	-	1219	63:58.54S	138:49.50E	3706
116 F2.29	1328 1	15-AUG-95	63:59.70S	139:01.86E 3706	498	1338	63:59.70S	139:01.62E	3696	-	1352	63:59.68S	139:01.36E	3706
117 F2.30	1458 1	15-AUG-95	64:01.04S	139:13.75E 3634	498	1510	64:01.07S	139:13.54E	3634	-	1528	64:01.04S	139:13.17E	3634
118 F2.31	1626 1	15-AUG-95	64:02.41S	139:25.20E 3604	498	1638	64:02.43S	139:24.99E	3604	-	1652	64:02.44S	139:24.70E	3604
119 F2.32	1739 1	15-AUG-95	64:03.69S	139:36.59E 3609	498	1754	64:03.60S	139:36.21E	3635	-	1809	64:03.57S	139:35.86E	3635
120 F2.33	1924 1	15-AUG-95	64:04.91S	139:48.41E 3634	498	1939	64:04.86S	139:48.09E	3639	-	2002	64:04.77S	139:47.47E	3634
121 F2.34	2106 1	15-AUG-95	64:06.19S	139:59.58E 3634	498	2122	64:06.10S	139:59.20E	3654	-	2136	64:06.01S	139:58.77E	3654
122 F2.35	2236 1	15-AUG-95	64:07.57S	140:11.61E 3645	498	2249	64:07.50S	140:11.22E	3634	-	2303	64:07.47S	140:10.84E	3634
123 F2.36	0006 1	16-AUG-95	64:09.56S	140:23.98E 3614	498	0020	64:09.49S	140:23.39E	3614	-	0033	64:09.42S	140:23.01E	3634
124 F2.37	0127 1	16-AUG-95	64:10.30S	140:34.55E 3593	504	0140	64:10.26S	140:34.16E	3634	-	0156	64:10.29S	140:33.84E	3634
125 F2.38	0257 1	16-AUG-95	64:11.44S	140:46.03E 3645	500	0310	64:11.47S	140:45.61E	-	-	0328	64:11.52S	140:45.10E	3604
126 F2.39	0436 1	16-AUG-95	64:12.75S	140:57.40E 3604	498	0450	64:12.73S	140:57.12E	3604	-	0511	64:12.81S	140:56.59E	3604
127 F2.40	0621 1	16-AUG-95	64:14.12S	141:08.89E 3604	498	0634	64:14.13S	141:08.59E	3604	-	0650	64:14.19S	141:08.18E	3604
128 F2.41	0757 1	16-AUG-95	64:18.81S	141:05.85E 3553	498	0809	64:18.85S	141:05.73E	-	-	0825	64:18.90S	141:05.50E	3553
129 F2.42	0929 1	16-AUG-95	64:23.62S	141:02.69E 3450	498	0941	64:23.64S	141:02.61E	3450	-	1000	64:23.61S	141:02.33E	3440
130 F2.43	1108 1	16-AUG-95	64:28.61S	141:00.02E 3389	498	1117	64:28.58S	141:00.00E	3368	-	1129	64:28.56S	140:59.83E	3358
131 F2.44				140:56.42E 3276	498			140:56.30E		-			140:56.08E	
132 F2.45	1606 1	16-AUG-95	64:37.72S	140:53.68E 3092	498	1617	64:37.70S	140:53.42E	3092	-	1631	64:37.63S	140:53.06E	3092
133 F2.46	1750 1	16-AUG-95	64:43.02S	140:50.58E 2856	498	1806	64:42.99S	140:50.31E	2851	-	1825	64:42.94S	140:49.86E	2851
134 F2.47	2119 1	16-AUG-95	64:47.72S	140:47.04E 2725	498			140:46.89E	-	-	2145	64:47.65S	140:46.58E	2719
135 F2.48	2342 1	16-AUG-95	64:52.54S	140:44.37E 2600	498	2357	64:52.47S	140:44.16E	2616	-	0012	64:52.45S	140:43.98E	2642
136 F2.1	0337 1	17-AUG-95	64:57.43S	140:41.82E 2518	498	0347	64:57.28S	140:41.07E	2535	-	0413	64:57.20S	140:40.50E	2550
137 F2.2	0845 1	17-AUG-95	65:02.08S	140:38.31E 2559	500	0859	65:02.08S	140:38.28E	2580	-	0913	65:02.06S	140:38.18E	2580
138 F2.3	1032 1	17-AUG-95	65:06.96S	140:35.71E 2406	498	1042	65:06.94S	140:35.59E	2385	-	1054	65:06.87S	140:35.56E	2365
139 F2.4	1209 1	17-AUG-95	65:12.00S	140:33.18E 2252	500	1219	65:11.94S	140:33.16E	2242	-	1237	65:11.90S	140:33.15E	2232
140 F2.5	1350 1	17-AUG-95	65:10.41S	140:20.97E 2395	498	1400	65:10.41S	140:20.96E	2395	-	1412	65:10.35S	140:20.92E	2395
141 F2.6	1552 1	17-AUG-95	65:09.35S	140:09.27E 2559	498	1607	65:09.34S	140:09.33E	2567	-	1626	65:09.27S	140:09.32E	2569
142 F2.7	1754 1	17-AUG-95	65:08.01S	139:57.91E 2744	498	1808	65:07.98S	139:57.96E	2739	-	1823	65:07.97S	139:58.02E	2739
143 F2.8	2020 1	17-AUG-95	65:06.90S	139:46.59E 2514	498	2033	65:06.88S	139:46.73E	2529	-	2049	65:06.91S	139:46.81E	2534
144 F2.9	2220 1	17-AUG-95	65:05.61S	139:34.99E 2511	498	2234	65:05.61S	139:35.08E	2526	-	2249	65:05.56S	139:35.34E	2531

station	START						ВОТ	ТОМ				END			
number	time	date	latitude	longitude depth(m)	(dbar)	time	latitude	longitude	depth(m	) altimeter	time	latitude	longitude	depth(m)	
	I														
145 F2.10	0505 1	18-AUG-95	65:04.17S	139:24.01E 3010	498	0517	65:04.14S	139:24.13E	-	-	0538	65:04.10S	139:24.33E	3030	
146 F2.11	0802 1	18-AUG-95	65:03.01S	139:13.23E 2907	498	0814	65:02.98S	139:13.32E	2917	-	0832	65:02.95S	139:13.38E	2917	
147 F2.12	1033 1	18-AUG-95	65:01.70S	139:01.50E 2617	498	1045	65:01.69S	139:01.57E	2627	-	1058	65:01.65S	139:01.64E	2627	
148 F2.13	1432 1	18-AUG-95	65:00.33S	138:49.09E 2319	500	1446	65:00.31S	138:49.12E	2315	-	1508	65:00.27S	138:49.23E	2313	
149 F2.14	1959 1	18-AUG-95	64:58.96S	138:36.09E 2445	498	2012	64:58.94S	138:36.14E	2440	-	2024	64:58.90S	138:36.12E	2440	
150 F2.15	2127 1	18-AUG-95	64:57.67S	138:25.90E 2215	496	2141	64:57.63S	138:25.88E	2230	-	2154	64:57.63S	138:25.91E	2230	
151 F2.16	2254 1	18-AUG-95	64:55.47S	138:15.13E 2588	498	2307	64:55.52S	138:15.13E	2593	-	2318	64:55.40S	138:15.18E	2598	
152 F2.17	0054 1	19-AUG-95	64:51.06S	138:07.90E 3034	498	0106	64:51.03S	138:07.93E	3034	-	0124	64:50.99S	138:07.99E	3028	
153 F2.18	0429 1	19-AUG-95	64:45.37S	138:15.57E 3163	498	0439	64:45.37S	138:15.67E	-	-	0453	64:45.33S	138:15.70E	3173	
154 F3.18	1501 2	20-AUG-95	64:46.93S	138:20.56E 2877	500	1512	64:46.96S	138:20.45E	2908	-	1526	64:46.99S	138:20.19E	2918	
155 F3.19	1652 2	20-AUG-95	64:41.94S	138:23.50E 2810	498	1705	64:41.98S	138:23.25E	2805	-	1723	64:42.02S	138:22.93E	2805	
156 F3.20	1850 2	20-AUG-95	64:37.18S	138:26.85E 2851	498	1907	64:37.21S	138:26.52E	2856	-	1923	64:37.24S	138:26.20E	2851	
157 F3.21	2024 2	20-AUG-95	64:32.38S	138:28.80E 3023	498	2039	64:32.41S	138:28.43E	3028	-	2055	64:32.50S	138:28.00E	3033	
158 F3.22	2201 2	20-AUG-95	64:27.46S	138:31.82E 3174	498	2215	64:27.48S	138:31.52E	3174	-	2229	64:27.52S	138:31.06E	3174	
159 F3.23	2352 2	20-AUG-95	64:22.65S	138:34.54E 3297	498	0006	64:22.69S	138:34.00E	3317	-	0025	64:22.74S	138:33.16E	3327	
160 F3.24	0136 2	21-AUG-95	64:18.09S	138:37.29E 3389	498	0148	64:18.15S	138:36.75E	3389	-	0201	64:18.16S	138:36.14E	3389	
161 F3.25	0314 2	21-AUG-95	64:12.97S	138:41.14E 3460	498	0327	64:12.96S	138:40.58E	3450	-	0343	64:13.04S	138:39.84E	3450	
162 F3.26	0444 2	21-AUG-95	64:08.16S	138:44.28E 3573	498	0455	64:08.18S	138:43.86E	3573	-	0514	64:08.22S	138:42.99E	3563	
163 F3.27	0622 2	21-AUG-95	64:03.40S	138:47.13E 3686	498	0632	64:03.43S	138:46.71E	3676	-	0650	64:03.51S	138:46.03E	3676	
164 F3.28	0755 2	21-AUG-95	63:58.65S	138:49.66E 3696	498	0808	63:58.72S	138:49.24E	3696	-	0823	63:58.78S	138:48.69E	3711	
165 F3.29	0946 2	21-AUG-95	63:59.85S	139:01.84E 3696	498	1000	63:59.94S	139:01.39E	-	-	1019	64:00.03S	139:00.64E	3717	
166 F3.30	1129 2	21-AUG-95	64:01.35S	139:13.29E 3604	498	1143	64:01.46S	139:12.67E	3604	-	1158	64:01.56S	139:12.21E	3604	
167 F3.31				139:25.30E 3614	498			139:24.56E		-			139:24.17E		
168 F3.32	1436 2	21-AUG-95	64:03.81S	139:35.83E 3634	502	1457	64:03.91S	139:35.43E	3634	-	1510	64:03.99S	139:35.27E	3634	
169 F3.33	1625 2	21-AUG-95	64:04.89S	139:48.28E 3634	498	1637	64:04.90S	139:47.80E	3634	-	1656	64:04.89S	139:47.16E	3634	
170 F3.34				139:59.51E 3645	498	1813	64:06.25S	139:59.04E	3645	-			139:58.43E		
171 F3.35				140:10.68E 3604	498			140:09.96E		-	2007	64:07.42S	140:09.20E	3604	
172 F3.36	2130 2	21-AUG-95	64:08.32S	140:21.48E 3634	500	2144	64:08.25S	140:21.21E	3634	-	2155	64:08.32S	140:20.45E	3604	
173 F3.37	2316 2	21-AUG-95	64:10.53S	140:36.97E 3634	498	2331	64:10.32S	140:36.00E	3604	-	2350	64:10.10S	140:34.58E	3604	
174 F3.38	0041 2	22-AUG-95	64:11.08S	140:44.86E 3604	498	0054	64:10.93S	140:44.11E	3604	-	0115	64:10.78S	140:42.87E	3604	
175 F3.39	0305 2	22-AUG-95	64:12.69S	140:56.98E 3604	498	0316	64:12.61S	140:56.53E	3604	-	0331	64:12.54S	140:55.72E	3604	
176 F3.40	0436 2	22-AUG-95	64:14.02S	141:08.70E 3604	498	0447	64:13.98S	141:08.26E	3604	-	0506	64:13.91S	141:07.60E	3604	
177 F3.41	0552 2	22-AUG-95	64:18.81S	141:05.60E 3563	504	0603	64:18.74S	141:05.35E	3563	-	0622	64:18.64S	141:04.87E	3563	
178 F3.42	0719 2	22-AUG-95	64:23.56S	141:02.71E 3471	496	0730	64:23.49S	141:02.50E	3440	-	0742	64:23.40S	141:02.27E	3405	
179 F3.43				140:59.28E 3348	498	0905	64:28.32S	140:59.02E	3348	-			140:58.74E		
180 F3.44	1030 2	22-AUG-95	64:33.06S	140:56.27E 3286	498	1044	64:32.98S	140:55.99E	3276	-	1057	64:32.84S	140:55.83E	3276	

station			STAR'	Т	maxP		ВС	OTTC	OM				EN	D	
number	time	date	latitude	longitude depth(m)	(dbar)	time	latitude	e l	ongitude o	depth(m	) altimeter	time	latitude	longitude	depth(m)
181 F3.45	1210 2	2-AUG-95	64:37.66S	140:53.70E 3102	498	1222	64:37.61	1S 14	40:53.56E	3102	-	1237	64:37.53S	140:53.31E	3092
182 F3.46	1348 2	2-AUG-95	64:42.79S	140:50.07E 2860	498	1359	64:42.75	5S 14	40:49.98E	2860	-	1416	64:42.66S	140:49.72E	2860
183 F3.47	1555 2	2-AUG-95	64:47.51S	140:47.36E 2741	498	1608	64:47.47	7S 14	40:47.24E	2741	-	1621	64:47.43S	140:47.11E	2741
184 F3.48	1728 2	2-AUG-95	64:52.67S	140:44.57E 2613	498	1740	64:52.62	2S 14	40:44.44E	2593	-	1753	64:52.58S	140:44.32E	2603
185 F3.1	1905 2	22-AUG-95	64:57.69S	140:40.87E 2540	498	1917	64:57.64	4S 14	40:40.77E	2545	-	1931	64:57.62S	140:40.68E	2545
186 F3.2	2053 2	2-AUG-95	65:02.19S	140:38.50E 2581	500	2106	65:02.18	8S 14	40:38.36E	2581	-	2122	65:02.14S	140:38.31E	2581
187 F3.3	2244 2	22-AUG-95	65:07.15S	140:35.33E 2448	498	2257	65:07.12	2S 14	40:35.29E	2453	-	2312	65:07.08S	140:35.24E	2458
188 F3.4	0050 2	23-AUG-95	65:12.06S	140:32.47E 2227	498	0104	65:12.03	3S 14	40:32.37E	2227	-	0118	65:11.98S	140:32.27E	2227
189 F3.5	0258 2	23-AUG-95	65:10.69S	140:20.81E 2387	500	0309	65:10.67	7S 14	40:20.67E	2387	-	0327	65:10.61S	140:20.58E	2387
190 F3.6	0434 2	23-AUG-95	65:09.34S	140:09.38E 2566	498	0444	65:09.32	2S 14	40:09.29E	2566	-	0457	65:09.30S	140:09.22E	2564
191 F3.7	0652 2	23-AUG-95	65:08.00S	139:57.58E 2764	498	0702	65:07.99	9 <mark>S</mark> 13	39:57.57E	2764	-	0714	65:07.98S	139:57.51E	2764
192 F3.8	0825 2	23-AUG-95	65:06.84S	139:46.30E 2493	498	0837	65:06.81	1S 13	39:46.23E	2473	-	0855	65:06.81S	139:46.20E	2473
193 F3.9	1003 2	23-AUG-95	65:05.61S	139:35.49E 2520	532	1017	65:05.60	0S 13	39:35.47E	2510	-	1032	65:05.56S	139:35.41E	2510
194 F3.10	1155 2	23-AUG-95	65:04.12S	139:23.08E 3000	498	1212	65:04.09	9S 13	39:23.07E	3009	-	1226	65:04.07S	139:23.03E	3010
195 F3.11	1331 2	23-AUG-95	65:03.00S	139:12.16E 2915	498	1346	65:02.98	8S 13	39:12.27E	2915	-	1402	65:02.92S	139:12.18E	2915
196 F3.12	1512 2	23-AUG-95	65:01.65S	139:00.33E 2617	498	1526	65:01.62	2S 13	39:00.37E	2622	-	1538	65:01.59S	139:00.33E	2622
197 F3.13	1655 2	23-AUG-95	65:00.33S	138:49.08E 2317	498	1706	65:00.30	0S 13	38:49.08E	2312	-	1718	65:00.25S	138:49.05E	2312
198 F3.14	1902 2	23-AUG-95	64:58.87S	138:37.50E 2522	498	1916	64:58.86	6S 13	38:37.47E	2517	-	1930	64:58.86S	138:37.50E	2522
199 F3.15	2110 2	23-AUG-95	64:57.75S	138:25.71E 2211	498	2120	64:57.77	7S 13	38:25.69E	-	-	2137	64:57.71S	138:25.77E	-
200 F3.16	0022 2	24-AUG-95	64:56.60S	138:14.10E 2576	500	0035	64:56.58	8S 13	38:14.09E	2566	-	0050	64:56.55S	138:14.04E	2573
201 F3.17	0254 2	24-AUG-95	64:51.57S	138:17.44E 2626	500				38:17.37E		-	0323	64:51.55S	138:17.37E	2640
202 SR3	1840 2	26-AUG-95	61:20.97S	139:52.00E 4402	4394	2046	61:19.93	3S 13	39:53.78E	4402	20.1	2230	61:19.68S	139:54.45E	4402
203 SR3	0253 2	27-AUG-95	60:51.05S	139:50.80E 4491	4462	0438	60:52.41	1S 13	39:49.81E	-	-	0616	60:53.09S	139:49.96E	-
204 SR3				139:50.65E 4505	4502				39:51.14E	-	16.1			139:51.40E	
205 SR3				143:29.56E 3563	3584				43:30.40E	3543	15.1			143:31.36E	
206 SR3	_			143:38.08E 3450	3696				43:39.64E	-	23.1			143:40.63E	
207 SR3	0257 3	80-AUG-95	51:32.13S	143:46.77E 3757	3796	0435	51:31.89	9S 14	43:47.71E	-	15.3	0554	51:31.35S	143:48.27E	-
208 SR3	1020 3	80-AUG-95	51:16.18S	143:54.75E 3757	3828	1206	51:16.51	1S 14	43:55.39E	-	25.0	1326	51:16.62S	143:56.33E	-

Table 1.3: Summary of samples drawn from Niskin bottles at each station, including salinity (sal), dissolved oxygen (do), nutrients (nut), dissolved inorganic carbon (dic), dissolved organic carbon (doc), iodate/iodide (i), primary productivity (pp), and the following biological samples: pigments (pig), microscopial protist examination (pro), cyanobacteria counts (cya), lugols iodine fixed plankton counts (lug), scanning and transmission electron microscopy (te), subsample of protist concentrate preserved (vir), and samples for culturing (cul). Note that 1=samples taken, 0=no samples taken, 2=surface sample only (i.e. from shallowest Niskin bottle).

											bio	ology			
St	tation	sal	do	nut	dic	doc	i	рр	pig	pro	cya	lug	te	vir	cul
1	TEST	1	1	1	0	0	0	0	0	0	0	0	0	0	0
2	SR3	1	1	1	2	0	1	1	1	0	1	0	0	0	0
3	SR3	1	1	1	0	0	1	0	0	0	0	0	0	0	0
4	SR3	1	1	1	0	0	1	0	1	1	1	0	0	0	0
5	SR3	1	1	1	2	0	1	0	0	0	0	0	0	0	0
6	SR3	1	1	1	0	1	1	1	1	0	1	0	0	0	0
7	SR3	1	1	1	0	0	0	0	1	1	1	1	0	0	0
8	SR3	1	1	1	2	0	1	1	0	0	0	0	0	0	0
9	SR3	1	1	1	0	1	1	0	1	1	1	0	0	0	0
10	SR3	1	1	1	2	0	1	0	0	0	0	0	0	0	0
11	SR3	1	1	1	0	0	1	0	1	1	1	1	0	0	0
12	SR3	1	1	1	0	0	1	1	0	0	0	0	0	0	0
13	SR3	1	1	1	2	0	1	0	1	1	1	0	0	0	0
14	SR3	1	1	1	0	0	1	0	0	0	0	0	0	0	0
15	SR3	1	1	1	2	1	1	0	1	1	1	1	1	1	1
16	SR3	1	1	1	0	0	0	0	0	0	0	0	0	0	0
17	SR3	1	1	1	0	0	0	0	1	1	1	1	0	0	0
18	SR3	1	1	1	2	0	1	0	0	0	0	0	0	0	0
19	SR3	1	1	1	0	0	1	0	1	1	1	0	0	0	0
20	SR3	1	1	1	0	0	0	1	1	1	1	1	0	0	0
21	SR3	1	1	1	2	1	1	0	0	0	0	0	0	0	0
22	SR3	1	1	1	0	0	0	0	0	0	0	0	0	0	0
23	SR3	1	1	1	0	0	0	0	0	0	0	0	0	0	0
24	SR3	1	1	1	0	0	1	1	1	1	1	0	1	1	1
25	SR3	1	1	1	2	0	0	0	0	0	0	0	0	0	0
26	SR3	1	1	1	0	1	1	0	1	1	1	0	0	0	0
27	SR3	1	1	1	2	0	0	0	0	0	0	0	0	0	0
28	SR3	1	1	1	0	0	1	0	0	0	0	0	0	0	0
29	SR3	1	1	1	0	0	1	1	1	1	1	0	1	1	0
30	SR3	1	1	1	2	0	1	0	1	1	1	0	1	0	0
31	SR3	1	1	1	2	1	0	0	0	0	0	0	0	0	0
32	SR3	1	1	1	0	0	1	1	1	1	1	0	1	1	1
33	SR3	1	1	1	0	0	0	0	0	0	0	0	0	0	0
34	SR3	1	1	1	2	1	1	0	1	1	0	0	0	1	0
35	SR3	1	1	1	0	0	0	0	0	0	0	0	0	0	0
36	SR3	1	1	1	2	0	1	1	1	1	1	0	0	1	0
37	SR3	1	1	1	0	0	0	0	1	1	1	0	0	1	0
38	SR3	1	1	1	2	0	0	0	0	0	0	0	0	0	0
39	SR3	1	1	1	2	1	1	1	1	1	1	1	0	1	0
40	SR3	1	1	1	0	0	0	0	1	1	0	0	0	1	0
41	SR3	1	1	1	2	0	1	0	0	0	0	0	0	0	0
42	SR3	1	1	1	0	1	1	1	1	1	1	0	0	1	0

Station												bio	ology	,		
44   SR3	St	tation	sal	do	nut	dic	doc	i	рр	pig	pro		_		vir	cul
45   SR3	43	SR3	1	1	1	0	0	0	0	1	0	0	0	0	0	0
46   SR3	44	SR3	1	1	1	2	0	0	0	0	0	0	0	0	0	0
47   SR3	45	SR3	1	1	1	2	0	0	1	1	1	1	0	0	1	0
Heat   Heat	46	SR3	1	1	1	0	1	1	0	1	1	0	1	0	1	0
49   SR3	47	SR3	1	1	1	0	0	0	0	0	0	0	0	0	0	0
SR3	48	SR3	1	1	1	1	0	1	1	1	1	1	0	1	1	0
51         SR3         1         1         1         2         0         1         0         1         1         1         0          5         1         1	49	SR3	1	1	1	0	0	0	0	1	1	0	0	0	1	0
S2   SR3	50	SR3	1	1	1	2	1	0	0	0	0	0	0	0	0	0
53-56         F1.1-F1.5         1         1         1         0         <	51	SR3	1	1	1	2	0	1	0	1	1	1	0	0	1	0
57         F1.5         1         1         1         0         0         0         1         1         0 <td>52</td> <td>SR3</td> <td>1</td> <td>1</td> <td>1</td> <td>0</td>	52	SR3	1	1	1	0	0	0	0	0	0	0	0	0	0	0
58-66         F1.6-1.14         1         1         1         0         <	53-56	F1.1-F1.5	1	1	1	0	0	0	0	0	0	0	0	0	0	0
67         F1.15         1         1         1         0         0         0         1         1         1         0 <td>57</td> <td>F1.5</td> <td>1</td> <td>1</td> <td>1</td> <td>0</td> <td>0</td> <td>0</td> <td>1</td> <td>1</td> <td>0</td> <td>0</td> <td>0</td> <td>0</td> <td>0</td> <td>0</td>	57	F1.5	1	1	1	0	0	0	1	1	0	0	0	0	0	0
68-77	58-66	F1.6-1.14	1	1	1	0	0	0	0	0	0	0	0	0	0	0
78         F1.26         1         1         1         0         0         0         1         1         1         0         0         0           79-94         F1.27-1.42         1         1         1         0	67	F1.15	1	1	1	0	0	0	1	1	1	1	0	0	1	0
T9-94	68-77	F1.16-1.25	1	1	1	0	0	0	0	0	0	0	0	0	0	0
95 F1.43	78	F1.26	1	1	1	0	0	0	1	1	1	1	0	0	0	0
96-100	79-94	F1.27-1.42	1	1	1	0	0	0	0	0	0	0	0	0	0	0
101   SR3	95	F1.43	1	1	1	0	0	0	1	1	1	1	0	0	1	0
102   SR3	96-100	F1.44-1.48	1	1	1	0	0	0	0	0	0	0	0	0	0	0
103   SR3	101	SR3	1	1	1	2	1	1	0	1	1	1	0	0	1	0
104   TEST	102	SR3	1	1	1	2	0	0	0	0	0	0	0	0	0	0
105         TEST         1         0 <td>103</td> <td>SR3</td> <td>1</td> <td>1</td> <td>1</td> <td>0</td> <td>0</td> <td>1</td> <td>0</td> <td>1</td> <td>1</td> <td>0</td> <td>0</td> <td>0</td> <td>1</td> <td>0</td>	103	SR3	1	1	1	0	0	1	0	1	1	0	0	0	1	0
106-109   F2.19-2.22	104	TEST	1	0	1	0	0	0	0	0	0	0	0	0	0	0
106-109   F2.19-2.22			1	0	0	0	0	0	0	0	0	0	0	0		
111-113         F2.24-2.26         1         1         1         0	106-109	F2.19-2.22	1	1	1	0	0	0	0	0	0	0	0	0	0	
111-113         F2.24-2.26         1         1         1         0			1	1	1	0	0	0	0	1	1	0	1	0	0	
115-124         F2.28-2.37         1         1         1         0	111-113	F2.24-2.26	1	1	1	0	0	0	0	0	0	0	0	0	0	
115-124         F2.28-2.37         1         1         1         0			1	1	1	0	2	0	0		0			0		
125         F2.38         1         1         1         0         2         0         1         1         1         0 </td <td></td> <td></td> <td>1</td> <td>1</td> <td>1</td> <td>0</td> <td></td>			1	1	1	0	0	0	0	0	0	0	0	0	0	
126         F2.39         1         1         1         0         2         0 </td <td></td> <td></td> <td></td> <td>1</td> <td>1</td> <td></td>				1	1											
127-128         F2.40-2.41         1         1         1         0				1					0	0	0	0	0			
129       F2.42       1       1       1       0       2       0 </td <td></td> <td></td> <td>1</td> <td>1</td> <td>1</td> <td></td> <td></td> <td></td> <td></td> <td>_</td> <td></td> <td>_</td> <td></td> <td>_</td> <td></td> <td></td>			1	1	1					_		_		_		
130       F2.43       1       1       1       0        0       0       0       0       0       0       0       0       0       0       0       0       0       0       0        0				1		_										1
131       F2.44       1       1       1       0       2       0        0       0       0       0       0       0       0       0       0       0       0       0       0       0       0        0				1	1											
132-135         F2.45-2.48         1         1         1         0							_								_	
136       F2.1       1       1       1       0       0       0       1       1       1       0       1       0        0       0       0       0       0       0       0       0       0       0       0       0       0       0       0        0       0       0       0       0       0       0       0       0       0       0       0       0       0       0        0																
137         F2.2         1         1         1         0 <td></td>																
138         F2.3         1         1         1         0         2         0 <td></td> <td></td> <td>_</td> <td>1</td> <td>1</td> <td>0</td> <td>0</td> <td>_</td> <td>0</td> <td>0</td> <td>0</td> <td>0</td> <td>0</td> <td>_</td> <td></td> <td></td>			_	1	1	0	0	_	0	0	0	0	0	_		
139-144       F2.4-2.9       1       1       1       0				1									1			
145       F2.10       1       1       1       0       2       0       0       1       1       0       1       0       1       0       1       0       1       0       1       0       1       0       1       0       1       0       1       0       1       0       1       0 </td <td></td>																
146-151       F2.11-2.16       1       1       1       0								_	_					_		
152       F2.17       1       1       1       0       2       0 </td <td></td>																
153       F2.18       1       1       1       0       2       0       0       1       0 </td <td></td>																
154-159       F3.18-3.23       1       1       1       0								_	_					_	_	
160       F3.24       1       1       1       0       2       0 </td <td></td> <td>1</td> <td></td> <td></td> <td></td>													1			
161     F3.25     1     1     1     0     2     0     0     1     0 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>_</td><td></td><td></td></t<>														_		
162     F3.26     1     1     1     0     2     0 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>_</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>								_								
163     F3.27     1     1     1     0     2     0     0     0     0     0     0     0     0       164-173     F3.28-3.37     1     1     1     0     0     0     0     0     0     0     0     0     0																
164-173 F3.28-3.37 1 1 1 0 0 0 0 0 0 0 0 0 0 0																
								_	_					_	_	
/4.63.30	174	F3.38	1	1	1	0	2	0	0	0	0	0	0	0	0	0

											bio	ology			
S	tation	sal	do	nut	dic	doc	i	рр	pig	pro	суа	lug	te	vir	cul
175	F3.39	1	1	1	0	2	0	0	1	0	0	0	0	0	0
176	F3.40	1	1	1	0	0	0	0	0	0	0	0	0	0	0
177	F3.41	1	1	1	0	2	0	0	0	0	0	0	0	0	0
178	F3.42	1	1	1	0	0	0	0	0	0	0	0	0	0	0
179	F3.43	1	1	1	0	2	0	0	0	0	0	0	0	0	0
180-181	F3.44-3.45	1	1	1	0	0	0	0	0	0	0	0	0	0	0
182	F3.46	1	1	1	0	2	0	0	0	0	0	0	0	0	0
183-187	F3.47-3.3	1	1	1	0	0	0	0	0	0	0	0	0	0	0
188-189	F3.4-F3.5	1	1	1	0	2	0	0	0	0	0	0	0	0	0
190	F3.6	1	1	1	0	2	0	0	1	1	0	1	0	1	0
191	F3.7	1	1	1	0	0	0	0	0	0	0	0	0	0	0
192	F3.8	1	1	1	0	2	0	0	0	0	0	0	0	0	0
193-200	F3.9-F3.16	1	1	1	0	0	0	0	0	0	0	0	0	0	0
201	F3.17	1	1	1	0	0	0	0	1	0	0	1	0	0	0
202	SR3	1	1	1	0	0	0	0	1	0	0	0	0	0	0
203	SR3	1	1	1	0	0	0	0	0	0	0	0	0	0	0
204	SR3	1	1	1	0	0	0	0	0	0	0	0	0	0	0
205	SR3	1	1	1	2	0	0	0	1	1	1	1	0	1	0
206	SR3	1	1	1	0	0	0	0	0	0	0	0	0	0	0
207	SR3	1	1	1	0	0	0	1	1	1	1	1	0	1	0
208	SR3	1	1	1	2	0	0	0	0	0	0	0	0	0	0

<u>Table 1.4:</u> CTD stations over current meter (CM) and inverted echo sounder (IES) moorings along SR3 transect in the vicinity of the Subantarctic Front. Note that bottom depths are calculated using a sound speed of 1498 ms<sup>-1</sup>. For CTD station positions, see Table 1.2.

CTD station no.	start time	bottom depth (m)	mooring number
12	03:18, 21/07/95	4064	I1 (IES)
16	03:38, 22/07/95	3686	12 (IES)
17	08:49, 22/07/95	3788	I4 (IES)
18	14:14, 22/07/95	3711	16 (IES)
19	19:08, 22/07/95	3583	I8 (CM+IES)
20	00:31, 23/07/95	3655	I9 (CM+IES)
21	05:03, 23/07/95	3808	I10 (CM+IES)
22	09:52, 23/07/95	3706	I12 (IES)
23	14:51, 23/07/95	3778	I14 (IES)
24	20:04, 23/07/95	3757	I16 (IES)
25	00:55, 24/07/95	3512	I18 (IES)
205	15:32, 29/08/95	3563	117 (IES)
206	21:01, 29/08/95	3450	I15 (IES)
207	02:57, 30/08/95	3757	I13 (IES)
208	10:20, 30/08/95	3757	I11 (IES)

<u>Table 1.5a:</u> Principal investigators (\*=cruise participant) for water sampling programmes.

measurement name affiliation

CTD, salinity,  $O_2$ , nutrients (SR3) Steve Rintoul/\*Nathan Bindoff CSIRO/Antarctc CRC

CTD, salinity, O<sub>2</sub> (FORMEX) \*Nathan Bindoff/\*lan Allison Antarctic CRC/Antarctic Division

D.O.C. Tom Trull Antarctic CRC iodate/iodide Ed Butler CSIRO primary productivity John Parslow CSIRO

biological sampling Harvey Marchant Antarctic Division

D.I.C. Bronte Tilbrook CSIRO

#### Table 1.5b: Scientific personnel (cruise participants).

Wojciech Wierzbicki

· ·	` ,	
name	measurement	affiliation
Nathan Bindoff	CTD	Antarctic CRC
Ross Edwards	CTD, trace metals	Antarctic CRC
Brett Goldsworthy	CTD	Antarctic CRC
Phil Reid	CTD	Antarctic CRC
Mark Rosenberg	CTD, moorings	Antarctic CRC
Chris Zweck	CTD	Antarctic CRC
Steve Bell	salinity, oxygen, nutrients	Antarctic CRC
Stephen Bray	salinity, oxygen, nutrients	Antarctic CRC
Martina Doblin	oxygen	Antarctic CRC
Mick Mackey	primary productivity	Antarctic CRC
Rick van den Enden	biological sampling	Antarctic Division
lan Jameson	biological sampling	Antarctic Division
Ian Allison	voyage leader, sea ice	Antarctic Division
Petra Heil	sea ice	Antarctic CRC
Ian Knott	sea ice, electronics	Antarctic CRC
Vicky Lytle	sea ice	Antarctic CRC
Rob Massom	sea ice	Antarctic CRC
Anton Rada	sea ice	Antarctic Division
Tony Worby	deputy voyage leader, sea ice	Antarctic Division
Greg Bush	upward looking sonar	Curtin University
Alec Duncan	upward looking sonar	Curtin University
Kevin Bartram	ornithology Royal	Australasian Ornithologists Union
Dion Hobcroft	ornithology Royal	Australasian Ornithologists Union
Peter Gill	whale observations	Ocean Research Foundation
Debbie Thiele	whale observations	Ocean Research Foundation
Pamela Brodie	computing	Antarctic Division
Andrew Climie	doctor	Antarctic Division
Vera Hansper	computing	Antarctic Division
Graham Hosie	sea ice biology	Antarctic Division
Andrew McEldowney	gear officer	Antarctic Division
Tim Pauly	hydroacoustics	Antarctic Division
Tim Ryan	underway measurements	Antarctic Division
Hyong-chul Shin	sea ice biology	Antarctic Division

electronics

Antarctic Division

Peter Colpo	helicopters	Helicopter Resources
Adrian Pate	helicopters	Helicopter Resources
Rick Piacenza	helicopters	Helicopter Resources

Ian McCarthy weather forecaster Bureau of Meteorology

#### 1.4 FIELD DATA COLLECTION METHODS

#### 1.4.1 CTD and hydrology measurements

In this section, CTD and hydrology data collection and processing methods are discussed. Preliminary results of the CTD data calibration, along with data quality information, are presented in Section 1.6. CTD instrumentation and CTD and hydrology data collection techniques are described in detail in Rosenberg et al. (1995b). Water sampling methods are also detailed in previous data reports.

#### 1.4.1.1 CTD Instrumentation

Briefly, General Oceanics Mark IIIC (i.e. WOCE upgraded) CTD units were used, with General Oceanics model 1015 pylons, and 10 litre General Oceanics Niskin bottles. A 24 position rosette package was deployed for stations 1 to 52 and 202 to 208 along the SR3 transect, with deep sea reversing thermometers (Gohla-Precision) mounted at rosette positions 2, 12 and 24. A Li-Cor photosynthetically active radiation sensor and Sea-Tech fluorometer were also attached to the package for some casts (Table 1.20). For stations 53 to 201, a 12 position rosette package was deployed. For most FORMEX stations, 6 bottles only were mounted, at alternate rosette positions, and with reversing thermometers at rosette position 2. Extra bottles were mounted for some FORMEX stations for the collection of biological samples (Table 1.3). For stations 101 to 105, 12 Niskin bottles were mounted.

#### 1.4.1.2 CTD instrument and data calibration

Complete calibration information for the CTD pressure, platinum temperature and pressure temperature sensors are presented in Table 1.22. Post cruise pressure, platinum temperature and pressure temperature calibrations, performed at the CSIRO Division of Marine Research Calibration Facility, were available for all CTD units. The complete CTD conductivity and the limited CTD dissolved oxygen calibrations, derived respectively from the in situ Niskin bottle salinity and dissolved oxygen samples, are presented in a later section.

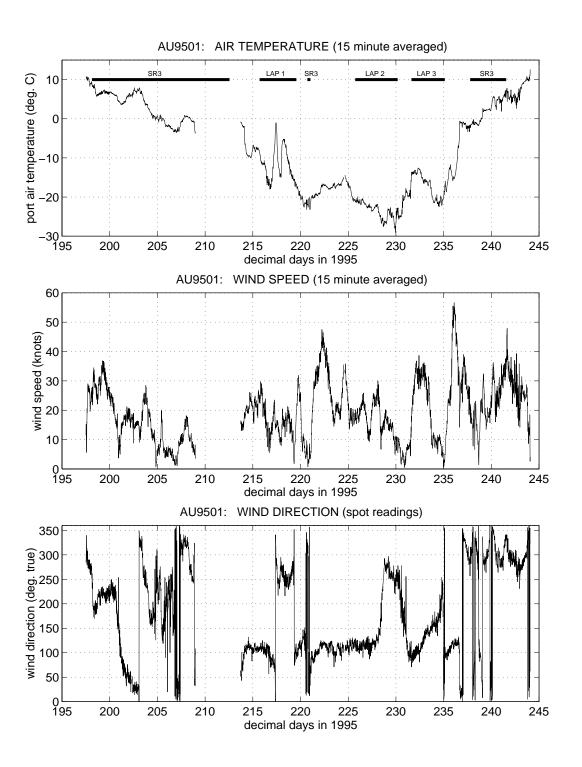
Manufacturer supplied calibrations were applied to the p.a.r. data, while fluorometer calibrations were performed at the Antarctic Division (Table 1.22). These calibrations are not expected to be correct - correct scaling of fluorescence data requires linkage with primary productivity data, while p.a.r. data requires recalculation using extinction coefficients for the signal strength (B. Griffiths, pers. comm.).

The CTD and hydrology data processing and calibration techniques are described in detail in Appendix 2 of Rosenberg et al. (1995b) (referred to as "CTD methodology" for the remainder of the report), with the following updates to the methodology:

- (i) the 10 seconds of CTD data prior to each bottle firing are averaged to form the CTD upcast for use in calibration (5 seconds was used previously);
- (ii) for stations 30 to 44, the minimum number of data points required in a 2 dbar bin to form an average was set to 6 (i.e. jmin=6; for other stations, jmin=10);

(iii) in the conductivity calibration for stations 30 to 44, an additional term was applied to remove the pressure dependent conductivity residual;

(iv) CTD raw data obtained from the CTD logging PC's no longer contain end of record characters after every 128 bytes.



<u>Figure 1.2:</u> Air temperature and wind speed and direction for cruise AU9501 from ship's underway data, including times of various cruise components (SR3 and FORMEX laps 1, 2 and 3). Note that decimal time = 0.0 at midnight of 31st December (so, e.g., midday on 2nd January = 1.5).

#### 1.4.1.3 CTD/hydrology data collection techniques in cold conditions

Extreme cold was experienced for much of the cruise (Figure 1.2), and most of the time during FORMEX the oceanographic operations were conducted in consolidated sea ice. As a result, new methods had to be developed for deployment of the rosette package. In particular, great care had to be taken to minimize freezing of the CTD sensors. After arriving on station, the ship had to first clear a hole in the sea ice (in thicker ice, this operation took up to 1 hour). During the CTD cast, stern thrusters were used to keep ice clear of the CTD wire. Bow thruster usage was minimized during FORMEX, to ensure good ADCP data whilst on station.

CTD sensor caps were filled with hypersaline water to depress the freezing point of water on the sensors. To minimize exposure of the sensors to the cold air, the caps were not drained until the package was about to be lowered into the water; and the package was lowered promptly, and while still moving out towards the end of the gantry. Adherence to these steps minimized sensor freezing, however near surface downcast conductivity data were still affected by a thin film of frozen water remaining on the conductivity cell. Upcast data were therefore used for stations 53 to 201.

When the package was retrieved, water was often frozen in the Niskin bottle spiggots, and sampling was delayed by approximately 10 to 15 minutes to allow thawing of the spiggots. On several occasions, the flow during sampling for dissolved oxygen was interrupted due to incomplete thawing, causing a long delay between opening of the Niskin bottle vent valve and taking of the sample. Dissolved oxygen samples thus affected were not analysed.

#### 1.4.1.4 Hydrology analytical methods

The analytical techniques and data processing routines employed in the Hydrographic Laboratory onboard the ship are discussed in Appendix 3 of Rosenberg et al. (1995b). Note the following changes to the methodology:

- (i) 150 ml sample bottles were used, and 1.0 ml of reagents 1, 2 and 3 were used; the corresponding calculated value for the total amount of oxygen added with the reagents = 0.017 ml;
- (ii) a mean volume of 147.00 ml for oxygen sample bottles was applied in the calculation of dissolved oxygen concentration.

#### 1.4.2 Underway measurements

Underway data collection is as described in previous data reports; data files are described in Part 5. Note that a sound speed of 1498 ms<sup>-1</sup> is used for all depth calculations, and the ship's draught of 7.3 m has been accounted for in final depth values (i.e. depths are values from the surface).

#### Table 1.6: ADCP logging parameters.

ping parameters bottom track ping parameters

no. of bins: 60 no. of bins: 128 bin length: 8 m bin length: 4 m pulse length: 8 m pulse length: 32 m

delay: 4 m

ping interval: minimum ping interval: same as profiling pings

reference layer averaging: bins 3 to 6 ensemble averaging duration: 3 min.

#### 1.4.3 ADCP

The acoustic Doppler current profiler (ADCP) instrumentation is described in Rosenberg et al. (1996). GPS data was collected by a Lowrance receiver for the first half of the cruise, and a Koden receiver for the second half. Note that the Lowrance unit received GPS positions every 2 seconds, and GPS velocities every 2 seconds, with positions and velocities received on alternate seconds; the Koden unit received both GPS positions and velocities every 1 second. ADCP data processing is discussed in more detail in Dunn (a and b, unpublished reports). Logging parameters are summarised in Table 1.6, while data results for this cruise will be discussed in a future report.

#### 1.5 MAJOR PROBLEMS ENCOUNTERED

#### 1.5.1 Logistics

Rough weather on the return northward leg prevented CTD measurements being taken at 3 of the inverted echo sounder mooring locations (mooring numbers I3, I5 and I7). Time was not available to wait for calmer conditions.

#### 1.5.2 CTD sensors

No good CTD dissolved oxygen data was obtained from CTD 1103. The problem, not diagnosed until after the cruise, was traced to an incorrectly wired oxygen sensor bulkhead connector (a factory fault). As a result, usable CTD dissolved oxygen data was only obtained from the limited number of stations where CTD 1193 was used.

The conductivity cell for CTD 1193 was faulty, displaying a large transient error when first entering the water (requiring several minutes to drift to a stable value), large hysteresis between the down and upcasts, and significant pressure dependent residuals. Conductivity data was recoverable for stations 30 to 41 (see section 1.6), but was unusable for stations 42 to 44 and 104 to 105.

Following station 50, a crack was discovered in the housing window for the photosynthetically active radiation sensor. The sensor was not used for the remainder of the cruise.

#### 1.5.3 Other equipment

Very cold conditions were experienced during the cruise (Figure 1.2). When the air temperature dropped below -20°C, icing of the CTD wire became a problem, causing jamming of the wire in the spooling sheath. On the worst occasion, several turns came off the winch drum, and several hundred metres of wire were badly kinked.

The Lowrance GPS receiver, accessed by the ADCP logging system, failed on 13/07/95. The replacement Koden unit came on line on 16/07/95. The missing 3 days of GPS data for the ADCP were obtained from data logged by the Magnavox GPS unit.

#### 1.6 CTD RESULTS

This section details information relevant to the creation and quality of the final CTD and hydrology data set. For actual use of the data, the following is important:

```
CTD data - Tables 1.14 and 1.15, and Table 1.7; hydrology data - Table 1.19.
```

Historical data comparisons are made in Part 4 of this report. Data file formats are described in Part 5.

#### 1.6.1 CTD measurements - data creation and quality

CTD data calibration and processing methods are described in detail in the CTD methodology (i.e. Appendix 2 of Rosenberg et al., 1995b, with the additions listed in section 1.4.1.2 of this report). Cases for cruise au9501 which vary from this methodology are detailed in this section. CTD data quality is also discussed. For conversion to WOCE data file formats, see Part 5 of this report.

The final calibration results for conductivity/salinity and dissolved oxygen, along with the performance check for temperature, are plotted in Figures 1.3 to 1.6. For temperature, salinity and dissolved oxygen, the respective residuals ( $T_{therm}$  -  $T_{cal}$ ), ( $s_{btl}$  -  $s_{cal}$ ) and ( $o_{btl}$  -  $o_{cal}$ ) are plotted. For conductivity, the ratio  $c_{btl}/c_{cal}$  is plotted.  $T_{therm}$  and  $T_{cal}$  are respectively the protected thermometer and calibrated upcast CTD burst temperature values;  $s_{btl}$ ,  $s_{cal}$ ,  $o_{btl}$ ,  $o_{cal}$ ,  $c_{btl}$  and  $c_{cal}$ , and the mean and standard deviation values in Figures 1.3 to 1.6, are as defined in the CTD methodology (with additional definitions described below for cases where a pressure dependent residual is removed from conductivity data).

#### 1.6.1.1 Conductivity/salinity

An excellent conductivity calibration was obtained for CTD 1103 (stations 1-29, 45-103 and 106-208) - after calibrating against bottle data, low residuals were obtained between CTD and bottle values (Figures 1.4a and 1.5a). Note that a new conductivity cell was installed on this CTD at the start of the cruise. Upcast CTD data was used for stations 53 to 103 and 106-201, owing to sensor freezing (as described in section 1.4.1.3).

The conductivity cell for CTD 1193 (stations 30-44 and 104-105) was faulty, as described in section 1.5.2. Upcast CTD data were used for these stations, due to the large transient error in conductivity when entering the water, and the significant hysteresis between downcast and upcast conductivity data. The pressure dependent conductivity residual for this cell was removed by the following steps:

- (a) CTD conductivity was initially calibrated to derive conductivity residuals ( $c_{btl}$   $c_{cal}$ ), where  $c_{btl}$  and  $c_{cal}$  are as defined in the CTD methodology, noting that  $c_{cal}$  is the conductivity value after the initial calibration only i.e. prior to any pressure dependent correction.
- (b) Next, for each station grouping (Table 1.9), a linear pressure dependent fit was found for the conductivity residuals i.e. for station grouping i, fit parameters  $\alpha_i$  (Table 1.9) and  $\beta_i$  were found from

$$(c_{btl} - c_{cal})_n = \alpha_i p_n + \beta_i$$
 (eqn 1.1)

where the residuals  $(c_{btl} - c_{cal})_n$  and corresponding pressures  $p_n$  (i.e. pressures where Niskin bottles fired) are all the values accepted for conductivity calibration in the station grouping.

(c) Lastly, the conductivity calibration was repeated, this time fitting ( $c_{ctd} + \alpha_i p$ ) to the bottle values  $c_{btl}$  in order to remove the linear pressure dependence for each station grouping i (for uncalibrated conductivity  $c_{ctd}$  as defined in the CTD methodology; and note that the offsets  $\beta_i$  were not applied).

A good conductivity calibration was obtained for stations 30 to 41 using this method (Figures 1.4b and 1.5b). However for stations 42 to 44 and 104 to 105, the conductivity data was not recoverable, owing to rapid deterioration of the cell.

The final standard deviation values for the salinity residuals (Figure 1.5) indicate the CTD salinity data over the whole cruise is accurate to within  $\pm 0.002$  (PSS78).

#### 1.6.1.2 Temperature

The comparison of CTD and thermometer temperatures is shown in Figure 1.3. The thermometer value used in each case is the mean of the two protected thermometer readings (protected thermometers used are listed in Table 1.21). Note that in the figures, the "dubious" and "rejected" categories refer to corresponding bottle samples and upcast CTD bursts in the conductivity calibration, rather than to CTD/thermometer temperature values.

Platinum temperature sensor performance of CTD's 1103 and 1193 is not consistent, as shown by the different offsets in Figures 1.3a and b. For CTD 1193 (Figure 1.3b), the offset is small (~+0.001°C), indicating a reliable laboratory calibration of the platinum temperature sensor. The offset for CTD 1103 of ~-0.007°C (Figure 1.3a), using the post cruise temperature calibration, is large. If the pre cruise temperature calibration (September 1994) is applied, the offset is ~+0.007°C, thus a significant calibration drift occurred for this CTD between the two laboratory calibrations. No attempt has been made to correct for this calibration drift, and the post cruise calibration is maintained. Note that over the actual period of the cruise, there was little calibration drift for CTD 1103, other than a possible small drift for stations 202-208 (although these stations were too few in number to confirm the trend).

#### **1.6.1.3 Pressure**

As described in previous data reports, noise in the pressure signal for CTD 1193 (used for stations 30 to 44 and 104 to 105) was high, with spikes of up to 1 dbar amplitude occurring, and with a large number of missing 2 dbar bins resulting. The number of missing bins was reduced by setting to 6 the minimum number of data points required in a 2 dbar bin to form an average (i.e. jmin=6; for CTD 1103 stations, jmin=10). For remaining missing bins, values were linearly interpolated between surrounding bins, except where the local temperature gradient exceeded 0.005°C between the surrounding bins i.e. temperature gradient > 0.00125 degrees/dbar.

For stations 22, 128 and 190, data logging commenced when the CTD was already in the water, so surface pressure offset values were estimated from surrounding stations. For stations 144 and 168, conductivity cell freezing interfered with the automatic estimation of surface pressure offsets (see CTD methodology), so surface pressure offset values were estimated from a manual inspection of the pressure data. Note that for all these stations, any resulting additional error in the CTD pressure data is judged to be small (no more than 0.2 dbar).

#### 1.6.1.4 Dissolved oxygen

Usable CTD dissolved oxygen data was only obtained from CTD 1193, stations 30 to 41, as discussed in section 1.5.2. For these stations, downcast oxygen temperature and oxygen current data were merged with the upcast pressure, temperature and conductivity data (upcast dissolved oxygen data is in general not reliable). With this data set, calibration of the dissolved oxygen data then followed the usual methodology. Note that for many of these stations, near surface CTD dissolved oxygen data were bad (Table 1.12).

A small additional error in CTD dissolved oxygen data is expected to occur from the merging of downcast oxygen data with upcast pressure, temperature and conductivity data - where horizontal gradients occur, there will be some mismatch of downcast and upcast data as the ship drifts during a CTD cast. At most, this error is not expected to exceed ~3%.

The dissolved oxygen residuals are plotted in Figure 1.6. The final standard deviation values are within ~1.2% of full scale values (where full scale is approximately equal to 250  $\mu$ mol/l for pressure > 750 dbar, and 350  $\mu$ mol/l for pressure < 750 dbar). Note that the standard deviation values are a little larger than for previous cruises, indicating a larger spread in the residuals for each station (Figure 1.6). The best calibration was achieved using large values of the order 13.0 for the coefficient  $K_1$  (i.e. oxygen current slope), and large negative values of the order -2.0 for the coefficient  $K_3$  (i.e. oxygen current bias) (Table 1.16). This, however, is not considered relevant to actual data quality.

#### 1.6.1.5 Fluorescence and P.A.R. data

As discussed in section 1.4 above, fluorescence and p.a.r. are effectively uncalibrated. These data should not be used quantitatively other than for linkage with primary productivity data.

**Table 1.7:** Summary of cautions to CTD data quality.

station no.	CTD parameter	caution
1	salinity	test cast - all bottles fired at same depth; salinity accuracy reduced
22	pressure	surface pressure offset estimated from surrounding stations
31	oxygen	dissolved oxygen data could not be calibrated due to bad bottle data
42-44	oxygen	no CTD dissolved oxygen data due to bad conductivity data
45	salinity	most bottles tripped on the fly, which may introduce small inaccuracy
		into the conductivity calibration
104-105	all parameters	data not used for these stations (test casts only)
128	pressure	surface pressure offset estimated from surrounding stations
144	pressure	surface pressure offset estimated manually
168	pressure	surface pressure offset estimated manually
190	pressure	surface pressure offset estimated from surrounding stations
1-29, 45-208	oxygen	no CTD dissolved oxygen data due to faulty hardware
30-41	salinity	additional correction applied for pressure dependent conductivity
		residual
all CTD1103	stns temperature	offset between CTD and reversing thermometer data
all stns f	luorescence/p.a.r.	fluorescence and p.a.r. sensors (where active) are uncalibrated

#### 1.6.1.6 Summary of CTD data creation

stations 1-29 and 42-208: no CTD dissolved oxygen data;

stations 30-44: all CTD data from upcast (except dissolved oxygen); pressure dependent conductivity residual removed;

stations 53-103 and 106-201: all CTD data from upcast;

Further information relevant to the creation of the calibrated CTD data is tabulated, as follows:

- \* Surface pressure offsets calculated for each station are listed in Table 1.8.
- \* CTD conductivity calibration coefficients, including the station groupings used for the conductivity calibration, are listed in Tables 1.9 and 1.10.
- \* CTD raw data scans flagged for special treatment are listed in Table 1.11.
- \* Missing 2 dbar data averages are listed in Table 1.12.
- \* 2 dbar bins which are linearly interpolated from surrounding bins are listed in Table 1.13.
- \* Suspect 2 dbar averages are listed in Tables 1.14 and 1.15.
- \* CTD dissolved oxygen calibration coefficients are listed in Table 1.16. The starting values used for the coefficients prior to iteration, and the coefficients varied during the iteration, are listed in Table 1.17.

- \* Stations containing fluorescence and photosynthetically active radiation data are listed in Table 1.20.
- \* The different protected and unprotected thermometers used for the stations are listed in Table 1.21.
- \* Laboratory calibration coefficients for the CTD's are listed in Table 1.22.

#### 1.6.1.7 Summary of CTD data quality

CTD data quality cautions for the various parameters are summarised in Table 1.7.

#### 1.6.2 Hydrology data

Quality control information relevant to the hydrology data is tabulated, as follows:

- \* Dissolved oxygen Niskin bottle samples flagged with the code -9 (rejected for CTD dissolved oxygen calibration) are listed in Table 1.18.
- \* Questionable nutrient Niskin bottle sample values are listed in Table 1.19. Note that questionable values are included in the hydrology data file, whereas bad values have been removed. Also note that there are no questionable dissolved oxygen bottle samples.

For station 45, the cast was abandoned at ~1000 m above the bottom on the downcast, due to ice bearing down on the ship. During retrieval, bottles at rosette positions 2 to 19 were tripped while the instrument package was still moving.

#### 1.6.2.1 Nutrients

As discussed in previous data reports, additional "dummy" samples drawn from the Niskin bottles were inserted in autoanalyser runs immediately following wash solution vials to artificially mask the suppression effect on subsequent phosphate samples (see section 6.2.1 in Rosenberg et al., 1995b). As a result, no phosphate data was lost.

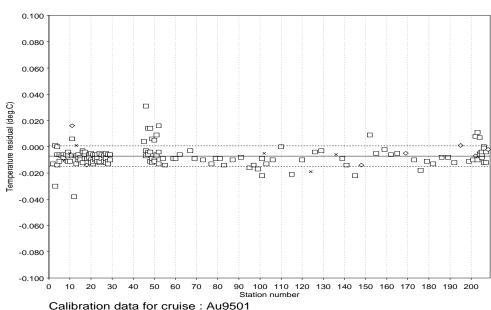
Laboratory temperature on the ship was stable, with lab temperatures at the times of nutrient analyses having a most common value of 18°C.

#### 1.6.2.2 Dissolved oxygen

Dissolved oxygen bottle data for stations 14, 23, 31 and 44 were unusable, as the bottles had not been adequately shaken following the addition of reagents during sampling.

Dissolved oxygen bottle values for stations 1 to 21 are ~6µmol/l smaller than for the remaining stations, due to drift of the laboratory standardisation values for the first 21 stations. See Part 4 of this report for a more detailed discussion.





dubious

rejected

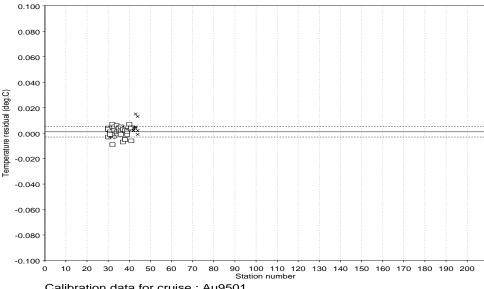
Calibration file: CTD1103.lis

good

Mean offset Temperature = -.00709312c (s.d. = 0.0078 °c)

Number of samples used = 155 out of 161





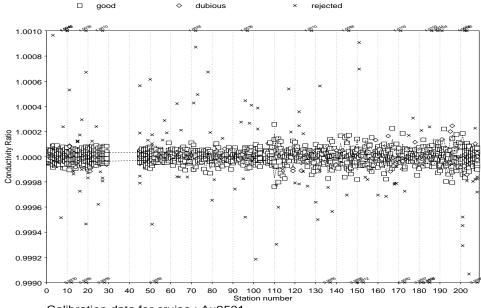
Calibration data for cruise: Au9501

Calibration file: CTD1193.lis

Mean offset Temperature = 0.00106312c (s.d. = 0.0041 °c)

Number of samples used = 33 out of 44

Figure 1.3: Temperature residual (T<sub>therm</sub> - T<sub>cal</sub>) versus station number for cruise au9501 for stations using (a) CTD1103, and (b) CTD 1193. The solid line is the mean of all the residuals; the broken lines are ± the standard deviation of all the residuals (see CTD methodology). Note that the "dubious" and "rejected" categories refer to the conductivity calibration.

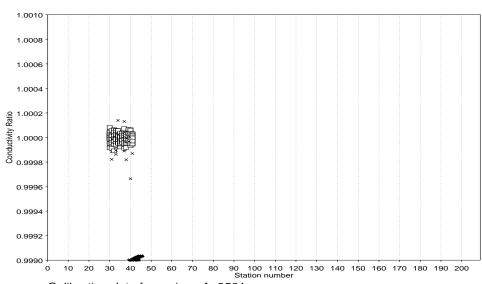


Calibration data for cruise : Au9501 Calibration file : CTD1103.lis

Conductivity s.d. = 0.00005

Number of bottles used = 1731 out of 1911 Mean ratio for all bottles = 1.00000

(b)



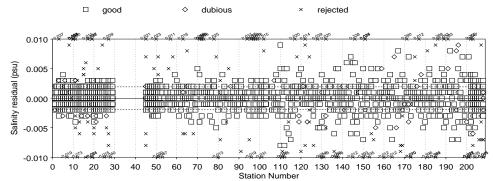
Calibration data for cruise : Au9501 Calibration file : CTD1193.lis

Conductivity s.d. = 0.00003

Number of bottles used = 275 out of 359 Mean ratio for all bottles = 1.00000

Comment:

<u>Figure 1.4:</u> Conductivity ratio  $c_{btl}/c_{cal}$  versus station number for cruise au9501 for stations using (a) CTD1103, and (b) CTD1193. The solid line follows the mean of the residuals for each station; the broken lines are  $\pm$  the standard deviation of the residuals for each station (see CTD methodology).



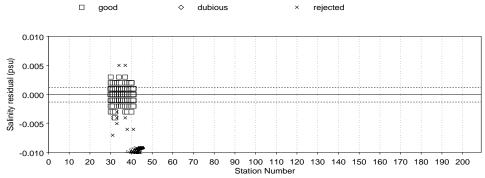
Calibration data for cruise: Au9501

Calibration file: CTD1103.lis

Mean offset salinity = 0.0000psu (s.d. = 0.0019 psu)

Number of bottles used = 1731 out of 1911

(b)



Calibration data for cruise: Au9501

Calibration file: CTD1193.lis

Mean offset salinity = 0.0000psu (s.d. = 0.0013 psu)

Number of bottles used = 275 out of 359

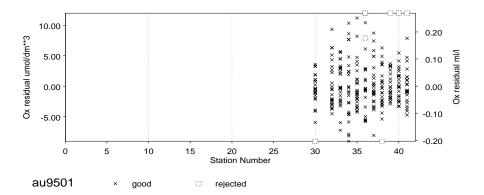
<u>Figure 1.5:</u> Salinity residual ( $s_{btl}$  -  $s_{cal}$ ) versus station number for cruise au9501 for stations using (a) CTD1103, and (b) CTD1193. The solid line is the mean of all the residuals; the broken lines are  $\pm$  the standard deviation of all the residuals (see CTD methodology).

Mean of Residual = -0.023umol/dm\*\*3

S.D. of residual = 3.591umol/dm\*\*3 (Equiv to 0.080ml/l)

Used 252 bottles out of total 358

S.D. deep (>750m) 2.977umol/dm\*\*3 (equiv to 0.067ml/l)



<u>Figure 1.6:</u> Dissolved oxygen residual ( $o_{btl}$  -  $o_{cal}$ ) versus station number for cruise au9501 (CTD1193 stations only).

<u>Table 1.8:</u> Surface pressure offsets (as defined in the CTD methodology). \*\* indicates that value is estimated from surrounding stations, or else determined from manual inspection of pressure data.

station	surface p	station	surface p		surface p	station	surface p
number	offset (dbar)	number		number	offset (dbar)	number	
1	0.99	53	0.13	105	-	157	1.04
2	0.63	54	0.33	106	0.23	158	1.14
3	0.49	55	0.21	107	0.78	159	1.26
4	0.46	56 57	0.14	108	1.21	160	0.95
5	0.50	57 50	-0.23	109	1.13	161	0.85
6	0.28	58 50	-0.24	110	0.78	162	1.04
7	0.18	59 60	0.05	111	1.08	163	0.97
8	0.45	60	-0.16	112	1.12	164 165	0.97
9	0.17 0.42	61 62	0.25 0.29	113 114	0.86	165 166	0.59
10	-0.23	62 63	0.29	114	0.65 1.04	166 167	1.15 0.78
11 12	-0.23 0.22	64	-0.13 -0.14	116	0.97	168	0.78**
13	0.22	65	0.27	117	0.97	169	1.29
14	0.13	66	0.27	117	0.93	170	1.04
15	-0.13 -0.11	67	-0.06	119	0.01	170	1.04
16	0.14	68	0.35	120	1.17	171	0.97
17	-0.01	69	0.33	121	1.17	172	1.14
18	-0.01	70	0.15	121	1.17	173	0.96
19	0.00	71	-0.11	123	1.12	175	0.96
20	-0.22	72	0.26	124	1.09	176	0.71
21	0.00	73	0.33	125	1.06	177	0.98
22	0.00**	74	0.44	126	0.98	178	0.91
23	-0.57	75	0.12	127	1.13	179	0.78
24	0.05	76	0.23	128	1.00**	180	1.17
25	-0.28	77	0.26	129	0.88	181	0.71
26	-0.45	78	0.57	130	0.66	182	0.70
27	-0.29	79	0.48	131	1.03	183	0.87
28	-0.40	80	0.46	132	0.68	184	0.51
29	-0.47	81	0.32	133	0.98	185	0.86
30	-0.69	82	0.31	134	0.67	186	1.40
31	-0.66	83	0.36	135	1.01	187	0.86
32	-1.26	84	0.26	136	0.82	188	0.73
33	-2.29	85	0.09	137	0.98	189	0.69
34	-1.90	86	0.28	138	0.82	190	0.66**
35	-1.30	87	0.12	139	1.03	191	0.63
36	-0.79	88	0.30	140	0.74	192	0.82
37	-1.15	89	0.29	141	0.96	193	0.81
38	-1.21	90	0.12	142	0.99	194	0.93
39	-1.73	91	0.80	143	0.55	195	1.10
40	-0.98	92	0.18	144	0.45**	196	0.65
41	-0.71	93	0.62	145	0.41	197	1.00
42	-1.08	94	0.40	146	0.72	198	0.70
43	-1.26	95	0.26	147	0.53	199	0.60
44	-0.80	96	0.46	148	0.56	200	0.79
45	0.65	97	0.14	149	0.56	201	0.82
46	0.23	98	0.29	150	0.36	202	0.68
47	-0.06	99	0.73	151	0.82	203	0.70
48	0.19	100	0.26	152	1.16	204	0.27
49	0.09	101	0.29	153	0.69	205	0.60
50	-0.02	102	0.46	154	0.56	206	0.70
51	-0.01	103	0.64	155	0.91	207	0.65
52	-0.30	104	-	156	0.94	208	0.52

<u>Table 1.9:</u> CTD conductivity calibration coefficients.  $F_1$ ,  $F_2$  and  $F_3$  are respectively conductivity bias, slope and station-dependent correction calibration terms. n is the number of samples retained for calibration in each station grouping;  $\sigma$  is the standard deviation of the conductivity residual for the n samples in the station grouping (see CTD methodology);  $\sigma$  is the correction applied to CTD conductivities due to pressure dependence of the conductivity residuals for stations 30 to 41 (eqn 1.1).

10014441010		(oq.: <i>)</i> .	_			
stn grouping	·	<b>F</b> <sub>2</sub>	F <sub>3</sub>	n	σ	α
001 to 003	15532800	0.10106622E-02	11470793E-08	43	0.001506	
004 to 006	12422183	0.10097721E-02	22838255E-07		0.001231	
007 to 011	11687464	0.10094945E-02	12108803E-07		0.001224	
012 to 013	10839249	0.10098253E-02	56286375E-07		0.001083	
014 to 017	10910666	0.10089800E-02	0.85821839E-08		0.001106	
018 to 024	10605356	0.10089344E-02	0.58253139E-08	152	0.001306	
025 to 026	11794039	0.10094659E-02	15959792E-08	43	0.001174	
027 to 029	11923390	0.10095053E-02	73952908E-09	65	0.000989	
030 to 032	84092238E-01	0.94275256E-03	0.65573267E-08	70	0.001063	1.207501E-06
033 to 037	83614084E-01	0.94281093E-03	0.34424272E-08	114	0.000946	1.239768E-06
038 to 041	84436830E-01	0.94285378E-03	0.28708290E-08	91	0.000948	1.321621E-06
042 to 044	-	-	-	-	-	-
045 to 047	50710766E-01	0.10080721E-02	17528905E-07	66	0.000900	
048 to 050	55259689E-01	0.10074674E-02	12693342E-09		0.001153	
051 to 052	51316066E-01	0.10065250E-02	0.14941010E-07		0.000960	
053 to 056	42571330E-01	0.10096393E-02	47862704E-07		0.000847	
057 to 061	46105712E-01	0.10066443E-02	0.76930518E-08		0.001093	
062 to 068	36372532E-01	0.10063733E-02	0.69886140E-08		0.001138	
069 to 071	56595171E-01	0.10105745E-02	42261552E-07		0.001753	
072 to 074	43002639E-01	0.10087385E-02	23044300E-07	15		
075 to 083	46658731E-01	0.10067303E 02 0.10068495E-02	0.30955746E-08	48	0.001327	
084 to 086	42416890E-01	0.10000493E-02 0.10070047E-02	50938148E-09		0.001327	
087 to 089		0.10070047E-02 0.10082777E-02	19533903E-07		0.000626	
	31545437E-01					
090 to 092	28704235E-01	0.10077391E-02	13458843E-07		0.000965	
093 to 094	49118959E-01	0.10094562E-02	23536990E-07	11		
095 to 097	62152866E-01	0.10025474E-02	0.53099831E-07	14		
098 to 101	14314088E-01	0.10047888E-02	0.12315666E-07		0.001345	
102 to 103	34956256E-01	0.10099761E-02	31950269E-07	22	0.001035	
104 to 105	-	-	-		-	
106 to 107	23593039E-01	0.10371770E-02	28856875E-06	11	0.001335	
108 to 109	19791365E-01	0.10130541E-02	63060262E-07		0.001446	
110 to 112	49023601E-01	0.10131578E-02	53759663E-07		0.003549	
113 to 129	40135147E-01	0.10069183E-02	85806002E-09		0.001647	
130 to 132	85296545E-02	0.10054166E-02	0.27726516E-08		0.001904	
133 to 134	25781684E-01	0.10052848E-02	0.71546988E-08		0.001136	
135 to 137	42318480E-01	0.10019220E-02	0.34902679E-07		0.002036	
138 to 140	14699730E-01	0.10035095E-02	0.14410654E-07		0.001514	
141 to 144	19358440E-01	0.10084928E-02	19248580E-07		0.001984	
145 to 148	28011470E-01	0.10051157E-02	0.68803976E-08		0.002432	
149 to 151	0.25657995E-01	0.10022988E-02	0.11828427E-07	14	0.002039	
152 to 153	45270083E-01	0.98897546E-03	0.11541208E-06	11	0.001242	
154 to 162	31067531E-01	0.10055354E-02	0.36686988E-10	51	0.001819	
163 to 167	34521659E-01	0.10018974E-02	0.23188345E-07	29	0.002383	
168 to 171	38682948E-01	0.10051592E-02	0.46065747E-08	19	0.001338	
172 to 174	38558169E-01	0.10161118E-02	58916707E-07	14	0.002094	
175 to 177	38509621E-01	0.10074843E-02	87849944E-08	14	0.000734	
178 to 180	55547340E-01	0.10069200E-02	19492192E-08	18	0.001820	
181 to 183	33533182E-01	0.99319718E-03	0.69701424E-07	16		
184 to 188	30982703E-01	0.10032052E-02	0.14044956E-07	26	0.001601	
189 to 191	15491941E-01	0.99199340E-03	0.69487626E-07	16	0.002096	
192 to 195	28909825E-01	0.10034465E-02	0.11624303E-07		0.002599	
196 to 197	0.21113085E-01	0.99194842E-03	0.61703687E-07		0.003203	
198 to 201	28802603E-01	0.10147873E-02	44840249E-07		0.002606	
202 to 204	73871355E-01	0.10032132E-02	0.20954622E-07	68	0.001897	
205 to 208	10645228	0.10052152E 02 0.10152894E-02	31595576E-07	78		
200 10 200	.100-10220	5.10102034L-02	.01000010L-01	70	0.001000	

<u>Table 1.10:</u> Station-dependent-corrected conductivity slope term ( $F_2 + F_3$ . N), for station number N, and  $F_2$  and  $F_3$  the conductivity slope and station-dependent correction calibration terms respectively. stn  $(F_2 + F_3. N)$  stn  $(F_2 + F_3. N)$  stn  $(F_2 + F_3. N)$  stn  $(F_2 + F_3. N)$ 

term	s respectively.						
stn	$(F_2 + F_3 . N)$	stn	$(F_2 + F_3 . N)$	stn	$(F_2 + F_3 . N)$	stn	$(F_2 + F_3 . N)$
no.		no.		no.	no	).	
1	0.10106610E-02	53	0.10071026E-02	105	-	157	0.10055412E-02
2	0.10106599E-02	54	0.10070547E-02	106	0.10065887E-02	158	0.10055412E-02
3	0.10106587E-02	55	0.10070069E-02	107	0.10063001E-02	159	0.10055412E-02
4	0.10096808E-02	56	0.10069590E-02	108	0.10062436E-02	160	0.10055413E-02
5	0.10096579E-02	57	0.10070828E-02	109	0.10062436E-02	161	0.10055413E-02
6	0.10096351E-02	58	0.10070925E-02	110	0.10072443E-02	162	0.10055413E-02
7	0.10090331E-02 0.10094098E-02	59	0.10070903E-02 0.10070982E-02	111	0.10072443E-02 0.10071905E-02	163	0.10055415E-02 0.10056771E-02
8	0.10094090E-02 0.10093977E-02	60	0.10070902E-02 0.10071059E-02	112	0.10071368E-02	164	0.10057771E-02 0.10057003E-02
9	0.10093977E-02 0.10093856E-02	61	0.10071039E-02 0.10071136E-02	113	0.10071306E-02 0.10068213E-02	165	0.10057005E-02 0.10057235E-02
10	0.10093030E-02 0.10093735E-02	62	0.10071130E-02 0.10068066E-02	114	0.10068205E-02	166	0.10057253E-02 0.10057467E-02
11	0.10093733E-02 0.10093613E-02	63	0.10068066E-02	115	0.10068196E-02	167	0.10057407E-02 0.10057699E-02
12	0.10093613E-02 0.10091499E-02	64		116	0.10068196E-02	168	0.10057699E-02 0.10059331E-02
			0.10068205E-02				
13	0.10090936E-02	65	0.10068275E-02	117	0.10068179E-02	169	0.10059377E-02
14	0.10091001E-02	66	0.10068345E-02	118	0.10068170E-02	170	0.10059423E-02
15	0.10091087E-02	67	0.10068415E-02	119	0.10068162E-02	171	0.10059469E-02
16	0.10091173E-02	68	0.10068485E-02	120	0.10068153E-02	172	0.10059781E-02
17	0.10091259E-02	69	0.10076584E-02	121	0.10068145E-02	173	0.10059192E-02
18	0.10090393E-02	70	0.10076162E-02	122	0.10068136E-02	174	0.10058603E-02
19	0.10090451E-02	71	0.10075739E-02	123	0.10068127E-02	175	0.10059469E-02
20	0.10090510E-02	72	0.10070793E-02	124	0.10068119E-02	176	0.10059381E-02
21	0.10090568E-02	73	0.10070563E-02	125	0.10068110E-02	177	0.10059294E-02
22	0.10090626E-02	74	0.10070333E-02	126	0.10068102E-02	178	0.10065731E-02
23	0.10090684E-02	75	0.10070817E-02	127	0.10068093E-02	179	0.10065711E-02
24	0.10090743E-02	76	0.10070848E-02	128	0.10068085E-02	180	0.10065692E-02
25	0.10094260E-02	77	0.10070879E-02	129	0.10068076E-02	181	0.10058131E-02
26	0.10094244E-02	78	0.10070910E-02	130	0.10057770E-02	182	0.10058828E-02
27	0.10094854E-02	79	0.10070941E-02	131	0.10057798E-02	183	0.10059525E-02
28	0.10094846E-02	80	0.10070972E-02	132	0.10057826E-02	184	0.10057895E-02
29	0.10094839E-02	81	0.10071003E-02	133	0.10062364E-02	185	0.10058036E-02
30	0.94294928E-03	82	0.10071034E-02	134	0.10062436E-02	186	0.10058176E-02
31	0.94295584E-03	83	0.10071065E-02	135	0.10066339E-02	187	0.10058317E-02
32	0.94296239E-03	84	0.10069620E-02	136	0.10066688E-02	188	0.10058457E-02
33	0.94292453E-03	85	0.10069614E-02	137	0.10067037E-02	189	0.10051266E-02
34	0.94292798E-03	86	0.10069609E-02	138	0.10054981E-02	190	0.10051960E-02
35	0.94293142E-03	87	0.10065783E-02	139	0.10055126E-02	191	0.10052655E-02
36	0.94293486E-03	88	0.10065588E-02	140	0.10055270E-02	192	0.10056784E-02
37	0.94293830E-03	89	0.10065392E-02	141	0.10057787E-02	193	0.10056900E-02
38	0.94296287E-03	90	0.10065278E-02	142	0.10057595E-02	194	0.10057016E-02
39	0.94296574E-03	91	0.10065143E-02	143	0.10057402E-02	195	0.10057133E-02
40	0.94296861E-03	92	0.10065008E-02	144	0.10057210E-02	196	0.10040423E-02
41	0.94297148E-03	93	0.10072673E-02	145	0.10061134E-02	197	0.10041040E-02
42	-	94	0.10072437E-02	146	0.10061203E-02	198	0.10059090E-02
43	-	95	0.10075919E-02	147	0.10061271E-02	199	0.10058641E-02
44	-	96	0.10076450E-02	148	0.10061340E-02	200	0.10058193E-02
45	0.10072833E-02	97	0.10076981E-02	149	0.10040612E-02	201	0.10057744E-02
46	0.10072658E-02	98	0.10059957E-02	150	0.10040730E-02	202	0.10074460E-02
47	0.10072483E-02	99	0.10060080E-02	151	0.10040849E-02	203	0.10074670E-02
48	0.10074613E-02	100	0.10060203E-02	152	0.10065181E-02	204	0.10074879E-02
49	0.10074612E-02	101	0.10060327E-02	153	0.10066335E-02	205	0.10088123E-02
50	0.10074611E-02	102	0.10067172E-02	154	0.10055411E-02	206	0.10087808E-02
51	0.10072870E-02	103	0.10066853E-02	155	0.10055411E-02	207	0.10087492E-02
52	0.10073019E-02	104	-	156	0.10055411E-02	208	0.10087176E-02

<u>Table 1.11:</u> CTD raw data scans, mostly in the vicinity of artificial density inversions, flagged for special treatment. Note that the pressure listed is approximate only; possible actions taken are either to ignore the raw data scans for all further calculations, or to apply a linear interpolation over the region of the bad data scans. Causes of bad data, listed in the last column, are detailed in the CTD methodology. For the raw scan number ranges, the lowest and highest scan numbers are not included in the ignore or interpolate actions.

station	approximate	raw scan	action	reason
number	pressure (dbar)	numbers	taken	
11	829	48358-48395	ignore	fouling of cond. cell
16	612	47637-47757	ignore	fouling of cond. cell
19	1850	75468-75585	ignore	fouling of cond. cell
23	206	16580-16738	ignore	wake effect
27	3030	126764-126858	ignore	fouling of cond. cell
49	234	21892-21901	ignore	fouling of cond. cell
68	458	19625-19640	ignore	fouling of cond. cell
81	20	43646-43867	ignore	fouling of cond. cell
100	12	33403-33449	ignore	fouling of cond. cell
204	186	13007-13104	ignore	wake effect
208	2468	100929-100979	ignore	fouling of cond. cell

<u>Table 1.12:</u> Missing data points in 2 dbar-averaged files. "1" indicates missing data for the indicated parameters: T=temperature; S=salinity,  $\sigma_T$ , specific volume anomaly and geopotential anomaly; O=dissolved oxygen; PAR=photosynthetically active radiation; F=fluorescence. Note that jmin is the minimum number of data points required in a 2 dbar bin to form the 2 dbar average (see CTD methodology).

station	pressures (dbar)				- 377-		reason
number	where data missing	Т	S	0	PAR	F	
7	1202	1	1		1		no. of data pts in 2 dbar bin < jmin
16	612	1	1		1		fouling of cond. cell
16	804	1	1		1		no. of data pts in 2 dbar bin < jmin
22	2-26	1	1		1		CTD data logging started at 27 dbar
30	2022, 2844	1	1		1		no. of data pts in 2 dbar bin < jmin
30	2-68			1			bad oxygen data
31	entire profile			1			no bottle data for calibration
32	310	1	1		1		no. of data pts in 2 dbar bin < jmin
33	3638	1	1		1		no. of data pts in 2 dbar bin < jmin
34	322	1	1		1		no. of data pts in 2 dbar bin < jmin
35	14-48			1			bad oxygen data
36	2-26			1			bad oxygen data
37	2324,2686,2974,4182	1	1		1		no. of data pts in 2 dbar bin < jmin
37	2-22,76			1			bad oxygen data
38	2-28			1			bad oxygen data
39	130, 1934	1	1		1		no. of data pts in 2 dbar bin < jmin
39	12-28			1			bad oxygen data
40	244	1	1		1		no. of data pts in 2 dbar bin < jmin
40	18-34			1			bad oxygen data
41	10-28			1			bad oxygen data
42-44	entire profile		1	1			bad conductivity data
43	4466	1	1		1		no. of data pts in 2 dbar bin < jmin
104	entire profile	1	1	1			data not used
105	entire profile	1	1	1			data not used
206	672	1	1				no. of data pts in 2 dbar bin < jmin
1-29	entire profile			1			faulty oxygen sensor hardware
45-103	entire profile			1			faulty oxygen sensor hardware
106-208	entire profile			1			faulty oxygen sensor hardware
51-208	entire profile				1		PAR sensor not installed
5-208	entire profile					1	fluorometer not installed

<u>Table 1.13:</u> 2 dbar averages interpolated from surrounding 2 dbar values, for the indicated paramaters: T=temperature; S=salinity,  $\sigma_T$ , specific volume anomaly and geopotential anomaly; O=dissolved oxygen; PAR=photosynthetically active radiation.

station	interpolated	parameters
number	2 dbar values	interpolated
19	1782, 1850	T, S, PAR
27	3032	T, S, PAR
30	560,608,1122	T, S, PAR
31	3076	T, S, PAR
32	300,440,882,902,2260,2454,3064	T, S, PAR
33	666,856,900	T, S, PAR
34	544	T, S, PAR
35	1466,2072,2960	T, S, PAR
36	1672, 4048	T, S, PAR
37	570,1774,2164	T, S, PAR
38	1428	T, S, PAR
39	948,1380,1526,1566	T, S, PAR
40	676,1926,3196	T, S, PAR
41	4036	T, S, PAR
81	18, 20	T, S
204	2042	T, S
205	1784	T, S

<u>Table 1.14a:</u> Suspect 2 dbar averages. Note: for suspect salinity values, the following are also suspect:  $\sigma_T$ , specific volume anomaly, and geopotential anomaly.

station	suspect 2 d	lbar values (dbar)	reason
number	bad	questionable	
Suspect salinity	values		
2	142	-	salinity spike due to wake effect
13	-	304	salinity spike in steep local gradient
14	-	328-330	salinity spike in steep local gradient
16	-	386-388	salinity spike in steep local gradient
19	-	266-268	salinity spike in steep local gradient

<u>Table 1.14b:</u> Suspect 2 dbar-averaged data from near the surface (applies to all parameters other than dissolved oxygen, except where noted).

stn	suspect	2dbar values(db	ar)	stn s	stn suspect 2dbar values(dbar)				
no.	bad	questionable	comment	no.	bad	questionable	comment		
1	2,4	-	-	48-49	2,4,6	-	-		
2	2	-	-	50-52	2,4	-	-		
3-7	2,4	-	-	72	-	2	temperature ok		
8	2,4,6	-	-	84	-	2	temperature ok		
9-12	2,4	-	-	85	-	6	temperature ok		
13	2	-	-	100	6-12	-	temperature ok		
14-15	2,4	-	-	115	-	2,4	temperature ok		
16-19	2	-	-	116	-	2	temperature ok		
20	2,4	-	-	123	-	2,4,8	temperature ok		
21	2	-	-	153	-	18	temperature ok		
23	2,4,6	-	-	172	-	10	temperature ok		
24	2,4	-	-	200	-	2	temperature ok		
25	2	-	-	201	-	2	temperature ok		
26	2,4	-	-	202	2	4	-		
27-28	2	-	-	203	2,4	6,8	-		
29	2,4	-	-	204	2	4	-		
45	2,4,6	-	-	205	2	-	-		
46-47	2,4	-	-	206-20	7 2	4	-		

Table 1.15: Suspect 2 dbar-averaged dissolved oxygen data.

 stn
 suspect 2dbar values(dbar)

 no.
 bad
 questionable

 32
 2, 14-28

 34
 2-22

 38
 3906-4044

<u>Table 1.16:</u> CTD dissolved oxygen calibration coefficients.  $K_1$ ,  $K_2$ ,  $K_3$ ,  $K_4$ ,  $K_5$  and  $K_6$  are respectively oxygen current slope, oxygen sensor time constant, oxygen current bias, temperature correction term, weighting factor, and pressure correction term. dox is equal to 2.8 $\sigma$  (for  $\sigma$  as defined by eqn A2.24 in the CTD methodology); n is the number of samples retained for calibration in each station or station grouping.

station	$K_1$	$K_2$	$K_3$	$K_4$	$K_5$	$K_6$	dox	n
number								
30	12.057	5.0000	-1.570	-0.16340	0.67515	0.16214E-03	0.1552	5 22
32	13.933	5.0000	-1.999	-0.19355	0.78517	0.93553E-04	0.2432	1 24
33	10.938	5.0000	-1.510	-0.14316	0.12891	0.33452E-04	0.2198	9 24
34	13.713	5.0000	-2.051	-0.14829	0.91995	0.11928E-03	0.3483	8 24
35	14.503	5.0000	-1.990	-0.24202	0.69512	0.74484E-04	0.2441	9 24
36	24.416	5.0000	-3.394	-0.42081	0.81637	0.75967E-04	0.2890	2 20
37	12.645	5.0000	-1.703	-0.20725	0.56959	0.58486E-04	0.2503	6 24
38	12.389	5.0000	-1.872	-0.11335	0.60504	0.11011E-03	0.1955	3 23
39	12.977	8.0000	-1.700	-0.23495	0.69338	0.64992E-04	0.1382	4 22
40	16.556	5.0000	-2.359	-0.26428	0.82111	0.92212E-04	0.1617	3 22
41	12.979	5.0000	-1.746	-0.21918	0.71336	0.97135E-04	0.1893	1 23

<u>Table 1.17:</u> Starting values for CTD dissolved oxygen calibration coefficients prior to iteration, and coefficients varied during iteration (see CTD methodology). Note that coefficients not varied during iteration are held constant at the starting value.

vailou c	ranoa dannig korakion aro nola conokant at the otal ting value.									
station	$K_1$	$K_2$	$K_3$	$K_{4}$	$K_5$	$K_6$	coef	ficients		
numbe	r						varie	d		
30	12.0500	5.0000	-1.300	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$		
32	11.5000	5.0000	-1.440	-0.500E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$		
33	11.6000	5.0000	-1.600	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$		
34	12.4000	5.0000	-1.450	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$		
35	12.7000	5.0000	-1.650	-0.400E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$		
36	10.8000	5.0000	-0.400	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$		
37	12.7500	5.0000	-1.650	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$		
38	12.6500	5.0000	-1.700	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$		
39	12.4300	8.0000	-1.650	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$		
40	14.1000	5.0000	-1.650	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$		
41	12.6000	5.0000	-1.650	-0.500E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$		

<u>Table 1.18:</u> Dissolved oxygen Niskin bottle samples flagged as -9 for dissolved oxygen calibration. Note that this does not necessarily indicate a bad bottle sample - in many cases, flagging is due to bad CTD dissolved oxygen data.

station	rosette
number	position
30	24,23
36	23,19,18,17
38	24
39	20
40	23,20
41	21

<u>Table 1.19:</u> Questionable nutrient sample values (not deleted from hydrology data file).

PHOSPHATE		NITR	RATE	SILICATE		
station	rosette	station	rosette	station	rosette	
number	position	number	position	number	position	
5	13	5	13			
8	1,2					
9	1,5,7	9	1,5,7			
27	11,13					
29	2,17	29	2,17	29	2	
		44	13			
45	whole stn					
46	whole stn					

# <u>Table 1.20:</u> Stations containing fluorescence (fl) and photosynthetically active radiation (par) 2 dbar-averaged data.

stations with fl data stations with par data

1 to 4 1 to 50

# <u>Table 1.21:</u> Protected and unprotected reversing thermometers used (serial numbers are listed).

protected thermometers

station	rosette position 24	rosette position 12	rosette position 2
numbers	thermometers	thermometers	thermometers
1 to 52	12095,12096	12094	12119,12120
53 to 100	-	-	12119,12120
101-105	-	12095,12096	12119,12120
100 to 128	-	-	12119,12120
129 to 201	-	-	12119,12094
202 to 208	12095,12096	12094	12119,12120

#### unprotected thermometers

4,6 6.0 6.0 4. 466		
station	rosette position 12	rosette position 2
numbers	thermometers	thermometers
1 to 52	11992	11993
53 to 100	-	11993
101-105	-	11993
100 to 128	-	11993
129 to 201	-	11993
202 to 208	11992	11993

<u>Table 1.22:</u> Calibration coefficients and calibration dates for CTD serial numbers 1103 and 1193 (unit nos 7 and 5 respectively) used during RSV Aurora Australis cruise AU9501. Note that an additional pressure bias term due to the station dependent surface pressure offset exists for each station (eqn A2.1 in the CTD methodology). Also note that platinum temperature calibrations are for the ITS-90 scale.

•	CTD serial 11	03 (unit no. 7)	CTD serial 1	193 (unit no. 5)
	coefficient	value of coefficient	coefficient	value of coefficient
pressu	ıre calibration co	pefficients	pressure calibration	coefficients
CSIR	O Calibration Fa	cility - 08/11/1995	CSIRO Calibration F	acility - 09/11/1995
	pcal0	-2.065725e+01	pcal0	-8.810839
	pcal1	1.002878e-01	pcal1	1.007713e-01
	pcal2	4.951104e-09	pcal2	1.985674e-09
	pcal3	4.500981e-14	pcal3	-1.521121e-14
	pcal4	-4.514384e-19	pcal4	0.0
platinu	ım temperature	calibration coefficients	platinum temperature	e calibration coefficients
		cility - 26/09/1995	CSIRO Calibration F	
	Tcal0	0.23396e-01	Tcal0	-0.20560e-01
	Tcal1	0.49983e-03	Tcal1	0.49936e-03
	Tcal2	0.35049e-11	Tcal2	0.27541e-11
pressu	ıre temperature	calibration coefficients	pressure temperature	e calibration coefficients
CSIR	O Calibration Fa	cility - 08/11/1995	CSIRO Calibration F	acility - 09/11/1995
	Tpcal0	1.695615e+02	Tpcal0	1.167581e+02
	Tpcal1	-3.240390e-03	Tpcal1	-2.450758e-03
	Tpcal2	0.0	Tpcal2	0.0
	Tpcal3	0.0	Tpcal3	0.0
coeffic	cients for temper	rature correction to coeffic	cients for temperature o	correction to
press			pressure	
CSIR	O Calibration Fa	cility - 08/11/1995	CSIRO Calibration F	
	$T_0$	20.00	$T_o$	20.00
	S <sub>1</sub>	-1.319844e-05	$S_1$	-1.474830e-05
	$S_2$	-3.465273e-02	$S_2$	-7.847037e-02
prelim	inary polynomia	nl coefficients applied to i	fluorescence (fl) (Antar	ctic Division, January 1996) and
		ive radiation (par) (suppli		
-	f0	-1.115084e+01	,	-

f1

f2

par0

par1

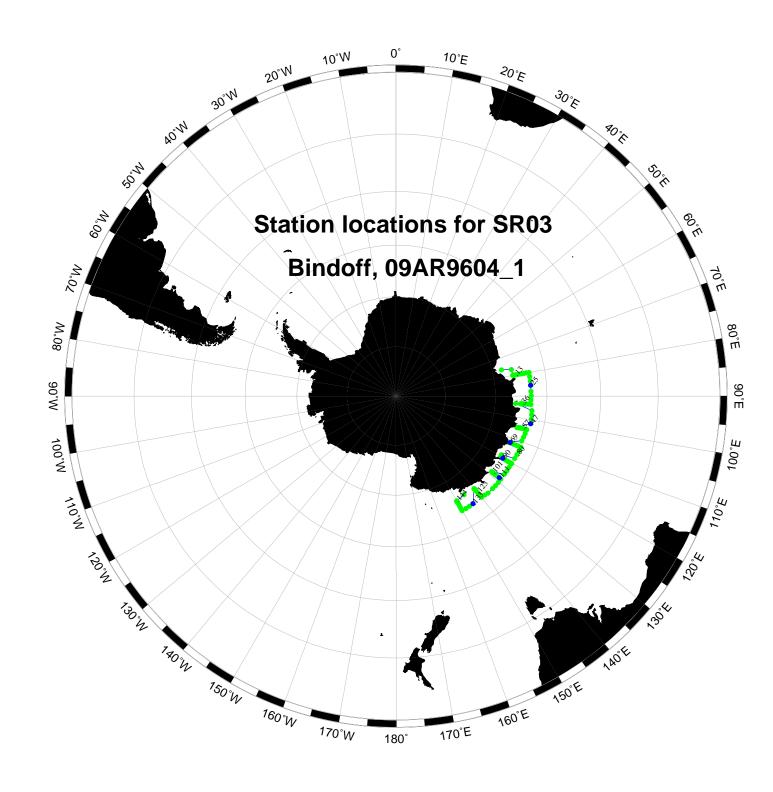
par2

3.402400e-04

1.373290e-04 -3.452156e-23

0.0

-4.499860



# Part 2 Aurora Australis Marine Science Cruise AU9604 - Oceanographic Field Measurements and Analysis

#### **ABSTRACT**

Oceanographic measurements were conducted along a series of meridional and zonal sections along the Antarctic continental shelf and slope region between 80 and 150°E, from January to March 1996. A total of 147 CTD vertical profile stations were taken, most to near bottom. Over 2450 Niskin bottle water samples were collected for the measurement of salinity, dissolved oxygen, nutrients, chlorofluorocarbons, oxygen 18, primary productivity, and biological parameters, using a 24 bottle rosette sampler. Near surface current data were collected using a ship mounted ADCP. Measurement and data processing techniques are summarised, and a summary of the data is presented in graphical and tabular form.

#### 2.1 INTRODUCTION

Marine science cruise AU9604, the fifth oceanographic cruise of the Cooperative Research Centre for the Antarctic and Southern Ocean Environment (Antarctic CRC), was conducted aboard the Australian Antarctic Division vessel RSV Aurora Australis from January to March 1996. The major constituent of the cruise was a joint oceanographic and biological survey along the continental shelf and slope region of Antarctica between 80 and 150°E (Figure 2.1). The primary objectives of the oceanographic survey, named MARGINEX (Antarctic Margin Experiment), were:

- 1. to estimate the rate of formation of surface and Antarctic Bottom Water masses;
- 2. to define the evolution and modification of Antarctic water masses along the shelf and slope in the experimental region;
- 3. to estimate the relative importance of air-sea interaction and advection of surface and deep waters on property changes in the major water masses.

The biology program comprised of a hydroacoustic survey of krill population in the region, to enable setting of catch limits (principal investigator Steve Nicol, Australian Antarctic Division). The linked oceanography-biology objective was to determine the relationship between the distribution and production of marine biota and the physical and biogeochemical conditions along the Antarctic shelf break.

Two bottom-mounted pressure recorders (principal investigators Tom Whitworth, University of Texas A&M, and Dale Pillsbury, Oregon State University) were successfully recovered from the northern and southern ends of the WOCE SR3 meridional section. A current meter mooring (principal investigator Ted Foster, University of Delaware) was also recovered from the eastern end of the MARGINEX study region. Two upward looking sonar moorings (principal investigator Ian Allison, Australian Antarctic Division) were deployed in the vicinity of Davis (Figure 2.1). Eight drifting buoys were also deployed throughout the voyage.

This report describes the collection of oceanographic data from MARGINEX, and summarises the chemical analysis and data processing methods employed. All information required for use of the data set is presented in tabular and graphical form.

#### 2.2 CRUISE ITINERARY

In early January 1996, prior to the cruise proper, marine trials were conducted from the Aurora Australis at Port Arthur, and south of Maatsuyker Island. A shallow CTD cast was taken at Port Arthur for calibration of the hydroacoustic equipment, and a deep cast was taken south of Tasmania for testing of CTD instrumentation. At the northern end of the SR3 section, an unsuccessful attempt was made to recover the pressure recorder mooring designated Hobart91b (Table 2.4). The pressure recorder mooring designated Hobart94 was successfully recovered from the same approximate location, and the mooring Hobart96 was deployed as a replacement.

The first CTD cast on the cruise proper was taken en route to Davis, to test CTD equipment and measure Niskin bottle CFC blank levels. Following cargo operations at Davis, the two upward looking sonar moorings were deployed, with a CTD cast taken at both mooring locations. CTD legs 1 and 4 were completed, with leg 4 finishing at station 42 near the edge of the Shackleton Ice Shelf. A speculative CTD cast was taken at station 43 to investigate possible ice crystal formation in water flowing over a sill (T. Pauly, pers. comm.). CTD legs 6 and 7 were then completed. After leg 7, a search was made of the old ULS mooring site SONEAR (Bush, 1994). Note that this was the third and final search for SONEAR. The mooring could not be located, so the ship proceeded to Casey for cargo operations.

At Casey, a shallow CTD cast (station 65) was taken for calibration of the hydroacoustic equipment in cold water. After Casey, the remaining CTD legs 9, 11, 13, 16 and 18 were completed. Leg 16 was interrupted briefly for pressure recorder mooring work: the mooring Dumont94 was successfully recovered, and the mooring Dumont96 was deployed as a replacement (Table 2.4).

Note that the southern end of all the meridional CTD sections were closed on the shelf or at the shelf break, with the exception of leg 18 - this leg had to be terminated early at a depth of ~2100 m on the continental slope, due to thickening sea ice conditions.

After completion of MARGINEX, grappling operations commenced to attempt recovery of 3 current meter moorings (Table 2.4). The mooring CM2 was recovered, and a CTD cast (station 145) was taken at the mooring location. Moorings CM1 and CM3 were not found. Two final shallow CTD casts were taken to attempt to sample shuga ice for biological analysis. The ship then proceeded to Macquarie Island for cargo operations, then returned to Hobart.

#### Table 2.1: Summary of cruise itinerary.

Expedition Designation
Cruise AU9604 (cruise acronym BROKE), encompassing MARGINEX

Chief Scientists
Nathan Bindoff, Antarctic CRC
Steve Nicol, Antarctic Division

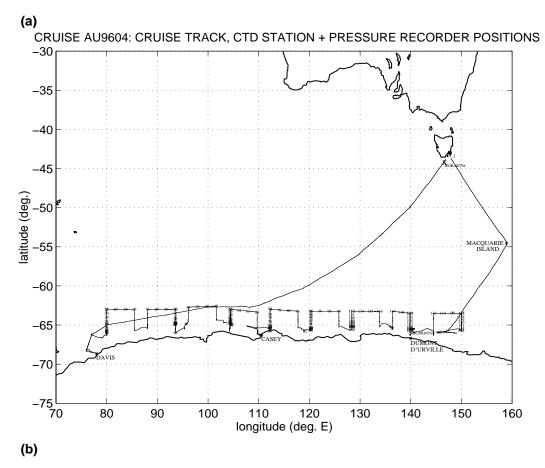
Ship RSV Aurora Australis

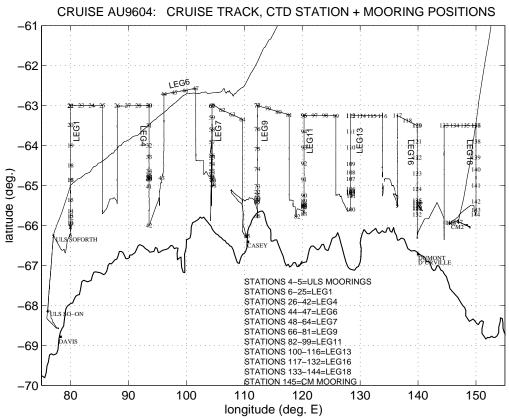
Ports of Call

Davis Casey Macquarie Island

Cruise Dates

January 19 to March 31 1996





<u>Figure 2.1a and b:</u> Cruise track, CTD station and mooring positions for RSV Aurora Australis cruise AU9604. Note that positions for pressure recorders are for recovered moorings only.

#### 2.3 CRUISE SUMMARY

#### 2.3.1 CTD casts and water samples

In the course of the cruise, 147 CTD casts were completed, 138 of which were along the MARGINEX study region (Figures 2.1a and b), with most casts reaching to within 20 m of the sea floor (Table 2.2). 8 meridional CTD sections and 9 shorter approximately zonal CTD sections were completed, providing closure for 7 different study areas (Figure 2.1b). Over 2450 Niskin bottle water samples were collected for the measurement of salinity, dissolved oxygen, nutrients (orthophosphate, nitrate plus nitrite, and reactive silicate), chlorofluorocarbons, oxygen 18, primary productivity, and biological parameters, using a 24 bottle rosette sampler. Table 2.3 provides a summary of samples drawn at each station. Principal investigators for the various water sampling programmes are listed in Table 2.6a. For all stations, the different samples were drawn in a fixed sequence (see previous data reports).

Table 2.2 (following 5 pages): Summary of station information for RSV Aurora Australis cruise AU9604. The information shown includes time, date, position and ocean depth for the start of the cast, at the bottom of the cast, and for the end of the cast. The maximum pressure reached for each cast, and the altimeter reading at the bottom of each cast (i.e. elevation above the sea bed) are also included. Missing ocean depth values are due to noise from the ship's bow thrusters interfering with the echo sounder. For casts which do not reach to within 100 m of the bed (i.e. the altimeter range), or for which the altimeter was not functioning, there is no altimeter value. For station names, LEGx is the MARGINEX CTD leg number (Figure 2.1b), TEST is a test cast, CAL is a cast for calibration of the hydroacoustic equipment, ULS is an upward looking sonar mooring site, CM is a current meter mooring site, and BIO is a speculative dip for biological analyses. Note that all times are UTC (i.e. GMT). CTD unit 7 (serial no. 1103) was used for stations 3 to 144; CTD unit 5 (serial no. 1193) was used for stations 1 to 2, and 145 to 147.

station	START		maxP		BOT	ТОМ				EN	D	
number	time date latitude lon	ngitude depth(m)	(dbar)	time	latitude	longitude d	epth(m)	altimeter	time	latitude	longitude (	depth(m)
1 CAL	0604 5-JAN-96 43:08.34S 14	7:52.26E 27	26	0610	43:08.34S	147:52.26E	-	8.1	0619	43:08.34S	147:52.26E	-
2 TEST	1436 5-JAN-96 43:26.20S 14	8:35.20E 3635	3552	1605	43:27.10S	148:34.75E	-	21.9	1711	43:28.00S	148:34.23E	3604
3 TEST	2112 20-JAN-96 49:54.55S 13	9:49.87E 3737	3924	2252	49:55.30S	139:50.70E	-	32.9	0006	49:55.74S	139:51.17E	-
4 ULS	2002 28-JAN-96 68:08.32S 76	6:02.67E 484	472	2014	68:08.38S	76:02.51E	479	12.6	2037	68:08.43S	76:01.96E	483
5 ULS	1059 29-JAN-96 66:15.50S 77	7:03.37E 2918	404	1118	66:15.51S	77:03.40E	-	-	1137	66:15.51S	77:03.41E	-
6 LEG1	0331 30-JAN-96 66:14.12S 80	0:00.21E 396	382	0400	66:14.21S	79:59.71E	-	9.5	0444	66:14.33S	79:58.92E	398
7 LEG1	0624 30-JAN-96 66:06.79S 79	9:59.50E 644	624	0653	66:06.89S	79:58.81E	638	9.7	0737	66:06.87S	79:57.87E	638
8 LEG1	1024 30-JAN-96 66:01.90S 79	9:59.94E 890	874	1058	66:01.98S	80:00.29E	870	2.5	1147	66:01.86S	80:00.16E	900
9 LEG1	1316 30-JAN-96 66:00.86S 79	9:59.92E 1208	1206	1407	66:00.60S	79:59.82E	1249	14.7	1516	66:00.25S	79:58.89E	1229
10 LEG1	1640 30-JAN-96 65:56.72S 79	9:59.60E 1668	1656	1731	65:56.69S	79:59.73E	-	11.2	1838	65:56.72S	79:59.11E	-
11 LEG1	2018 30-JAN-96 65:55.24S 80	0:00.29E 2099	2046	2115	65:55.26S	80:00.34E	2089	8.7	2232	65:55.33S	80:00.10E	-
12 LEG1	0000 31-JAN-96 65:47.99S 80	0:00.09E 2457	2522	0108	65:47.99S	79:59.64E	-	10.5	0229	65:48.29S	79:59.29E	2457
13 LEG1	0534 31-JAN-96 65:44.55S 79	9:59.65E 2866	2782	0701	65:44.74S	79:57.14E	2816	14.7	0841	65:45.34S	79:57.48E	-
14 LEG1	1153 31-JAN-96 65:38.11S 79	9:58.89E 3174	3144			79:58.60E	-	24.5	1436	65:39.05S	79:58.41E	-
15 LEG1	1701 31-JAN-96 65:21.56S 79	9:59.92E 3384	3396	1829	65:21.81S	79:58.52E	-	13.8	1958	65:21.99S	79:57.64E	-
16 LEG1	0255 1-FEB-96 64:51.51S 80	0:00.14E 3634	168	0309	64:51.45S	79:59.86E	-	-	0329	64:51.36S	79:59.62E	-
17 LEG1	0359 1-FEB-96 64:51.36S 79	9:59.68E 3634	3640	0526	64:51.10S	79:58.72E	-	20.4	0703	64:50.88S	79:57.35E	-
18 LEG1	1124 1-FEB-96 64:29.91S 79	9:59.89E 3634	3668	1303	64:29.12S	80:00.52E	-	15.0	1422	64:28.86S	80:00.75E	-
19 LEG1	1852 1-FEB-96 64:00.00S 79	9:59.82E 3686	3706			79:59.42E	-	18.3	_		79:59.40E	-
20 LEG1	0317 2-FEB-96 63:29.26S 79		3756	0447	63:29.22S	79:58.85E	-	13.2	0637	63:29.35S	79:58.61E	-
21 LEG1	1121 2-FEB-96 63:00.08S 80	0:00.01E 3583	166	1127	63:00.16S	80:00.18E	-	-	1146	63:00.09S	80:00.09E	-
22 LEG1	1226 2-FEB-96 63:00.13S 79		3574			79:59.83E	-	12.0	1508	63:00.79S	80:00.58E	-
23 LEG1	2159 2-FEB-96 62:59.97S 81		2862			81:49.48E	-	15.1			81:49.30E	-
24 LEG1	0526 3-FEB-96 62:59.98S 83	3:39.99E 2508	2490	0628	62:59.78S	83:40.09E	-	14.4	0754	62:59.65S	83:39.98E	-
25 LEG1	1531 3-FEB-96 62:59.92S 85	5:30.09E 3757	3784	1705	62:59.52S	85:30.42E	-	14.5			85:29.65E	
26 LEG4	2009 5-FEB-96 62:59.87S 88		3800			88:02.91E	-	13.7			88:02.52E	
27 LEG4	0318 6-FEB-96 62:59.92S 89		4008			89:53.45E	-	17.1			89:52.68E	4044
28 LEG4	1114 6-FEB-96 62:59.86S 91		3714			91:44.01E	-	13.9			91:43.32E	-
29 LEG4	1909 6-FEB-96 63:00.01S 93		170	1917	63:00.00S	93:33.83E	-	-	1933	62:59.98S	93:33.43E	-
30 LEG4	2010 6-FEB-96 62:59.98S 93	3:33.81E 3327	3318	2134	63:00.34S	93:32.97E	-	14.1	2305	63:00.23S	93:31.72E	3327
31 LEG4	0327 7-FEB-96 63:30.10S 93		3182	0436	63:30.16S	93:34.06E	-	14.3	0604	63:30.25S	93:33.00E	-
32 LEG4	1103 7-FEB-96 64:00.01S 93		3262	1218	64:00.07S	93:33.86E	-	10.9			93:33.61E	-
33 LEG4	1645 7-FEB-96 64:17.45S 93	3:33.59E 3051	3034	1804	64:17.82S	93:34.18E	3051	15.3	1941	64:17.98S	93:33.30E	-
34 LEG4	0058 8-FEB-96 64:38.25S 93	3:33.84E 2651	2638	0159	64:38.16S	93:33.78E	2651	13.0	0317	64:37.96S	93:33.16E	2651
35 LEG4	0435 8-FEB-96 64:43.97S 93		2252			93:32.61E	-	14.0			93:31.82E	
36 LEG4	0812 8-FEB-96 64:46.98S 93	3:33.22E 1791	1730	0905	64:47.22S	93:32.90E	1730	14.4	1006	64:47.54S	93:31.79E	1669

station	START	maxF	)	BOT	TOM				EN	ID	
number	time date latitude longitu	ude depth(m) (dbar	r) time	latitude	longitude de	epth(m) a	altimeter	time lati	tude	longitude of	depth(m)
37 LEG4	1137 8-FEB-96 64:48.06S 93:33	3.22E 1492 1440	1227	64:48.44S	93:31.62E	1413	17.9	1320 64:4	48.98S	93:30.22E	-
38 LEG4	1427 8-FEB-96 64:48.75S 93:33	3.40E 1278 1210	1506	64:49.20S	93:32.41E	1229	11.5	1545 64:4	49.73S	93:31.74E	-
39 LEG4	1651 8-FEB-96 64:50.05S 93:32	2.25E 925 888	1728	64:50.43S	93:30.77E	870	6.6	1815 64:	50.91S	93:28.89E	772
40 LEG4	2027 8-FEB-96 64:51.05S 93:32	2.73E 593 522	2059	64:51.34S	93:32.08E	532	14.3	2136 64:	51.59S	93:31.30E	512
41 LEG4	0109 9-FEB-96 65:01.62S 93:32	2.63E 467 450	0128	65:01.62S	93:32.32E	463	13.6	0156 65:	01.71S	93:31.90E	463
42 LEG4	1210 9-FEB-96 66:00.04S 93:33	3.62E 1228 1198	1253	65:59.88S	93:32.80E	1228	13.6			93:32.06E	1228
43 CAL	0454 10-FEB-96 64:48.96S 95:44			64:48.97S	95:44.45E	-	13.4	0509 64:4	48.93S	95:44.20E	112
44 LEG6	0026 11-FEB-96 62:42.58S 96:07					3614	14.4			96:07.15E	3635
45 LEG6	0823 11-FEB-96 62:39.84S 97:56	6.92E 3839 3886	0955	62:40.34S	97:55.12E	-	17.2	1118 62:4	40.83S	97:53.93E	-
46 LEG6	1623 11-FEB-96 62:37.06S 99:47	7.17E 4095 4124	1805	62:37.32S	99:47.70E	4095	13.2	2000 62:	37.45S	99:48.79E	4095
47 LEG6	0021 12-FEB-96 62:34.16S 101:3	37.59E 4761 4244	4 0150	62:33.61S	101:37.62E	4761	16.2	0353 62:	33.70S	101:36.99E	4761
48 LEG7	0841 13-FEB-96 65:00.15S 104:3			65:00.19S	104:39.90E	-	11.4	0926 65:	00.31S	104:39.71E	359
49 LEG7	1102 13-FEB-96 64:53.41S 104:3	7.66E 630 618	1125	64:53.38S	104:37.53E	635	15.8	1159 64:	53.35S	104:37.23E	644
50 LEG7	1256 13-FEB-96 64:50.03S 104:2			64:49.91S	104:29.16E	955	14.2	1405 64:4	49.74S	104:28.92E	981
51 LEG7	1608 13-FEB-96 64:47.13S 104:2	7.18E 1251 1238	3 1658	64:46.89S	104:26.63E	1251	14.1	1759 64:4	46.62S	104:25.98E	1254
52 LEG7	1924 13-FEB-96 64:43.78S 104:2			64:43.66S	104:23.76E	1561	13.9	2112 64:4	43.59S	104:23.76E	1575
53 LEG7	2229 13-FEB-96 64:38.27S 104:2	25.09E 1817 1786	2315	64:38.24S	104:24.51E	1761	15.0	0015 64:	38.16S	104:23.74E	1704
54 LEG7	0241 14-FEB-96 64:27.87S 104:2			64:27.83S	104:25.60E	2109	15.6	0452 64:	28.00S	104:24.45E	2048
55 LEG7	0729 14-FEB-96 64:17.68S 104:2			64:17.62S	104:25.69E	-	14.4	0953 64:	17.68S	104:25.29E	2549
56 LEG7	1106 14-FEB-96 64:15.02S 104:2			64:14.53S	104:26.20E	-	18.7	1349 64:	13.68S	104:26.68E	-
57 LEG7	1926 14-FEB-96 63:54.68S 104:2	26.00E 3337 3334	4 2053	63:54.49S	104:25.53E	3327	14.3	2221 63:	54.25S	104:25.69E	3357
58 LEG7	0203 15-FEB-96 63:35.75S 104:2				104:26.06E	3707	14.7	0514 63:	35.37S	104:26.14E	-
59 LEG7	0940 15-FEB-96 63:17.89S 104:2			63:18.20S	104:26.79E	-	13.6	1247 63:	18.09S	104:26.67E	-
60 LEG7	1619 15-FEB-96 63:00.02S 104:2	25.99E 3901 166	1628	63:00.07S	104:26.01E	-	-	1643 63:	00.13S	104:26.20E	3891
61 LEG7	1720 15-FEB-96 63:00.11S 104:2			63:00.29S	104:26.70E	-	14.6			104:25.64E	
62 LEG7	0155 16-FEB-96 63:06.60S 106:1				106:11.68E	-	13.9			106:12.15E	
63 LEG7	0907 16-FEB-96 63:13.60S 107:5				107:56.38E	-	14.6			107:56.61E	
64 LEG7	1655 16-FEB-96 63:20.44S 109:4	1.33E 3716 3726	1822	63:20.52S	109:40.91E	-	14.9	2004 63:	20.45S	109:39.90E	3716
65 CAL	1604 19-FEB-96 66:15.92S 110:3	31.36E 56 46	1610	66:15.88S	110:31.40E	59	22.5	1616 66:	15.85S	110:31.43E	59
66 LEG9	1211 23-FEB-96 65:45.43S 112:1	5.04E 438 420	1228	65:45.42S	112:15.13E	-	14.6	1300 65:4	45.47S	112:15.06E	438
67 LEG9	1643 23-FEB-96 65:25.11S 112:1				112:15.82E	328	11.0	1731 65:	24.80S	112:15.32E	348
68 LEG9	1915 23-FEB-96 65:23.87S 112:1				112:12.27E	584	33.8			112:11.93E	
69 LEG9	2222 23-FEB-96 65:19.65S 112:1			65:19.52S	112:12.66E	1106	14.8	2347 65:	19.24S	112:11.48E	1124
70 LEG9	0053 24-FEB-96 65:19.09S 112:1	4.88E 1222 1182	2 0144	65:18.94S	112:13.81E	-	14.3	0234 65:	18.85S	112:12.42E	1142
71 LEG9	0412 24-FEB-96 65:14.00S 112:1			65:14.20S	112:15.04E	-	13.4	0607 65:	14.51S	112:14.86E	-
72 LEG9	0732 24-FEB-96 65:09.30S 112:1	5.00E 1843 1832	2 0830	65:09.45S	112:15.92E		13.0	0942 65:	10.55S	112:16.26E	-

station		STA	RT	maxP	воттом	END
number	time date	latitude	longitude depth(m)	(dbar)	time latitude longitude depth(m) altime	eter time latitude longitude depth(m)
73 LEG9	1136 24-FEB-96	65:01.63	S 112:14.83E 2211	2152	1237 65:01.42\$ 112:15.91E - 18.0	) 1351 65:01.66S 112:16.17E -
74 LEG9	1806 24-FEB-96	64:35.07	S 112:14.99E 1873	1864	1903 64:35.07S 112:15.45E 1893 16.0	0 2017 64:35.08S 112:15.76E 1873
75 LEG9	0217 25-FEB-96	64:04.98	S 112:15.05E 2518	2542	0315 64:05.02S 112:15.63E - 16.1	0428 64:05.05S 112:15.74E 2560
76 LEG9	1017 25-FEB-96	63:34.98	S 112:14.92E 3276	3260	1149 63:35.38\$ 112:15.51E - 13.0	1313 63:35.33S 112:15.87E -
77 LEG9	1944 25-FEB-96	62:59.97	S 112:14.89E 3768	168	1953 62:59.97S 112:15.04E	2006 62:59.98S 112:15.28E 3788
78 LEG9	2034 25-FEB-96	62:59.97	S 112:16.01E 3768	3810	2206 63:00.05\$ 112:17.94E - 13.1	2350 63:00.36S 112:19.50E -
79 LEG9	0548 26-FEB-96	63:04.54	S 114:05.08E 3604	3618	0719 63:04.81S 114:05.57E - 17.0	0857 63:04.94S 114:04.63E -
80 LEG9	1314 26-FEB-96	63:09.20	S 115:55.07E 3512	3494	1443 63:09.55\$ 115:56.54E - 14.7	7 1614 63:09.99S 115:57.56E -
81 LEG9	2113 26-FEB-96	63:13.79	S 117:45.24E 3512	3526	2243 63:13.80S 117:47.05E - 13.2	
82 LEG11	0532 28-FEB-96	65:46.56	S 119:07.77E 614	598	0557 65:46.44S 119:08.35E - 13.8	
83 LEG11	1304 28-FEB-96			438	1331 65:42.75\$ 120:18.64E 450 15.0	
84 LEG11	1647 28-FEB-96	65:32.50	S 120:18.37E 614	574	1713 65:32.56S 120:18.59E 584 19.0	6 1745 65:32.80S 120:18.41E 522
85 LEG11			S 120:18.81E 948	948	1934 65:31.53S 120:19.17E 953 13.3	2 2013 65:31.78S 120:19.08E 829
86 LEG11			S 120:18.75E 1237	1180	2149 65:30.76S 120:18.87E 1198 15.	
87 LEG11	2341 28-FEB-96	65:29.44	S 120:19.74E 1848	1824	0030 65:29.55\$ 120:20.16E 1838 15.4	
88 LEG11	0232 29-FEB-96	65:28.34	S 120:18.70E 2132	2210	0337 65:28.19S 120:18.90E 2212 15.	7 0454 65:28.00S 120:19.54E -
89 LEG11			S 120:18.95E 2764	2762	0816 65:22.89S 120:20.01E - 14.9	
90 LEG11	1103 29-FEB-96	6 65:14.99	§ 120:18.87E 3071	3066	1225 65:15.00\$ 120:20.04E - 18.9	
91 LEG11			S 120:18.87E 3061	3064	1913 64:51.31S 120:18.51E 3061 13.8	
92 LEG11			S 120:18.62E 3502	3518	0154 64:27.34S 120:17.56E 3497 14.8	
93 LEG11			S 120:18.62E 3430	3414	1135 64:03.67\$ 120:17.90E 3410 17.	
94 LEG11			S 120:18.84E 3655	3652	1818 63:39.70S 120:19.57E 3635 14.3	
95 LEG11			S 120:18.81E 3727	166	2336 63:14.68S 120:18.70E	2348 63:14.56S 120:18.59E -
96 LEG11			S 120:18.93E 3737	3748	0147 63:14.38S 120:19.15E - 12.2	
97 LEG11			S 122:08.91E 3839	3888	0955 63:14.71S 122:10.09E - 14.4	
98 LEG11			S 123:58.77E 3983	4012	1825 63:14.70S 123:59.51E - 14.2	
99 LEG11			S 125:48.76E 4116	4146	0144 63:15.51S 125:50.90E 4111 15.0	
100 LEG13	0739 4-MAR-96			372	0757 65:35.91S 128:21.93E - 14.1	
101 LEG13	1216 4-MAR-96			352	1235 65:16.20S 128:28.26E 358 14.9	
102 LEG13			S 128:22.11E 614	590	1632 65:11.75S 128:21.45E - 17.4	
103 LEG13	1845 4-MAR-96			952	1923 65:10.69S 128:22.00E 921 16.9	
104 LEG13			S 128:22.20E 1249	1272	2217 65:09.97\$ 128:21.61E 1269 16.0	
105 LEG13			S 128:22.51E 1551	1484	0039 65:09.33S 128:22.12E 1474 12.	
106 LEG13			S 128:22.56E 1843	1804	0327 65:05.18S 128:22.40E 1843 13.	
107 LEG13			S 128:22.64E 1924	1884	0827 64:50.10S 128:23.69E 1894 15.3	
108 LEG13	1221 5-MAR-96	64:40.00	S 128:22.53E 2539	2522	1322 64:40.12S 128:22.27E - 15.2	2 1448 64:40.80S 128:22.15E -

station		STAI	RT	maxP	ВС	TTOM			EN	ND	
number	time date	latitude	longitude depth(m)	(dbar)	time latitude	longitude d	epth(m)	altimeter	time latitude	longitude dep	oth(m)
			<u> </u>				• • •			<u> </u>	, ,
109 LEG13	1725 5-MAR-96	64:27.245	S 128:22.50E 2682	2678	1824 64:27.55	S 128:22.62E	2672	16.9	1930 64:28.06S	128:23.32E 2	662
110 LEG13	2352 5-MAR-96	64:03.079	S 128:22.59E 3583	3606	0112 64:02.98	S 128:23.05E	-	12.8	0244 64:02.65S	128:23.14E 3	583
111 LEG13	0714 6-MAR-96	63:39.079	S 128:22.46E 3993	4010	0847 63:39.34	S 128:24.88E	-	15.4	1040 63:40.08S	128:27.63E	-
112 LEG13	1452 6-MAR-96	63:15.095	S 128:22.44E 4218	164	1459 63:15.18	S 128:22.35E	4218	-	1512 63:15.21S	128:22.47E 4	218
113 LEG13	1605 6-MAR-96	63:15.049	S 128:22.42E 4218	4266	1740 63:15.57	S 128:22.62E	-	13.7	1907 63:16.00S	128:23.23E 4	218
114 LEG13	0034 7-MAR-96	63:15.108	3 130:12.78E 4249	4302	0214 63:14.72	S 130:15.07E	-	16.5	0402 63:14.46S	130:17.37E	-
115 LEG13	0855 7-MAR-96	63:15.095	S 132:02.61E 4198	4250	1026 63:15.60	S 132:04.60E	-	13.1	1203 63:16.42S	132:05.41E	-
116 LEG13	1804 7-MAR-96	63:15.205	3 133:53.40E 4208	4260	1937 63:15.61	S 133:53.63E	4208	9.6	2107 63:15.63S	133:53.38E 4	208
117 LEG16	2231 11-MAR-96	63:14.91	S 136:26.24E 3993	4036	0010 63:15.17	S 136:27.64E	-	15.4	0147 63:15.31S	136:29.35E	-
118 LEG16	0739 12-MAR-96	63:22.42	S 138:08.53E 3880	3912	0909 63:22.33	S 138:08.43E	-	14.7	1043 63:22.48S	138:07.48E	-
119 LEG16	1733 12-MAR-96	63:29.97	S 139:50.98E 3788	164	1745 63:29.96	S 139:50.82E	-	-	1800 63:29.91S	139:50.83E	-
120 LEG16	1831 12-MAR-96	63:29.86	S 139:50.64E 3788	3824	1952 63:29.55	S 139:50.58E	-	15.1	2115 63:29.22S	139:50.53E 3	798
121 LEG16	0358 13-MAR-96	63:54.00	S 139:51.13E 3727	3750	0516 63:53.62	S 139:52.57E	-	11.1	0656 63:52.78S	139:54.50E	-
122 LEG16	1139 13-MAR-96	64:17.95	S 139:51.12E 3460	3456	1258 64:17.83	S 139:50.59E	-	13.1	1430 64:17.40S	139:50.14E	-
123 LEG16	1911 13-MAR-96	64:41.94	S 139:50.91E 2918	2910	2026 64:42.20	S 139:52.00E	-	15.2	2142 64:42.10S	139:52.41E 2	908
124 LEG16	0334 14-MAR-96	65:05.08	S 139:50.92E 2764	2768	0451 65:05.13	S 139:51.87E	-	14.4	0624 65:05.23S	139:52.94E	-
125 LEG16	1015 14-MAR-96	65:22.10	S 139:50.89E 2518	2486	1113 65:22.24	S 139:49.80E	-	14.1	1229 65:22.23S	139:48.88E	-
126 LEG16	1513 15-MAR-96	65:25.15	S 139:50.95E 2150	2292	1612 65:25.09	S 139:50.36E	-	23.7	1721 65:25.12S	139:49.78E 2	294
127 LEG16	1824 15-MAR-96	65:25.65	S 139:50.79E 1843	2136	1918 65:25.87	S 139:50.17E	-	22.4	2025 65:26.20S	139:49.24E	-
128 LEG16	0052 16-MAR-96	65:29.85	S 139:50.95E 1535	1480	0139 65:30.15	S 139:51.13E	-	17.4	0237 65:30.18S	139:51.85E	-
129 LEG16	0345 16-MAR-96	65:32.74	S 139:51.57E 1177	1130	0426 65:32.86	S 139:51.97E	-	15.2	0515 65:32.91S	139:52.12E	-
130 LEG16	0800 16-MAR-96	65:33.93	S 139:50.84E 942	910	0829 65:33.87	S 139:50.25E	932	15.1	0913 65:33.68S	139:49.14E 9	952
131 LEG16	1126 16-MAR-96	65:34.95	S 139:50.86E 614	548	1151 65:35.11	S 139:50.72E	543	8.8	1230 65:35.49S	139:50.34E 4	151
132 LEG16	1349 16-MAR-96	65:43.03	S 139:50.72E 296	288	1407 65:43.12	S 139:50.34E	307	16.0	1434 65:43.45S	139:50.10E 3	307
133 LEG18	0511 19-MAR-96	63:29.98	S 144:29.99E 3906	3952	0642 63:30.17	S 144:29.07E	-	13.6	0825 63:30.88S	144:28.15E	-
134 LEG18	1444 19-MAR-96	63:30.01	S 146:20.03E 3890	3926	1627 63:30.70	S 146:20.84E	-	15.2	1754 63:30.94S	146:20.58E	-
135 LEG18	2254 19-MAR-96	63:29.95	S 148:09.97E 3839	3868	0015 63:29.88	S 148:09.85E	-	12.9	0144 63:29.90S	148:09.88E	-
136 LEG18	0627 20-MAR-96	63:30.09	S 150:00.10E 3737	166	0645 63:30.13	S 150:00.14E	-	-	0705 63:30.20S	149:59.98E	-
137 LEG18	0742 20-MAR-96	63:29.95	S 149:59.78E 3737	3762	0902 63:30.45	S 149:59.91E	-	15.9	1039 63:30.94S	150:00.16E	-
138 LEG18	1503 20-MAR-96	63:54.08	S 149:59.98E 3675	3698	1634 63:53.76	S 150:00.04E	-	12.2	1802 63:53.32S	150:00.05E 3	675
139 LEG18	2147 20-MAR-96	64:18.04	S 149:59.58E 3573	3600	2301 64:18.07	S 150:00.37E	-	14.9	0024 64:18.20S	150:01.03E 3	573
140 LEG18	0315 21-MAR-96	64:36.09	S 149:59.77E 3481	3490	0440 64:36.66	S 150:00.41E	-	15.4	0600 64:36.90S	150:00.80E	-
141 LEG18	1228 21-MAR-96	65:00.13	S 149:59.86E 3317	3308	1345 65:00.25	S 149:58.12E	-	12.6	1516 65:00.49S	149:56.39E	-
142 LEG18	1910 21-MAR-96	65:23.97	S 150:00.19E 2923	2916	2018 65:23.73	S 149:59.87E	2918	13.8	2139 65:23.65S	150:00.21E 2	918
143 LEG18	0000 22-MAR-96	65:36.89	S 149:59.88E 2462	2448	0054 65:36.84		_	12.4	0201 65:36.78S	149:59.89E 2	467
144 LEG18	0854 22-MAR-96	65:43.41	S 149:54.54E 2099	2096	0954 65:43.29	S 149:54.22E	2099	10.3	1105 65:43.18S	149:54.04E	-

station	START	maxP	BOTTOM	END
number	time date latitude longitude depth(m)	(dbar)	time latitude longitude depth(m) altimeter	time latitude longitude depth(m)
145 CM 146 BIO 147 BIO	0856 23-MAR-96 65:55.74\$ 145:23.86E 796 1140 23-MAR-96 65:56.28\$ 145:41.21E 573 0732 25-MAR-96 65:54.39\$ 146:56.74E 576	688 154 150	0938 65:56.01\$ 145:23.92E 676 13.1 1157 65:56.28\$ 145:41.38E 563 - 0748 65:54.45\$ 146:56.62E	1017 65:56.22S 145:23.51E 625 1220 65:56.19S 145:41.12E 573 0808 65:54.48S 146:56.63E 545

<u>Table 2.3:</u> Summary of samples drawn from Niskin bottles at each station, including salinity (sal), dissolved oxygen (do), nutrients (nut), chlorofluorocarbons (CFC), <sup>18</sup>O, primary productivity (pp), fast repitition rate fluorometry (frrf), and pigments (pig); Seacat cast information was not available. Note that 1=samples taken, 0=no samples taken, 2=surface sample only (i.e. from shallowest Niskin bottle).

1 1 0 0 0 0 0 0 0	pig
2	0 0 0 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1

Table 2.3: (continued)

station	sal	do	nut	CFC	<sup>18</sup> O	pp	frrf	pig
51	1	1	1	1	1	0	1	1
52	1	1	1	1	1	0	1	1
53	1	1	1	1	1	0	1	1
54	1	1	1	1	1	1	1	1
55	1	1	1	1	1	0	1	1
56	1	1	1	1	1	0	1	1
57	1	1	1	1	1	0	1	1
58	1	1	1	1	1	0	1	1
59	1	1	1	1	1	0	1	1
60	0	0	0	0	0	1	1	1
61	1	1	1	1	1	0	0	0
62	1 1	1 1	1 1	1 1	1 1	0	0 0	0
63 64	1	1	1	1	1	0	0	0 0
65	1	0	0	0	0	0	0	0
66	1	1	1	1	1	1	1	1
67	1	1	1	1	1	0	1	1
68	1	1	1	1	1	0	1	1
69	1	1	1	1	1	0	1	1
70	1	1	1	1	1	0	1	1
71	1	1	1	1	1	1	1	1
72	1	1	1	1	1	1	1	1
73	1	1	1	1	1	0	1	1
74	1	1	1	1	1	0	1	1
75	1	1	1	1	1	0	1	1
76	1	1	1	1	1	0	1	1
77	0	0	0	0	0	1	1	1
78	1	1	1	1	1	0	0	0
79	1	1	1	1	1	0	0	0
80	1	1	1	1	1	0	0	0
81	1	1	1	1	1	0	0	0
82	1	1	1	1	1	1	1	1
83	1	1	1	1	1	0	1	1
84	1	1	1	1	1	0	1	1
85	1	1	1	1	1	0	1	1
86	1	1	1	1	1	0	1	1
87	1	1	1	1	1	0	1	1
88	1 1	1 1	1	1 1	1 1	1 1	1	1
89 90	1	1	1 1	1	1	0	1 1	1 1
90	1	1	1	1	1	0	1	1
92	1	1	1	1	1	0	1	1
93	1	1	1	1	1	0	1	1
94	1	1	1	1	1	0	1	1
95	0	0	0	0	0	1	1	1
96	1	1	1	1	1	0	0	0
97	1	1	1	1	1	0	0	0
98	1	1	1	1	1	0	0	0
99	1	1	1	1	1	0	0	0
100	1	1	1	1	1	1	1	1
101	1	1	1	1	1	0	1	1
102	1	1	1	1	1	0	1	1
103	1	1	1	1	1	0	1	1
104	1	1	1	1	1	0	1	1

Table 2.3: (continued)

station	sal	do	nut	CFC	<sup>18</sup> O	pp	frrf	pi	g
105	1	1	1	1	1	1	1	1	
106	1	1	1	1	1	0	1	1	
107	1	1	1	1	1	1	1	1	
108	1	1	1	1	1	0	1	1	
109	1	1	1	1	1	0	1	1	
110	1	1	1	1	1	0	1	1	
111	1	1	1	1	1	0	1	1	
112	0	0	0	0	0	1	1	1	
113	1	1	1	1	1	0	0	0	
114	1	1	1	1	1	0	0	0	
115	1	1	1	1	1	0	0	0	
116	1	1	1	1	1	0	0	0	
117	1	1	1	1	1	0	0	0	
118	1	1	1	1	1	0	0	0	
119	0	0	0	0	0	0	1	1	
120	1	1	1	1	1	0	0	0	
121	1	1	1	1	1	1	1	1	
122	1	1	1	1	1	0	1	1	
123	1	1	1	1	1	0	1	1	
124	1	1	1	1	1	1	1	1	
125	1	1	1	1	1	0	1	1	
126	1	1	1	1	1	0	1	1	
127	1	1	1	1	1	0	1	1	
128	1	1	1	1	1	1	1	1	
129	1	1	1	1	1	0	1	1	
130 131	1 1	1 1	1 1	1 1	1 1	0 0	1	1 1	
132	1	1	1	1	1	0	1	1	
133	1	1	1	1	1	0	0	0	
134	1	1	1	1	1	0	0	0	
135	1	1	1	1	1	0	0	0	
136	0	0	0	0	0	1	1	1	
137	1	1	1	1	1	0	0	0	
138	1	1	1	1	1	0	1	1	
139	1	1	1	1	1	0	1	1	
140	1	1	1	1	1	1	1	1	
141	1	1	1	1	1	0	1	1	
142	1	1	1	1	1	0	1	1	
143	1	1	1	1	1	0	1	1	
144	1	1	1	1	1	1	1	1	
145	1	1	1	1	1	0	0	0	
146	0	0	0	0	0	0	1	1	
147	0	0	0	0	0	0	1	1	

<u>Table 2.4:</u> Bottom pressure recorder, upward looking sonar, and current meter moorings deployed/recovered during cruise AU9604. Note that for current meter moorings, mooring locations and water depths are estimates only, and instrument elevations are elevations above the bottom.

BOTTOM PRA deployment number		ent/recovery	latitude	longitude	CTD station no.	bottom depth(m)
instruments de Hobart96 Dumont96	06:24, (	06/01/96 16/03/96	44 <sup>0</sup> 07.019' 65 <sup>0</sup> 33.71'S			998 1024
instruments re Hobart94 Dumont94	06:11, (	06/01/96 15/03/96	44 <sup>0</sup> 07.18'S 65 <sup>0</sup> 33.67'S			1028 1024
unsuccessful de Hobart91b		ttempts 06/01/96	44 <sup>0</sup> 06.83'S	146 <sup>0</sup> 14.03'l	Ē -	1024
name tii	ployment me (UTC)	<i>DNARS</i> latitud	e longitu	ude instrumer depths (m)		bottom depth(m)
instruments de SO-ON 21	:56, 28/01/	96 68 <sup>0</sup> 08	3.30'S 76 <sup>0</sup> 0	2.37'E 150 (UL	S) 4	478
SOFORTH 13	3:15, 29/01	/96 66 <sup>0</sup> 15	5.28'S 77 <sup>0</sup> 0	2.74'E 160 (UL 210 (CM		2866
CURRENT MA site recov name time (	ery	ORINGS latitude	longitude	current meter elevations (m)	CTD station no.	bottom depth(m)
instruments re CM2 08:02	ecovered , 23/03/96	65 <sup>0</sup> 55.72'S	145 <sup>0</sup> 24.69'E	65 25 (not reco 15	145 overed) vel recorder (not	~740
unsuccessful de CM1 24-25, CM3 24/03,	/03/96	ttempts 65° 54.11'S 66° 03.13'S			<u>-</u> -	~600 ~515

#### 2.3.2 Moorings deployed/recovered

Two bottom pressure recorders were recovered near the north and south ends of the WOCE SR3 section, and two pressure recorders were deployed as replacements. A further pressure recorder at the north end of SR3 could not be recovered. Two upward looking sonar moorings were deployed in the vicinity of Davis. One current meter mooring was recovered from the eastern end of the MARGINEX study region; two further current meter moorings in the vicinity could not be recovered. Table 2.4 summarizes all mooring locations and deployment/recovery times.

#### 2.3.3 **Drifters deployed**

8 drifting Argos buoys, manufactured by Turo Technology, were deployed throughout the cruise in the MARGINEX study region (Table 2.5).

#### Principal investigators 2.3.4

The principal investigators for the CTD and water sample measurements are listed in Table 2.6a. Cruise participants are listed in Table 2.6b.

Table 2.5: Argos buoys deployed on cruise au9604.

Buoy id no.	deployment time (UTC)	latitude	longitude	bottom depth (m)	sea surf. temp. (°C)	air temp. ( <sup>O</sup> C)	air pressure (hPa)
27237 27239 27236 27235 27240 27238 24669	12:25,12/02/96 18:48,27/02/96 20:53,03/03/96 14:41,08/03/96 05:03,11/03/96 09:15,18/03/96 10:34,24/03/96	65° 09.18'S 65° 10.34'S 64° 38.55'S 64° 59.87'S 65° 54.01'S	101° 37.35'E 117° 44.95'E 125° 48.44'E 135° 52.52'E 136° 26.32'E 144° 29.60'E 148° 59.31'E	1211 1415 1214 1218 1165	-0.51 -0.51 -0.49 -0.32 -0.13 -1.62	-1.0 -5.8 -2.1 -2.0 -2.7 -1.3 -3.2	985.4 992.4 984.8 989.7 975.0 997.2 980.6
24669 24673	08:43,25/03/96		147 <sup>0</sup> 00.59'E		-1.80 -1.76	-3.2 -3.4	985.1

Table 2.6a: Principal investigators (\*=cruise participant) for rosette water sampling programmes.

measurement	name	affiliation
CTD, salinity, O <sub>2</sub> , nutrients	*Nathan Bindoff/Steve Rintoul	Antarctic CRC/CSIRO
chlorofluorocarbons	*Mark Warner	University of Washington
<sup>18</sup> O	Russell Frew	Otago University
primary productivity	John Parslow	CSIRO
fast repitition rate fluorometry	*Peter Strutton(PhD student)	Flinders University
biological sampling	Harvey Marchant/*Simon Wright	Antarctic Division

<u>Table 2.6b:</u> Scientific personnel (cruise participants).

name	measurement	affiliation
Nathan Bindoff Tim Gibson Doug Gillespie John Hunter Ian Knott Mark Rosenberg Mike Williams	CTD CTD, weather balloons whale hydroacoustics, CTD CTD CTD, electronics CTD, moorings CTD	Antarctic CRC Antarctic CRC Oxford University CSIRO Antarctic CRC Antarctic CRC Antarctic CRC
Stephen Bray Mark Rayner Phillip Towler	salinity, oxygen, nutrients salinity, nutrients oxygen	Antarctic CRC CSIRO University of Melbourne
Steve Covey Mark Warner	CFC CFC	University of Washington University of Washington
Clive Crossley Rick van den Enden Paul Scott Peter Strutton Raechel Waters Simon Wright biolo	biological sampling biological sampling biological sampling biological sampling biological sampling gical sampling, deputy voyage lea	Antarctic CRC Antarctic Division Antarctic Division Flinders University Antarctic Division ider Antarctic Division
Toby Bolton Jon Havenhand Rob King John Kitchener Steve Nicol Robin Thompson Patti Virtue	krill krill krill krill krill, voyage leader krill	Flinders University Flinders University Antarctic Division Antarctic Division Antarctic Division Antarctic Division Antarctic Division Antarctic Division
lan Higginbottom Tim Pauly	hydroacoustics hydroacoustics	Antarctic Division Antarctic Division
Karen Evans Peter Gill Jennifer Gillot Deb Glasgow Claire Green Paul Hodda Mick Mackey Debbie Thiele	whale observations	Antarctic Division
Eric Woehler Stephanie Zador	ornithology ornithology	Antarctic Division Antarctic Division
Pamela Brodie Chris Boucher Roy Francis Gordon Keith Steve Oakley Tim Ryan Rob Walker	programmer electronics doctor programmer returnee underway measurements gear officer	Antarctic Division

#### 2.4 FIELD DATA COLLECTION METHODS

#### 2.4.1 CTD and hydrology measurements

In this section, CTD and hydrology data collection and processing methods are discussed. Preliminary results of the CTD data calibration, along with data quality information, are presented in Section 2.6. CTD instrumentation, CTD and hydrology data collection techniques and water sampling methods are described in detail in previous data reports (Rosenberg et al. 1995a, 1995b, 1996).

Briefly, General Oceanics Mark IIIC (i.e. WOCE upgraded) CTD units were used, with a General Oceanics model 1015 pylon, and 10 litre General Oceanics Niskin bottles. A 24 bottle rosette package was used, with deep sea reversing thermometers (Gohla-Precision) mounted at rosette positions 2, 12 and 24. A Li-Cor photosynthetically active radiation (p.a.r.) sensor and Sea-Tech fluorometer were also attached to the package for some casts. Complete calibration information for the CTD pressure, platinum temperature and pressure temperature sensors are presented in Table 2.23, along with fluorometer and p.a.r. calibrations. Note that correct scaling of fluorescence data requires linkage with primary productivity data, while p.a.r. data requires recalculation using extinction coefficients for the signal strength (B. Griffiths, pers. comm.). The complete CTD conductivity and CTD dissolved oxygen calibrations, derived respectively from the in situ Niskin bottle salinity and dissolved oxygen samples, are presented in a later section.

The CTD and hydrology data processing and calibration techniques are described in detail in Appendix 2 of Rosenberg et al. (1995b) (referred to as "CTD methodology" for the remainder of the report), with the following updates to the methodology:

- (i) the 10 seconds of CTD data prior to each bottle firing are averaged to form the CTD upcast for use in calibration (5 seconds was used previously);
- (ii) in the conductivity calibration for stations 11 to 61 and stations 71 to 144, an additional term was applied to remove the pressure dependent conductivity residual.

The analytical techniques and data processing routines employed in the Hydrographic Laboratory onboard the ship are discussed in Appendix 2.1 of this report, and in Appendix 3 of Rosenberg et al. (1995b). Note the following changes to the methodology:

- (i) 150 ml sample bottles were used, and 1.0 ml of reagents 1, 2 and 3 were used; the corresponding calculated value for the total amount of oxygen added with the reagents = 0.017 ml;
- (ii) a mean volume of 147.00 ml for oxygen sample bottles was applied in the calculation of dissolved oxygen concentration;
- (iii) nutrient autoanalyser results were processed by the software package "FASPac" (Astoria-Pacific International):
- (iv) salinity substandards were measured every 12 samples typically.

#### 2.4.2 Underway measurements

Underway data collection is as described in previous data reports; data files are described in Part 5. Note that a sound speed of 1498 ms<sup>-1</sup> is used for all depth calculations, and the ship's draught of 7.3 m has been accounted for in final depth values (i.e. depths are values from the surface).

#### 2.4.3 ADCP

The acoustic Doppler current profiler (ADCP) instrumentation is described in previous data reports. GPS data were collected by a Koden receiver for the entire cruise, receiving both GPS positions and velocities every 1 second. ADCP data processing is discussed in more detail in Dunn (a and b, unpublished reports). Logging parameters are summarised in Table 2.7, while data results for this cruise will be discussed in a future report.

### Table 2.7: ADCP logging parameters.

ping parameters bottom track ping parameters

no. of bins: 60 no. of bins: 128 bin length: 8 m bin length: 4 m pulse length: 8 m pulse length: 32 m

delay: 4 m

ping interval: minimum ping interval: same as profiling pings

reference layer averaging: bins 8 to 20 ensemble averaging duration: 3 min.

#### 2.5 MAJOR PROBLEMS ENCOUNTERED

## 2.5.1 Logistics

On the final CTD leg 18 (Figure 2.1b), traversed north to south, the section was prematurely terminated in a depth of ~2100 m, well short of the shelf break. Heavy ice together with time and fuel limitations did not allow further ice-breaking which would have been necessary to reach the shelf break.

### 2.5.2 CTD sensors

Following station 81, the CTD dissolved oxygen sensor was replaced. After the cruise, analysis of data collected with the replacement sensor indicated that the oxygen current response of the sensor was poor. Thus CTD dissolved oxygen data for the second half of the cruise was of low quality, and these data were not processed further.

For most of the cruise, conductivity calibrations were of a lower quality than for previous cruises. This was due to a combination of unstable salinometer performance and a significant pressure dependent response of both conductivity cells used on CTD 1103 (see section 6 for more details).

The fluorometer on the rosette package flooded during station 35, and was unusable for the remainder of the cruise.

#### 2.5.3 Moorings

Of the three current meter moorings at the eastern end of the MARGINEX study region, only one was recovered, and only partially so - a current meter and a water level recorder were lost while dragging for the recovered mooring. No precise positions or water depths were available for the moorings, and no ranging equipment was included in the moorings, making the recovery operation a difficult one.

The four year pressure recorder mooring Hobart91b (Table 2.4) failed to release from the bottom mooring weight, despite flawless communication with the acoustic release. This failure was identical with that for the two moorings Dumont92a and b, described in Rosenberg et al. 1995b.

#### 2.5.4 Other equipment

The ship's gyrocompass malfunctioned on several occasions throughout the cruise, at one stage leaving the ship with no gyro for several days. ADCP data from these times will be poor.

#### 2.6 CTD RESULTS

This section details information relevant to the creation and quality of the final CTD and hydrology data set. For actual use of the data, the following is important:

```
CTD data - Tables 2.15 and 2.16, and Table 2.8; hydrology data - Tables 2.20 and 2.21.
```

Historical data comparisons are made in Part 4 of this report. Data file formats are described in Part 5.

#### 2.6.1 CTD measurements - data creation and quality

CTD data calibration and processing methods are described in detail in the CTD methodology (i.e. Appendix 2 of Rosenberg et al., 1995b, with the additions listed in section 2.4.1 of this report). Cases for cruise au9604 which vary from this methodology are detailed in this section. CTD data quality is also discussed. For conversion to WOCE data file formats, see Part 5 of this report.

The final calibration results for conductivity/salinity and dissolved oxygen, along with the performance check for temperature, are plotted in Figures 2.2 to 2.5. For temperature, salinity and dissolved oxygen, the respective residuals ( $T_{therm}$  -  $T_{cal}$ ), ( $s_{btl}$  -  $s_{cal}$ ) and ( $o_{btl}$  -  $o_{cal}$ ) are plotted. For conductivity, the ratio  $c_{btl}/c_{cal}$  is plotted.  $T_{therm}$  and  $T_{cal}$  are respectively the protected thermometer and calibrated upcast CTD burst temperature values;  $s_{btl}$ ,  $s_{cal}$ ,  $o_{btl}$ ,  $o_{cal}$ ,  $c_{btl}$  and  $c_{cal}$ , and the mean and standard deviation values in Figures 2.2 to 2.5, are as defined in the CTD methodology (with additional definitions described below for cases where a pressure dependent residual is removed from conductivity data).

## 2.6.1.1 Conductivity/salinity

The conductivity calibration for CTD 1103 (stations 3 to 144) revealed problems with the salinity measurements for both the CTD and salinometers. A larger than usual conductivity calibration scatter (Figures 2.3 and 2.4) resulting from poor salinometer performance was superimposed on a pressure dependent conductivity residual resulting from CTD conductivity cell contamination. The pressure dependent conductivity residual was found for both conductivity cells used with CTD 1103, and is assumed to result from a light fouling or contamination of both cells. An extra fit was applied to remove this residual, following the same method as described in Part 1 (section 1.6.1.1) of this report. Note that station grouping for the extra fit parameter  $\alpha$  (defined in eqn 1.1 in Part 1 of this report) was separate from and different to the initial conductivity calibration station grouping (Table 2.10). After application of the pressure dependent conductivity correction, the standard deviation of the salinity calibration scatter decreased from 0.0027 to 0.0024 (PSS78) (Figure 2.4). This standard deviation value remained high due to unstable performance of all 4 YeoKal salinometers used for salinity sample analysis on the cruise.

For the remaining stations using CTD 1193, CTD conductivity cell performance was good.

#### 2.6.1.2 Temperature

Platinum temperature sensor performance of the CTD's was stable throughout the entire cruise, with a small offset between thermometer and CTD temperature values (Figure 2.2). Note that a post cruise temperature calibration was required for CTD 1193, as the pre cruise calibration for this instrument did not appear to be applicable.

#### **2.6.1.3 Pressure**

For stations 8, 89 and 116, data logging commenced when the CTD was already in the water, so surface pressure offset values were estimated from surrounding stations. For station 68, conductivity cell freezing interfered with the automatic estimation of surface pressure offsets (see CTD methodology), while pressure spiking interfered with pressure offset values for stations 29 and 48; for these stations, surface pressure offset values were estimated from a manual inspection of the pressure data. Note that for all these stations, any resulting additional error in the CTD pressure data is judged to be small (no more than 0.2 dbar).

#### 2.6.1.4 Dissolved oxygen

Usable CTD dissolved oxygen data were only obtained for half of the cruise (stations 6 to 80 and station 145). For these stations, the final standard deviation value of the dissolved oxygen residuals (Figure 2.5) are less than 1% of full scale values (where full scale is approximately equal to 250  $\mu$ mol/l for pressure > 750 dbar, and 350  $\mu$ mol/l for pressure < 750 dbar). In most cases, the best calibration was achieved using large values of the order 12.0 for the coefficient K<sub>1</sub> (i.e. oxygen current slope), and large negative values of the order -2.0 for the coefficient K<sub>3</sub> (i.e. oxygen current bias) (Table 2.17).

#### 2.6.1.5 Fluorescence and P.A.R. Data

Fluorescence and p.a.r. are effectively uncalibrated. These data should not be used quantitatively other than for linkage with primary productivity data.

Table 2.8: Summary of cautions to CTD data quality.

station no.	CTD parameter	caution
2,3	salinity	test cast - all bottles fired at same depth; salinity accuracy reduced
8	salinity	CTD conductivity cell behaviour for this station different to surrounding stations - stn 8 calibrated on its own (i.e. not grouped)
8,89,116	pressure	surface pressure offset estimated from surrounding stations
29,48,68	pressure	surface pressure offset estimated from manual inspection of data
19,24,26	oxygen	oxygen calibration fit fairly poor
146,147	salinity	conductivity calibration for stn 145 applied to these stations
11-61,71-14	14 salinity	additional correction applied for pressure dependent conductivity residual
81-144	oxygen	no CTD dissolved oxygen data due to faulty oxygen sensor
all stns	fluorescence/p.a.r.	fluorescence and p.a.r. sensors (where active) are uncalibrated

#### 2.6.1.6 Summary of CTD data creation

Information relevant to the creation of the calibrated CTD data is tabulated, as follows:

- \* Surface pressure offsets calculated for each station are listed in Table 2.9.
- \* CTD conductivity calibration coefficients, including the station groupings used for the conductivity calibration, are listed in Tables 2.10 and 2.11.
- \* CTD raw data scans flagged for special treatment are listed in Table 2.12.
- \* Missing 2 dbar data averages are listed in Table 2.13.
- \* 2 dbar bins which are linearly interpolated from surrounding bins are listed in Table 2.14.
- \* Suspect 2 dbar averages are listed in Tables 2.15 and 2.16.
- \* CTD dissolved oxygen calibration coefficients are listed in Table 2.17. The starting values used for the coefficients prior to iteration, and the coefficients varied during the iteration, are listed in Table 2.18.
- \* The different protected and unprotected thermometers used for the stations are listed in Table 2.22.
- \* Laboratory calibration coefficients for the CTD's are listed in Table 2.23.

#### 2.6.1.7 Summary of CTD data quality

CTD data quality cautions for the various parameters are summarised in Table 2.8.

#### 2.6.2 Hydrology data

Quality control information relevant to the hydrology data is tabulated, as follows:

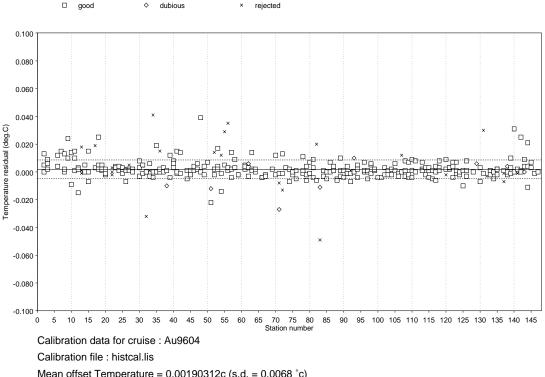
- \* Dissolved oxygen Niskin bottle samples flagged with the code -9 (rejected for CTD dissolved oxygen calibration) are listed in Table 2.19.
- \* Questionable dissolved oxygen and nutrient Niskin bottle sample values are listed in Tables 2.20 and 2.21 respectively. Note that questionable values are included in the hydrology data file, whereas bad values have been removed.

Laboratory temperature on the ship was stable, with lab temperatures at the times of nutrient analyses having a most common value of 19.6°C.

For stations 23 to 26, autoanalyser peak heights for silicate were measured manually, and a linear fit was applied to the calibration standards.

For station 22, bottle salinity values were bad, and were not used in the calibration procedure.

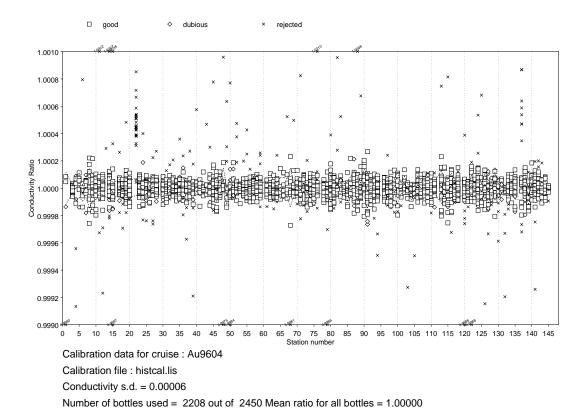
For stations 28 and 42, phosphate data were bad.



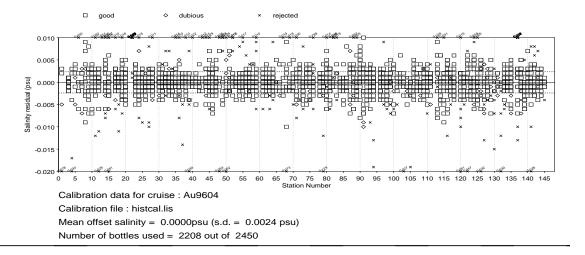
Mean offset Temperature = 0.00190312c (s.d. = 0.0068 °c)

Number of samples used = 289 out of 326

Figure 2.2: Temperature residual ( $T_{therm}$  -  $T_{cal}$ ) versus station number for cruise au9604. The solid line is the mean of all the residuals; the broken lines are  $\pm$  the standard deviation of all the residuals (see CTD methodology). Note that the "dubious" and "rejected" categories refer to the conductivity calibration.



<u>Figure 2.3:</u> Conductivity ratio  $c_{btl}/c_{cal}$  versus station number for cruise au9604. The solid line follows the mean of the residuals for each station; the broken lines are  $\pm$  the standard deviation of the residuals for each station (see CTD methodology).



<u>Figure 2.4:</u> Salinity residual ( $s_{btl}$  -  $s_{cal}$ ) versus station number for cruise au9604. The solid line is the mean of all the residuals; the broken lines are  $\pm$  the standard deviation of all the residuals (see CTD methodology).

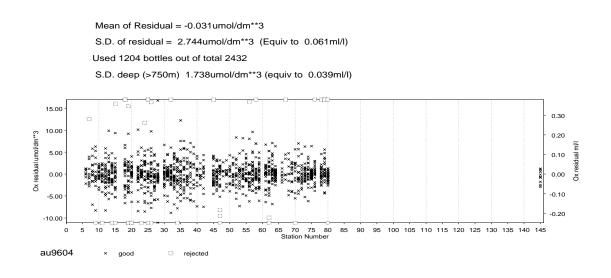


Figure 2.5: Dissolved oxygen residual (o<sub>btl</sub> - o<sub>cal</sub>) versus station number for cruise au9604.

<u>Table 2.9:</u> Surface pressure offsets (as defined in the CTD methodology). \*\* indicates that value is estimated from surrounding stations, or else determined from manual inspection of pressure data.

stn no.	surface p offset (dbar)	stn no.	surface p offset (dbar)	stn no.	surface p offset (dbar)	str no	
1	-0.25	41	-0.37	81	-0.33	12	
2	-0.61	42	-0.49	82	-0.89	12	
3	0.37	43	-0.48	83	-0.92	12	
4	0.11	44	-0.39	84	-0.56	12	
5	0.95	45	0.05	85	-0.51	12	
6	1.16	46	-0.65	86	-0.47	12	
7	1.33	47	-0.19	87	-0.35	12	
8	1.36**	48	0.00**	88	-0.75	12	
9	1.40	49	-0.40	89	-0.77**	12	
10	0.41	50	-0.15	90	-0.80	13	
11	1.61	51	-0.54	91	-0.74	13	
12	0.09	52	-0.32	92	-0.81	13	
13	0.28	53	-0.25	93	-0.88	13	
14	0.16	54	-0.99	94	-0.64	13	
15	0.04	55	-0.46	95	-0.75	13	
16	-0.06	56	-0.69	96	-0.92	13	
17	-0.03	57	-1.01	97	-0.75	13	
18	-0.24	58	-0.70	98	-0.39	13	
19	-0.22	59	-0.51	99	-0.45	13	
20	-0.36	60	-0.20	100		14	
21 22	0.07	61 62	-1.02	101		14	
	-0.33		0.94	102		14	
23 24	-0.34 -0.59	63 64	-0.45	103		14 14	
24 25	-0.38	65	-0.80 -0.26	104 105		14	
26	-0.36	66	-0.26 -0.45	105		14	
27	-0.26	67	-0.45 -0.35	107		14	
28	-0.26	68	-0.50**	107		14	7 -0.45
29	-0.40	69	-0.42	109			
30	-1.05	70	-0.42	110			
31	-0.33	71	-0.10	111			
32	-0.40	72	-0.20	112			
33	-0.53	73	-0.14	113			
34	-0.30	74	-0.63	114			
35	-0.53	75	-0.69	115			
36	-0.41	76	-0.84	116			
37	-0.68	77	-0.49	117			
38	-0.09	78	-0.64	118			
39	-0.08	79	-0.47	119			
40	-0.37	80	-0.18	120			
. •							

<u>Table 2.10:</u> CTD conductivity calibration coefficients.  $F_1$ ,  $F_2$  and  $F_3$  are respectively conductivity bias, slope and station-dependent correction calibration terms. n is the number of samples retained for calibration in each station grouping;  $\sigma$  is the standard deviation of the conductivity residual for the n samples in the station grouping (see CTD methodology);  $\sigma$  is the correction applied to CTD conductivities due to pressure dependence of the conductivity residuals (see eqn 1.1 in Part 1 of this report).

stn grouping	g F₁	F <sub>2</sub>	$F_3$	n	σ	α
001 to 001	-3.4008230	0.10266676E-02	0	3	0.004993	-
002 to 002	-3.4008230	0.10266676E-02	0	3	0.004993	-
003 to 004	0.55764682	0.99645743E-03	28960267E-05	24	0.001263	_
005 to 007	52606214E-02	0.10046804E-02	0.95765457E-07	23	0.002064	_
008 to 008	0.44036103E-01	0.10031503E-02	0		0.004031	_
009 to 010	79348989E-01	0.10081906E-02	41941891E-07	31	0.002407	_
011 to 017	63365640E-01	0.10002300E 02 0.10072857E-02	0.92934405E-08	98	0.002407	6.30E-07
018 to 019	16941205E-01	0.10072037E-02 0.10029438E-02	0.16218103E-06	41	0.001703	6.30E-07
020 to 024	34773276E-01	0.10023430E 02 0.10062501E-02	0.27600438E-07	67	0.002006	6.30E-07(stn20)
020 10 024	.047702702 01	0.100020012 02	0.270004002 07	01	0.002000	6.99E-07(stn21-24)
025 to 027	42861170E-01	0.10088248E-02	72135270E-07	65	0.001325	6.99E-07
028 to 030	38426094E-01	0.10043136E-02	0.84881449E-07	45	0.001317	
031 to 033	45089981E-01	0.10045100E 02 0.10086500E-02	50005682E-07	67	0.001317	8.14E-07
034 to 035	16210020E-01	0.10030300E-02 0.10136385E-02	22598949E-06	41	0.001103	
034 to 033	21369310E-01	0.10130303E-02 0.10091878E-02	82466648E-07	31	0.001223	8.14E-07
038 to 040	50591527E-02	0.10091676E-02 0.10050644E-02	0.20181984E-07	32	0.001314	8.14E-07
036 to 040 041 to 042	45224069E-01	0.10030644E-02 0.10118294E-02	10457316E-06	32 20	0.001201	7.36E-07
			50554005E-06			
043 to 044	89106026E-01	0.10309086E-02		26	0.001366	7.36E-07
045 to 047	17972448E-02	0.10058200E-02	25894965E-08	69	0.001945	7.36E-07
048 to 051	11278398E-02	0.10018826E-02	0.75038871E-07	32	0.002178	7.36E-07(stn48-50)
050 / 054	000001705 04	0.400770405.00	000050445 07	4.4	0.004050	6.06E-07(stn51)
052 to 054	22038176E-01	0.10077813E-02	29925844E-07	41	0.001056	6.06E-07
055 to 057	25708043E-01	0.10036519E-02	0.51001329E-07	63	0.001257	6.06E-07
058 to 060	16543813E-01	0.10067962E-02	11086368E-07	39	0.001133	6.06E-07
061 to 062	47632077E-01	0.10066633E-02	0.10413888E-07	45	0.001201	6.06E-07(stn61)
0001 001	007050405 00	0.404550005.00	450000055 00	40	0.004444	- (stn62)
063 to 064	60785919E-02	0.10155002E-02	15326305E-06	40	0.001144	-
065 to 066	16546893E-01	0.10296772E-02	35846498E-06	14	0.001768	-
067 to 068	0.55308088E-02	0.10128742E-02	10922184E-06	13	0.003147	- ( , , , , , , , , , , , , , , , , , ,
069 to 074	22735305E-01	0.10084174E-02	30649004E-07	82	0.001731	- (stn69-70)
.===.	004000045 04	0.400740075.00				10.16E-07(stn71-74)
075 to 076	86408281E-01	0.10071895E-02	0.16918503E-07	41		10.16E-07
077 to 079	19036812E-01	0.10126020E-02	82942800E-07	44		10.16E-07
080 to 081	24748542E-01	0.10069379E-02	84236957E-08	43	0.002302	10.16E-07(stn80)
0001 001	050744745 04	0.404400045.00	004044575 07		0.004004	4.09E-07(stn81)
082 to 084	35271471E-01	0.10118694E-02	62164157E-07	20	0.001201	4.09E-07
085 to 088	43779395E-01	0.10081677E-02	15567609E-07	56	0.002321	4.09E-07
089 to 091	26888057E-01	0.10126024E-02	70609756E-07	67	0.002901	4.09E-07(stn89-90)
						7.45E-07(stn91)
092 to 093	25957370E-01	0.10035524E-02	0.29544867E-07	43	0.001936	7.45E-07
094 to 096	18031989E-01	0.10067845E-02	75915753E-08	46		7.45E-07
097 to 099	0.72025201E-02	0.10024057E-02	0.27868859E-07		0.001602	
100 to 101	53994702E-01	0.10336150E-02	26094479E-06	15	0.002287	7.45E-07(stn100)
						9.30E-07(stn101)
102 to 106	32221287E-01	0.10092370E-02	25813131E-07	54	0.001596	
107 to 108	27064708E-01	0.10121597E-02	55131810E-07	35		9.30E-07
109 to 110	41781867E-01	0.10204373E-02	12507360E-06	44		9.30E-07
111 to 116	51999880E-01	0.10066765E-02	0.40501302E-08	96	0.002602	10.39E-07
117 to 120	78123279E-01	0.10079076E-02	0.14758557E-08	62		10.39E-07
121 to 123	30409364E-01	0.10153867E-02	74014007E-07	65		10.33E-07
124 to 129	26783184E-01	0.10070376E-02	63658094E-08	97		10.33E-07
130 to 132	99892436E-01	0.99483839E-03	0.10644714E-06	18		10.33E-07(stn130)
					(	6.37E-07(stn131-132)

# Table 2.10: (continued)

stn grouping	ι F <sub>1</sub>	$F_2$	$F_3$	n	σ	α
133 to 134	45705617E-01	0.10181827E-02	85306942E-07	44	0.001385	6.37E-07
135 to 137	56982632E-01	0.99366156E-03	0.10145251E-06	36	0.002465	6.37E-07
138 to 140	35961294E-01	0.10126337E-02	42141044E-07	67	0.002214	6.37E-07
141 to 142	18766667E-01	0.10120811E-02	42780742E-07	41	0.001695	6.37E-07
143 to 144	40630706E-01	0.98885825E-03	0.12512651E-06	40	0.001301	6.37E-07
145 to 145	0.90433855E-01	0.95596375E-03	0	6	0.000397	-
146 to 146	0.90433855E-01	0.95596375E-03	0	6	0.000397	-
147 to 147	0.90433855E-01	0.95596375E-03	0	6	0.000397	-

stn no.	(F <sub>2</sub> + F <sub>3</sub> . N)	stn no.	(F <sub>2</sub> + F <sub>3</sub> . N)	stn no.	(F <sub>2</sub> + F <sub>3</sub> . N)	stn no.	(F <sub>2</sub> + F <sub>3</sub> . N)
1	0.10266676E-02	41	0.10075419E-02	81	0.10062556E-02	121	0.10064310E-02
2	0.10266676E-02	42	0.10074373E-02	82	0.10067720E-02	122	0.10063570E-02
3	0.98776935E-03	43	0.10091704E-02	83	0.10067098E-02	123	0.10062829E-02
4	0.98487332E-03	44	0.10086648E-02	84	0.10066477E-02	124	0.10062482E-02
5	0.10051592E-02	45	0.10057035E-02	85	0.10068445E-02	125	0.10062418E-02
6	0.10052550E-02	46	0.10057009E-02	86	0.10068289E-02	126	0.10062355E-02
7	0.10053508E-02	47	0.10056983E-02	87	0.10068134E-02	127	0.10062291E-02
8	0.10031503E-02	48	0.10054845E-02	88	0.10067978E-02	128	0.10062227E-02
9	0.10079131E-02	49	0.10055595E-02	89	0.10063182E-02	129	0.10062164E-02
10	0.10078712E-02	50	0.10056346E-02	90	0.10062476E-02	130	0.10086765E-02
11	0.10073879E-02	51	0.10057096E-02	91	0.10061770E-02	131	0.10087830E-02
12	0.10073972E-02	52	0.10062251E-02	92	0.10062705E-02	132	0.10088894E-02
13	0.10074065E-02	53	0.10061952E-02	93	0.10063001E-02	133	0.10068369E-02
14	0.10074158E-02	54	0.10061653E-02	94	0.10060709E-02	134	0.10067516E-02
15	0.10074251E-02	55	0.10064570E-02	95	0.10060633E-02	135	0.10073576E-02
16	0.10074344E-02	56	0.10065080E-02	96	0.10060557E-02	136	0.10074591E-02
17	0.10074437E-02	57	0.10065590E-02	97	0.10051090E-02	137	0.10075606E-02
18	0.10058631E-02	58	0.10061532E-02	98	0.10051368E-02	138	0.10068183E-02
19	0.10060253E-02	59	0.10061421E-02	99	0.10051647E-02	139	0.10067761E-02
20	0.10068021E-02	60	0.10061310E-02	100	0.10075206E-02	140	0.10067340E-02
21	0.10068297E-02	61	0.10072986E-02	101	0.10072596E-02	141	0.10060490E-02
22	0.10068573E-02	62	0.10073090E-02	102	0.10066040E-02	142	0.10060063E-02
23	0.10068849E-02	63	0.10058447E-02	103	0.10065782E-02	143	0.10067513E-02
24	0.10069125E-02	64	0.10056914E-02	104	0.10065524E-02	144	0.10068765E-02
25	0.10070214E-02	65	0.10063770E-02	105	0.10065266E-02	145	0.95596375E-03
26	0.10069493E-02	66	0.10060185E-02	106	0.10065008E-02	146	0.95596375E-03
27	0.10068771E-02	67	0.10055564E-02	107	0.10062606E-02	147	0.95596375E-03
28	0.10066903E-02	68	0.10054471E-02	108	0.10062055E-02		
29	0.10067751E-02	69	0.10063026E-02	109	0.10068043E-02		
30	0.10068600E-02	70	0.10062720E-02	110	0.10066792E-02		
31	0.10070999E-02	71 70	0.10062413E-02	111	0.10071260E-02		
32	0.10070499E-02	72	0.10062107E-02	112	0.10071301E-02		
33	0.10069999E-02	73	0.10061800E-02	113	0.10071341E-02		
34	0.10059549E-02	74 75	0.10061494E-02	114	0.10071382E-02		
35	0.10057289E-02	75 76	0.10084584E-02	115	0.10071422E-02		
36	0.10062190E-02	76 77	0.10084753E-02	116	0.10071463E-02		
37 38	0.10061365E-02 0.10058313E-02	77 78	0.10062154E-02 0.10061325E-02	117	0.10080803E-02 0.10080818E-02		
39	0.10058515E-02	76 79	0.10061325E-02 0.10060495E-02	118 119	0.10080818E-02		
39 40	0.10058515E-02 0.10058717E-02	79 80	0.10060495E-02 0.10062640E-02	120	0.10080847E-02		
40	0.10030717E-02	80	U.1UUU∠U4U⊏-UZ	120	0.10000041E-02		

<u>Table 2.12:</u> CTD raw data scans flagged for special treatment (see previous data reports for explanation).

station	approximate	raw scan	action	reason
number	pressure (dbar)	numbers	taken	
4(downcas	st) 286	22602-22953	ignore	fouling of cond. cell
7(downcas	st) 146	10608-10626	ignore	bad data scans
145(upcast)	)	571-579,730-741,799-802	ignore	bad pressure data
145(upcast)	)	855-858,1137-1140,1404-1408	3 ignore	bad pressure data
145(upcast)	)	2218-2236,2872-2879	ignore	bad pressure data
145(upcast)	)	5607-5612,5703-5711	ignore	bad pressure data
146(upcast)	)	3097-3100,3151-3155,3260-32	263 ignore	bad pressure data
146(upcast)	)	3286-3298,3334-3337,3388-33	390 ignore	bad pressure data
146(upcast)	)	3421-3425,3442-3445,3477-34	480 ignore	bad pressure data
147(upcast)	)	3036-3039,3142-3146,3158-3	163 ignore	bad pressure data
147(upcast)	)	3210-3213	ignore	bad pressure data

<u>Table 2.13:</u> Missing data points in 2 dbar-averaged files. "1" indicates missing data for the indicated parameters: T=temperature; S=salinity,  $\sigma_T$ , specific volume anomaly and geopotential anomaly; O=dissolved oxygen; PAR=photosynthetically active radiation; F=fluorescence. Note that jmin is the minimum number of data points required in a 2 dbar bin to form the 2 dbar average (see CTD methodology).

station number	pressures (dbar) where data missing	Т	S	0	PAR	F	reason
1	entire profile			1			no bottles for oxygen calibration
2	entire profile		1	1			no bottles for calibration
3	entire profile			1			bad oxygen data
3	3924	1	1	1	1		no. of data pts in 2 dbar bin < jmin
4,5	entire profile			1			no bottles for oxygen calibration
8	2	1	1	1	1		CTD not logging
13	618	1	1	1	1		no. of data pts in 2 dbar bin < jmin
16,21,29	entire profile			1			no bottles for oxygen calibration
17	entire profile			1			bad oxygen data
20	2852-2864			1			bad oxygen data
26	2-58			1			bad oxygen data
35	448	1	1	1	1		no. of data pts in 2 dbar bin < jmin
38	1210	1	1	1	1		no. of data pts in 2 dbar bin < jmin
40	522	1	1	1	1		no. of data pts in 2 dbar bin < jmin
41	2-16			1			bad oxygen data
43	entire profile			1			no bottles for oxygen calibration
43	100	1	1	1	1		no. of data pts in 2 dbar bin < jmin
44	2032-2104		1				fouling of cond. cell
44	entire profile			1			bad oxygen data
60	entire profile			1			no bottles for oxygen calibration
62	2	1	1	1			bad data
62	950	1	1	1	1		no. of data pts in 2 dbar bin < jmin
62	952			1			bad oxygen data
64	932-946		1				fouling of cond. cell
65,77	entire profile			1			no bottles for oxygen calibration
72	1832	1	1	1	1		no. of data pts in 2 dbar bin < jmin
74	18-28			1			bad oxygen data
75	2542	1	1	1	1		no. of data pts in 2 dbar bin < jmin
79	2-72	=	-	1	•		bad oxygen data
82	2	1	1	•			bad data

Table 2.13: (continued)

station number	pressures (dbar) where data missing	Т	S	0	PAR	F	reason
83 89 92 97 98 123 133 134 141 81-144 145 146,147 147 1-3,14-33 35 36-147	438 2 3518 3888 2110-3106 1904-2180 3952 3926 1804 entire profile 326,374,428 entire profile 2-24 entire profile entire profile entire profile	1 1 1 1 1 1 1	1 1 1 1 1 1 1	1 1 1 1 1 1 1	1 1 1	1 1 1	no. of data pts in 2 dbar bin < jmin CTD not logging no. of data pts in 2 dbar bin < jmin no. of data pts in 2 dbar bin < jmin fouling of cond. cell fouling of cond. cell no. of data pts in 2 dbar bin < jmin no. of data pts in 2 dbar bin < jmin no. of data pts in 2 dbar bin < jmin no. of data pts in 2 dbar bin < jmin had oxygen data bad oxygen data had oxygen data no bottles for oxygen calibration fouling of cond. cell fluorometer not installed bad fluorometer data fluorometer not installed
						-	

 $\underline{\textbf{Table 2.14:}} \ \ \textbf{2 dbar averages interpolated from surrounding 2 dbar values, for the indicated parameters.}$ 

station number	interpolated 2 dbar values	parameters interpolated
2	3320	T, PAR
133	1482	T, S, PAR
135	1986	T, S, PAR

Table 2.15a: Suspect 2 dbar salinity averages (+ temperature where indicated). Note: for suspect salinity values, the following are also suspect:  $\sigma_T$ , specific volume anomaly, and geopotential anomaly.

station	suspect 2 dl	oar values (dbar)	reason	
number	bad	questionable		
3	-	66	salinity spike in steep local gradient	
4	-	64,66	salinity spike in steep local gradient	
9	-	138	bad data scans	
11	-	36,38	salinity spike in steep local gradient	
13	-	52,54	salinity spike in steep local gradient	
15	-	600	salinity spike in steep local gradient	
17	-	198,200	salinity spike in steep local gradient	
18	-	150,152	salinity spike in steep local gradient	
20	-	2856-2870	possible fouling of conductivity cell	
21	-	48	salinity spike in steep local gradient	
22	-	52,54	salinity spike in steep local gradient	
30	-	8,10	salinity spike in steep local gradient	
32	-	170	salinity spike in steep local gradient	
36	-	46	salinity spike in steep local gradient	
39	-	12,14	salinity spike in steep local gradient	
46	-	44,46	salinity spike in steep local gradient	
59	-	42,44	salinity spike in steep local gradient	
61	-	40,42	salinity spike in steep local gradient	
62	-	952	possible fouling of conductivity cell	
63	-	108,110	salinity spike in steep local gradient	
70	-	14-20	salinity spike in steep local gradient	
80	-	32,34	salinity spike in steep local gradient	
85	-	36	salinity spike in steep local gradient	
93	-	34,64,66	salinity spike in steep local gradient	
94	-	34,42-52	salinity spike in steep local gradient	
97	-	38,56	salinity spike in steep local gradient	
98	-	34,36	salinity spike in steep local gradient	
99	-	44,46	salinity spike in steep local gradient	
104	-	36,38	salinity spike in steep local gradient	
107	-	38	salinity spike in steep local gradient	
109	-	32,34,138,168	salinity spike in steep local gradient	
110	-	32	salinity spike in steep local gradient	
111	-	40-44	salinity spike in steep local gradient	
112	-	52-56	salinity spike in steep local gradient	
113	-	42	salinity spike in steep local gradient	
114	-	50-54	salinity spike in steep local gradient	
117	-	54-58	salinity spike in steep local gradient	
118	-	64	salinity spike in steep local gradient	
119	-	56	salinity spike in steep local gradient (T	also)
120	-	48-52	salinity spike in steep local gradient	
129	-	696	salinity spike in steep local gradient	
133	-	64,66	salinity spike in steep local gradient	
137	-	62,64	salinity spike in steep local gradient	
140	-	56,58,126	salinity spike in steep local gradient	
142	-	34,36	salinity spike in steep local gradient	

<u>Table 2.15b:</u> Suspect 2 dbar-averaged data from near the surface (applies to all parameters other than dissolved oxygen, except where noted).

No.   bad   questionable   No.   bad   questionable   Such a	stn s		2dbar values			dbar values
5         2,4         -         68         2-60         - (Tokay)           6,7         -         2         69         2,4         6           8         -         4         70,71         -         2           10         -         2 (Tokay)         74,75         2         4           11,12         -         2         76         -         2-6           13         2         4         79         -         2           14         2,4         6         80         2         4           15         -         2         82         -         4           16         2         4,6         83         -         2           17         -         2,4         84,85         2         4           18,19         -         2         86         -         2           20         -         2,6         87         -         2,4           21         -         2,4         90         -         2           22         -         2         91         2         4           22         -         2         96,97         -			- T			<u>questionable</u>
6,7 - 2			4			-
8 - 4 70,71 - 2 10 - 2 (Tokay) 74,75 2 4 11,12 - 2 76 - 2-6 13 2 4 79 - 2 14 2,4 6 80 2 4 15 - 2 82 - 4 16 2 4,6 83 - 2 17 - 2,4 84,85 2 4 18,19 - 2 86 - 2 20 - 2-6 87 - 2,4 21 - 2,4 90 - 2 22 - 4 (Tokay) 92 - 2,4 22 - 4 (Tokay) 92 - 2 24 2 2 4 100,101 - 2 29 - 2 102 2 4,6 31 2 4 103 - 2 32,33 - 2 104 - 2,4 34 - 6 (Tokay) 106,107 - 2,4 35 - 6 (Tokay) 106,107 - 2,4 35 - 2,4 110,111 - 2,4 39 - 2 112 2 4 40 - 2,4 (Tokay) 113 - 2 44,45 - 2,4 116-118 - 2 44,45 - 2,4 116-118 - 2 49 - 2,4 (Tokay) 113 - 2 44,45 - 2,4 116-118 - 2 49 - 2,4 (Tokay) 113 - 2 44,45 - 2,4 116-118 - 2 44,45 - 2,4 116-118 - 2 44,45 - 2,4 116-118 - 2 44,45 - 2,4 116-118 - 2 44,45 - 2,4 116-118 - 2 44,45 - 2,4 116-118 - 2 44,45 - 2,4 116-118 - 2 47,4 116-118 - 2 48,5 2 - 126 2 123 - 2,4 48,6 3 2 4 116-118 - 2 49 - 2,4 (Tokay) 113 - 2 40 - 2,4 (Tokay) 113 - 2 41,42 - 2,4 114 (Tokay) 126 2 4 46-48 - 2 120 - 2 49 - 2,4 121 2 4 41,41 - 2,4 124 - 2 49 - 2,4 121 2 4 41,42 - 2,4 121 2 4 42,4 124 - 2 43 2 4 116-118 - 2 44,45 - 2,4 121 2 4 46-48 - 2 120 - 2 49 - 2,4 121 2 4 46-48 - 2 120 - 2 49 - 2,4 121 2 4 46-48 - 2 120 - 2 49 - 2,4 121 2 4 46-48 - 2 120 - 2 127 2 - 125 - 2,4 127 2 - 125 - 2,4 127 2 - 125 - 2,4 127 2 - 125 - 2,4 127 2 - 125 - 2,4 127 2 - 125 - 2,4 127 2 - 125 - 2,4 127 2 - 125 - 2,4 128 2 4 139 - 2,4 129 - 2,4 131 - 2 132 2 4 131 - 2 133 2 4,6 134 - 2,4 135 - 2,6 136 2 4 136,137 - 2 138 - 2,4 139 - 2 140 - 2,4 141,142 - 2 140 - 2,4 141,142 - 2 140 - 2,4 141,142 - 2 140 - 2,4 140 - 2,4		2,4				
10 - 2 (Tokay) 74,75 2 4 11,12 - 2 76 - 2-6 13 2 4 79 - 2 14 2,4 6 80 2 4 15 - 2 82 - 4 16 2 4,6 83 - 2 17 - 2,4 84,85 2 4 18,19 - 2 86 - 2 20 - 2-6 87 - 2,4 21 - 2,4 90 - 2 22 - 2 91 2 4 22 - 2 91 2 4 22 - 2 96,97 - 2 26 2 4-8 98,99 2 4 27 2 4 100,101 - 2 29 - 2 102 2 4,6 31 2 4 27 2 4 100,101 - 2 29 - 2 102 2 4,6 31 3 2 4 32,33 - 2 104 - 2,4 34 - 6 (Tokay) 105 - 2 31 2 4 103 - 2 32,33 - 2 104 - 2,4 34 - 6 (Tokay) 106,107 - 2,4 35 - 6 (Tokay) 106,107 - 2,4 36,37 - 2 110,111 - 2,4 39 - 2 112 2 4 40 - 2,4 (Tokay) 113 - 2 41,42 - 2,4 (Tokay) 113 - 2 41,42 - 2,4 (Tokay) 113 - 2 44,45 - 2,4 (Tokay) 113 - 2 44,45 - 2,4 (Tokay) 113 - 2 41,42 - 2,4 (Tokay) 113 - 2 44,45 - 2,4 (Tokay) 113 - 2 45 - 2,4 (Tokay) 113 - 2 47 - 2,4 (Tokay) 113 - 2 48 - 2,4 (Tokay) 113 - 2 49 - 2,4 (Tokay) 113 - 2 40 - 2,4 (Tokay) 113 - 2 41,42 - 2,4 (Tokay) 113 - 2 41,42 - 2,4 (Tokay) 113 - 2 41,43 - 2,4 (Tokay) 113 - 2 41,44 - 2,4 (Tokay) 113 - 2 41,45 - 2,4 (Tokay) 113 - 2 41,47 - 2,4 (Tokay) 126 2 4 41,48 - 2,4 (Tokay) 126 2 4 41,49 - 2,4 (Tokay) 126 2 4 41,41 - 2,4 (Tokay) 126 2 4 41,41 - 2,4 (Tokay) 128		-			2,4	
11,12 - 2 4 76 - 2-6 13 2 4 79 - 2 14 2,4 6 80 2 4 15 - 2 82 - 4 16 2 4,6 83 - 2 17 - 2,4 84,85 2 4 18,19 - 2 86 - 2,4 21 - 2,4 90 - 2 22 - 2 91 2 4 22 - 2 91 2 4 22 - 2 94 - 2 23 - 2 94 - 2 24 2 - 96,97 - 2 26 2 4-8 98,99 2 4 27 2 4 100,101 - 2 29 - 2 102 2 4,6 31 2 4 103 - 2 32,33 - 2 104 - 2,4 34 - 6 (T okay) 106,107 - 2,4 35 - 2,4 108 2 4 36,37 - 2 34 - 6 (T okay) 106,107 - 2,4 35 - 2,4 108 2 4 36,37 - 2 40 - 2,4 (T okay) 113 - 2,4 43 2 4 116-118 - 2 40 - 2,4 (T okay) 113 - 2 44,45 - 2,4 119 - 2,4 44,45 - 2,4 119 - 2,4 46-48 - 2 120 - 2 49 - 2,4 119 - 2,4 46-48 - 2 49 - 2,4 119 - 2,4 46-48 - 2 49 - 2,4 119 - 2,4 46-48 - 2 49 - 2,4 119 - 2,4 46-48 - 2 49 - 2,4 119 - 2,4 46-48 - 2 49 - 2,4 119 - 2,4 46-48 - 2 49 - 2,4 119 - 2,4 46-48 - 2 49 - 2,4 119 - 2,4 46-48 - 2 49 - 2,4 119 - 2,4 46-48 - 2 49 - 2,4 119 - 2,4 46-48 - 2 49 - 2,4 119 - 2,4 46-48 - 2 49 - 2,4 119 - 2,4 46-48 - 2 49 - 2,4 119 - 2,4 46-48 - 2 49 - 2,4 119 - 2,4 46-48 - 2 49 - 2,4 119 - 2,4 46-48 - 2 49 - 2,4 119 - 2,4 46-48 - 2 49 - 2,4 121 2 4 40 - 2,4 131 - 2 55 - 2,4 132 - 2,4 55 2 - 130 2 4,6 56 2 4 131 - 2 57 - 2,4 132 - 2,4 58,59 - 2 58,59 - 2 59 - 2 133 2 4,6 50 - 2 (T okay) 134 - 2,4 56 2 4 139 - 2 56 2 4 139 - 2 56 2 4 139 - 2 56 2 4 139 - 2 56 2 4 139 - 2 56 2 4 139 - 2 56 2 4 139 - 2 56 2 4 139 - 2 56 2 4 139 - 2 56 2 4 139 - 2 56 2 4 130 - 2,4 57 - 2,4 138 - 2,4 58,59 - 2 58 2 4 136,137 - 2 59 2 4 130 - 2,4 59 2 138 - 2,4 59 2 138 - 2,4 59 2 138 - 2,4 59 2 138 - 2,4 59 2 140 - 2,4		-				
13       2       4       79       -       2         14       2,4       6       80       2       4         15       -       2       82       -       4         16       2       4,6       83       -       2         17       -       2,4       84,85       2       4         18,19       -       2       86       -       2         20       -       2-6       87       -       2,4         21       -       2-6       87       -       2,4         21       -       2,4       90       -       2         22       -       4       (T okay)       92       -       2,4         23       -       2       94       -       2         24       2       -       96,97       -       2         26       2       4-8       98,99       2       4         27       2       4       100,101-       2       2         29       -       2       104       -       2,4         31       2       4       105       -       2		-		,	2	
14		-			-	
15         -         2         4,6         83         -         2           17         -         2,4         84,85         2         4           18,19         -         2         86         -         2           20         -         2-6         87         -         2,4           21         -         2,4         90         -         2           22         -         2         91         2         4           22         -         2         94         -         2           24         2         -         96,97         -         2           26         2         4-8         98,99         2         4           27         2         4         100,101         2         2           29         -         2         102         2         4,6         31         2         4         103         -         2         4         6         7         2,4         4         103         -         2         4,6         31         2         2,4         103         -         2         2,4         34         105         -         2						
16       2       4,6       83       -       2         17       -       2,4       84,85       2       4         18,19       -       2       86       -       2         20       -       2-6       87       -       2,4         21       -       2,4       90       -       2         22       -       2       91       2       4         22       -       2       94       -       2         24       2       -       96,97       -       2         24       2       -       96,97       -       2         26       2       4-8       98,99       2       4         27       2       4       100,101       2       2         29       -       2       102       2       4,6         31       2       4       103       -       2         32,33       -       2       104       -       2,4         34       -       6 (Tokay)       106,107       2       2,4         35       -       6 (Tokay)       109       2       4		2,4			2	
17 - 2,4 84,85 2 4 18,19 - 2 86 - 2 20 - 2-6 87 - 2,4 21 - 2,4 90 - 2 22 - 2 91 2 4 22 - 4 (T okay) 92 - 2,4 23 - 2 96,97 - 2 26 2 4-8 98,99 2 4 27 2 4 100,101 - 2 29 - 2 102 2 4,6 31 2 4 103 - 2 32,33 - 2 104 - 2,4 34 - 2,4 105 - 2 34 - 6 (T okay) 106,107 - 2,4 35 - 2,4 108 2 4 35 - 6 (T okay) 109 2 4 36,37 - 2 110,111 - 2,4 39 - 2 110,111 - 2,4 39 - 2 110,111 - 2,4 39 - 2 110,111 - 2,4 43 2 4 116,118 - 2 44,45 - 2,4 114,115 - 2,4 43 2 4 116,118 - 2 44,45 - 2,4 119 - 2,4 46-48 - 2 120 - 2 49 - 2,4 (T okay) 113 - 2 41,42 - 2,4 114,115 - 2,4 43 2 4 116,118 - 2 44,45 - 2,4 119 - 2,4 46-48 - 2 120 - 2 49 - 2,4 (T okay) 126 2 4 50 - 2 123 - 2,4 51 - 2,4 124 - 2 52 2 - 123 - 2,4 51 - 2,4 124 - 2 52 2 - 123 - 2,4 51 - 2,4 124 - 2 52 2 - 123 - 2,4 51 - 2,4 124 - 2 52 2 - 123 - 2,4 51 - 2,4 124 - 2 52 2 - 123 - 2,4 51 - 2,4 124 - 2 52 2 - 123 - 2,4 51 - 2,4 124 - 2 52 2 - 133 2 4,6 56 2 4 131 - 2 57 - 2,4 132 - 2,4 58,59 - 2 133 2 4,6 66 6 135 - 2-6 63 2 4 136,137 - 2 66 - 2 (T okay) 134 - 2,4 66 - 2 138 - 2,4 66 - 2 140 - 2,4 66 - 2 140 - 2,4 66 - 2 140 - 2,4 66 - 2 140 - 2,4 66 - 2 140 - 2,4 66 - 2 140 - 2,4					-	
18,19       -       2       86       -       2         20       -       2-6       87       -       2,4         21       -       2,4       90       -       2         22       -       2       91       2       4         22       -       4 (Tokay)       92       -       2,4         23       -       2       94       -       2         24       2       -       96,97       -       2         26       2       4-8       98,99       2       4         27       2       4       100,101       2       2         29       -       2       102       2       4,6         31       2       4       103       -       2         32,33       -       2       104       -       2,4         34       -       2,4       105       -       2         34       -       6 (Tokay)       106,107       -       2,4         35       -       2,4       108       2       4         36,37       -       2       112,111       2       4     <		2			-	
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35       -       6 (T okay)       109       2       4         36,37       -       2       110,111 -       2,4         39       -       2       112       2       4         40       -       2,4 (T okay)       113       -       2         41,42       -       2,4       114,115 -       2,4         43       2       4       116-118 -       2         44,45       -       2,4       119       -       2,4         46-48       -       2       120       -       2         49       -       2,4       121       2       4         50       -       2       123       -       2,4         51       -       2,4       124       -       2         52       2       -       125       -       2,4         52       2       -       125       -       2,4         53       2       -       127       2       -         53       2       -       127       2       -         53       2       -       130       2       4,6         55		-				
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46-48       -       2       120       -       2         49       -       2,4       121       2       4         50       -       2       123       -       2,4         51       -       2,4       124       -       2         52       2       -       125       -       2,4         52       -       4-14 (T okay)       126       2       4         53       2       -       127       2       -         53       -       4-14 (T okay)       128       2       4         54       2       4       129       -       2,4         55       2       -       130       2       4,6         56       2       4       131       -       2         57       -       2,4       132       -       2,4         58,59       -       2       133       2       4,6         60       -       2 (T okay)       134       -       2,4         62       4       6       135       -       2-6         63       2       4       136,137       -       2<					_	
49       -       2,4       121       2       4         50       -       2       123       -       2,4         51       -       2,4       124       -       2         52       2       -       125       -       2,4         52       -       4-14 (T okay)       126       2       4         53       2       -       127       2       -         53       -       4-14 (T okay)       128       2       4         54       2       4       129       -       2,4         55       2       -       130       2       4,6         56       2       4       131       -       2         57       -       2,4       132       -       2,4         58,59       -       2       133       2       4,6         60       -       2 (T okay)       134       -       2,4         62       4       6       135       -       2-6         63       2       4       136,137       -       2         64       -       2       138       -       2,4 </td <td></td> <td>_</td> <td></td> <td></td> <td>_</td> <td></td>		_			_	
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51       -       2,4       124       -       2         52       2       -       125       -       2,4         52       -       4-14 (T okay)       126       2       4         53       2       -       127       2       -         53       -       4-14 (T okay)       128       2       4         54       2       4       129       -       2,4         55       2       -       130       2       4,6         56       2       4       131       -       2         57       -       2,4       132       -       2,4         58,59       -       2       133       2       4,6         60       -       2 (T okay)       134       -       2,4         62       4       6       135       -       2-6         63       2       4       136,137       -       2         64       -       2       138       -       2,4         65       2       4       139       -       2         66       -       2       140       -       2,4 <td></td> <td>_</td> <td></td> <td></td> <td>-</td> <td></td>		_			-	
52       2       -       125       -       2,4         52       -       4-14 (T okay)       126       2       4         53       2       -       127       2       -         53       -       4-14 (T okay)       128       2       4         54       2       4       129       -       2,4         55       2       -       130       2       4,6         56       2       4       131       -       2         57       -       2,4       132       -       2,4         58,59       -       2       133       2       4,6         60       -       2 (T okay)       134       -       2,4         62       4       6       135       -       2-6         63       2       4       136,137       -       2         64       -       2       138       -       2,4         65       2       4       139       -       2         66       -       2       140       -       2,4         66       -       4-18 (T okay)       141,142       -		_			_	
52       -       4-14 (T okay)       126       2       4         53       2       -       127       2       -         53       -       4-14 (T okay)       128       2       4         54       2       4       129       -       2,4         55       2       -       130       2       4,6         56       2       4       131       -       2         57       -       2,4       132       -       2,4         58,59       -       2       133       2       4,6         60       -       2 (T okay)       134       -       2,4         62       4       6       135       -       2-6         63       2       4       136,137       -       2         64       -       2       138       -       2,4         65       2       4       139       -       2         66       -       2       140       -       2,4         66       -       4-18 (T okay)       141,142       -       2		2	_, ·		_	
53       2       -       127       2       -         53       -       4-14 (T okay)       128       2       4         54       2       4       129       -       2,4         55       2       -       130       2       4,6         56       2       4       131       -       2         57       -       2,4       132       -       2,4         58,59       -       2       133       2       4,6         60       -       2 (T okay)       134       -       2,4         62       4       6       135       -       2-6         63       2       4       136,137       -       2         64       -       2       138       -       2,4         65       2       4       139       -       2         66       -       2       140       -       2,4         66       -       4-18 (T okay)       141,142       -       2		_	4-14 (T okav)		2	
53       -       4-14 (T okay)       128       2       4         54       2       4       129       -       2,4         55       2       -       130       2       4,6         56       2       4       131       -       2         57       -       2,4       132       -       2,4         58,59       -       2       133       2       4,6         60       -       2 (T okay)       134       -       2,4         62       4       6       135       -       2-6         63       2       4       136,137       -       2         64       -       2       138       -       2,4         65       2       4       139       -       2         66       -       2       140       -       2,4         66       -       4-18 (T okay)       141,142       -       2		2	-			
54       2       4       129       -       2,4         55       2       -       130       2       4,6         56       2       4       131       -       2         57       -       2,4       132       -       2,4         58,59       -       2       133       2       4,6         60       -       2 (T okay)       134       -       2,4         62       4       6       135       -       2-6         63       2       4       136,137       -       2         64       -       2       138       -       2,4         65       2       4       139       -       2         66       -       2       140       -       2,4         66       -       4-18 (T okay)       141,142       -       2		_	4-14 (T okav)			4
55       2       -       130       2       4,6         56       2       4       131       -       2         57       -       2,4       132       -       2,4         58,59       -       2       133       2       4,6         60       -       2 (T okay)       134       -       2,4         62       4       6       135       -       2-6         63       2       4       136,137       -       2         64       -       2       138       -       2,4         65       2       4       139       -       2         66       -       2       140       -       2,4         66       -       4-18 (T okay)       141,142       -       2		2			_	
56       2       4       131       -       2         57       -       2,4       132       -       2,4         58,59       -       2       133       2       4,6         60       -       2 (T okay)       134       -       2,4         62       4       6       135       -       2-6         63       2       4       136,137       -       2         64       -       2       138       -       2,4         65       2       4       139       -       2         66       -       2       140       -       2,4         66       -       4-18 (T okay)       141,142       -       2			-		2	
57       -       2,4       132       -       2,4         58,59       -       2       133       2       4,6         60       -       2 (T okay)       134       -       2,4         62       4       6       135       -       2-6         63       2       4       136,137       -       2         64       -       2       138       -       2,4         65       2       4       139       -       2         66       -       2       140       -       2,4         66       -       4-18 (T okay)       141,142       -       2			4		-	
58,59       -       2       133       2       4,6         60       -       2 (T okay)       134       -       2,4         62       4       6       135       -       2-6         63       2       4       136,137       -       2         64       -       2       138       -       2,4         65       2       4       139       -       2         66       -       2       140       -       2,4         66       -       4-18 (T okay)       141,142       -       2		-	2,4		-	
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66 - 4-18 (T okay) 141,142 - 2		-			-	2,4
143,144 2 4	66	-	4-18 (T okay)			2
				143,144	2	4

Table 2.16: Suspect 2 dbar-averaged dissolved oxygen data.

stn suspect 2dbar values(dbar)			stn	suspect	2dbar values(dbar)
no.	bad	questionable	no.	bad	<u>questionable</u>
6	-	16-28	42	-	2-12
9	-	2-12,138,228	45	-	2
9	-	230,262,264	47	-	2,4
11	-	2	48	-	14-56
13	-	2-6	49	-	2-12
14	-	2,4	51	-	2-10
23	-	2-42	54	-	6-10
27	-	2-16	55	-	2-14
28	-	2-6,48-56	56	-	2
30	-	2-6	57	-	2,4
31	-	2-26,54-58	58	-	2-8
32	-	2	62	-	4-8,954-960
33	-	2-8	63	-	2-28
34	-	4-30	64	-	932-946
35	-	2-10	67	-	2,10-58
38	-	2-8,54-60	68	-	2-12
41	-	54-60	75	-	2

<u>Table 2.17:</u> CTD dissolved oxygen calibration coefficients.  $K_1$ ,  $K_2$ ,  $K_3$ ,  $K_4$ ,  $K_5$  and  $K_6$  are respectively oxygen current slope, oxygen sensor time constant, oxygen current bias, temperature correction term, weighting factor, and pressure correction term. dox is equal to 2.8 $\sigma$  (for  $\sigma$  as defined by eqn A2.24 in the CTD methodology); n is the number of samples retained for calibration in each station or station grouping.

	u u. uu		J Gag.	·· otatioii t	or oranion gro	~P		
station	$K_1$	$K_2$	$K_3$	$K_4$	$K_{\scriptscriptstyle{5}}$	$K_6$	dox n	
number	r							
1-5	-	-	-	-	-	-	-	-
6	7.418	5.00	-0.565	-0.06023	1.6962	-0.20179E-04	0.07725	7
7	6.872	5.00	-0.708	-0.13410	0.7181	0.24655E-03	0.14338	10
8	3.642	5.00	0.096	-0.12494	0.5941	-0.10229E-03	0.21158	11
9	7.093	5.00	-0.748	-0.11343	0.6713	0.89483E-04	0.23546	13
10	11.981	5.00	-1.621	-0.17472	0.9308	0.12612E-03	0.10240	17
11	6.451	5.00	-0.560	-0.14690	0.6141	0.67143E-04	0.10334	17
12	17.160	5.00	-2.450	-0.25734	1.0491	0.14873E-03	0.19673	24
13	20.289	5.00	-3.071	-0.25086	1.0967	0.17067E-03	0.19821	23
14	6.458	5.00	-0.699	-0.05269	0.2338	0.98041E-04	0.13005	23
15	14.242	5.00	-2.061	-0.16623	0.9724	0.14757E-03	0.20143	22
16-17	-	-	-	-	-	-	-	-
18	14.222	5.00	-2.049	-0.14751	1.0652	0.14078E-03	0.22139	22
19	8.206	5.00	-0.813	-0.17663	0.7010	0.61268E-04	0.21079	19
20	9.633	5.00	-1.285	-0.08468	0.7706	0.13244E-03	0.14319	20
21	-	-	-	-	-	-	-	-
22	14.502	5.00	-2.099	-0.16000	0.8689	0.14116E-03	0.22888	23
23	12.887	6.00	-1.907	-0.10053	0.8371	0.16632E-03	0.11743	22
24	13.362	5.00	-1.989	-0.11649	0.9941	0.20188E-03	0.24027	23
25	12.223	5.00	-1.746	-0.09636	0.8988	0.15115E-03	0.15767	21
26	9.611	5.00	-1.041	-0.25649	0.7004	0.80656E-04	0.25574	22
27	7.947	5.00	-0.957	-0.09613	0.6344	0.11430E-03	0.17697	24
28	12.035	5.00	-1.684	-0.15714	0.6915	0.13169E-03	0.29089	24
29	-	-	-	-	-	-	-	-

Table 2.17: (continued)

station number	Κ <sub>1</sub>	K <sub>2</sub>	K <sub>3</sub>	K <sub>4</sub>		K <sub>5</sub>	K <sub>6</sub>	dox r	1
30	11.283	5.00	1 500	-0.11215		0.5598	0.12912E-03	0.15112	24
31	10.148					0.3398	0.12912E-03 0.13585E-03	0.13112	
			-1.384						
32	7.618			-0.04725		0.5352	0.11641E-03	0.16382	
33	35.331			-0.38808		1.0868	0.20304E-03	0.18587	
34	16.145			-0.16724		0.9970	0.18210E-03	0.18263	
35	13.675			-0.17720		0.9764	0.12958E-03	0.27098	
36	14.710			-0.19929		0.9144	0.14117E-03	0.23900	
37	18.358			-0.21192		0.9571	0.15181E-03	0.17370	
38	21.256		-3.387			0.8768	0.25256E-03	0.24543	
39	10.125			-0.12277			-0.16664E-04	0.24269	
40	8.252		-1.028			0.2829	0.22137E-03	0.20618	
41	13.477	5.00	-1.923	-0.14286		0.8308	0.18302E-03	0.09454	8
42	13.110	5.00	-1.792	-0.11370		0.9803	0.15074E-03	0.20964	12
43-44	-	-	-	-		-	-	-	-
45	8.231	5.00	-1.044	-0.09496		0.5569	0.12043E-03	0.14826	23
46	9.107	5.00	-1.227	-0.05124		0.3477	0.12590E-03	0.11759	24
47	14.485	5.00	-2.190	-0.12723		1.2218	0.18700E-03	0.12920	21
48	2.745	8.00	1.062	0.37630		0.0352	-0.12314E-03	0.13448	6
49	17.719	8.00	-2.755	-0.19351		1.0108	0.22516E-03	0.11148	9
50	14.718		-2.083			0.8862	0.15609E-03	0.14124	
51	12.666			-0.18490		0.8430	0.73093E-04	0.13368	
52	15.079		-2.041			0.8909	0.10585E-03	0.22428	
53	16.435		-2.359			0.9059	0.12835E-03	0.17349	
54	8.565		-1.023			0.5068	0.87403E-04	0.18297	
55	17.456		-2.586	-0.18771		0.9519	0.14376E-03	0.14614	
56	13.541			-0.17231		0.8238	0.11222E-03	0.18034	
57	17.585		-2.693			0.9900	0.16884E-03	0.19072	
58	8.252		-1.050	-0.10559		0.2405	0.110004E-03	0.13072	
59	12.812		-1.830	-0.04307		0.8256	0.11100E-03 0.13463E-03	0.17513	
60	-	-	-1.030	-0.11019		-	0.13403L-03	0.13343	-
61	- 15.443			-0.15869		0.7950	0.12621E-03	0.16280	
62	7.552			-0.13809			0.12021E-03 0.89890E-04	0.10200	
63	7.801		-0.872	-0.06247		0.3376	0.96123E-04	0.17730	
			-0.920			0.3663	0.96123E-04 0.10736E-03		
64 65	10.588		-1.423	-0.09551		0.4398	0.10/36E-03	0.10591	24
65 66	- 45 COZ	-	-	- 0 00040		- 0.7054	- 0.24000E.02	- 0.00004	-
66 67	15.627			-0.23340		0.7954	0.21008E-03	0.09261	
67	10.786			-0.12683		0.9951	0.14226E-03	0.17909	
68	13.291			-0.14946		0.8944	0.24323E-03	0.20779	
69 70	25.046			-0.26061		1.0344	0.20912E-03	0.14930	
70	15.205			-0.21336		0.8850	0.12566E-03	0.20667	
71	7.230			-0.22886		0.5820	0.37917E-04	0.21003	
72	11.370			-0.18495		0.7181	0.94158E-04	0.13537	
73	6.947			-0.08066		0.2406		0.14414	
74	15.394			-0.20745		0.9438		0.15400	
75	7.348			-0.04344		0.3395			
76	13.500	10.0		-0.06560		1.2992	0.19319E-03	0.11749	23
77	-	-	-	-		-	-	-	-
78	10.578			-0.04315			0.14700E-03	0.10303	
79	5.153			-0.08473			0.98564E-04		
80	11.496	10.0	-1.606	-0.08090		0.9995	0.14893E-03	0.07288	22
81-144	-	-	-	-		-	-	-	-
145	6.980	7.00	-0.716	-0.11934		0.5563	0.12412E-03	0.10894	9
146-14	7	-	-	-	-			-	-

<u>Table 2.18:</u> Starting values for CTD dissolved oxygen calibration coefficients prior to iteration, and coefficients varied during iteration (see CTD methodology). Note that coefficients not varied during iteration are held constant at the starting value.

station numbe	K <sub>1</sub>	K <sub>2</sub>	K <sub>3</sub>	$K_{4}$	<b>K</b> <sub>5</sub>	$K_6$	coe vari	efficients ed
1-5	_	_	_	_	_	-		-
6	9.100	5.0000	-0.200	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
7	6.600	5.0000	-0.800	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
8	6.600	5.0000	-1.100	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
9	12.400	5.0000	-1.700	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
10	11.700	5.0000	-1.400	-0.360E-01	0.750	0.15000E-03	K₁ K₁	$K_3 K_4 K_5 K_6$
11	6.700	5.0000	-0.600	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
12	9.300	5.0000	1.600	-0.360E-01	0.750	0.15000E-03	K₁ K₁	$K_3 K_4 K_5 K_6$
13	8.400	5.0000	0.400	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
14	8.300	5.0000	-0.100	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
15	11.300	5.0000	-2.400	-0.360E-01	0.750	0.15000E-03	K₁ K₁	$K_3 K_4 K_5 K_6$
16-17	-	-	-	-	-	-	• • • • •	-
18	10.500	5.0000	-2.500	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
19	8.200	5.0000	-0.700	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
20	9.550	5.0000	-1.300	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
21	-	-	-	-	-	-		
22	12.600	5.0000	-2.100	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
23	9.410	6.0000	-2.100	-0.360E-01	0.750	0.15000E-03	K₁ K₁	$K_3 K_4 K_5 K_6$
24	11.170	5.0000	-2.300	-0.300E-01	0.750	0.15000E-03	K₁ K₁	$K_3 K_4 K_5 K_6$
25	11.200	5.0000	-2.000	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
26	9.900	5.0000	-1.100	-0.450E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
27	9.300	5.0000	-0.700	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
28	12.600	5.0000	-1.400	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
29	-	-	-	-	-	-		
30	13.600	5.0000	-0.800	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
31	10.100	5.0000	-1.400	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
32	12.000	5.0000	0.000	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
33	9.100	5.0000	-2.300	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
34	13.330	5.0000	-2.300	-0.340E-01	0.750	0.15000E-03	K₁ ٰ	$K_{3}^{3} K_{4}^{4} K_{5}^{3} K_{6}^{6}$
35	12.000	5.0000	-2.000	-0.360E-01	0.750	0.15000E-03	K₁ ٰ	$K_{3}^{3} K_{4}^{4} K_{5}^{3} K_{6}^{6}$
36	14.400	5.0000	-1.900	-0.360E-01	0.750	0.15000E-03	K₁ ٰ	$K_{3}^{3} K_{4}^{4} K_{5}^{3} K_{6}^{6}$
37	7.500	5.0000	1.000	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_{3}^{3}K_{4}^{4}K_{5}^{3}K_{6}^{6}$
38	3.900	5.0000	0.500	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_{3}^{3} K_{4}^{4} K_{5}^{3} K_{6}^{6}$
39	7.900	5.0000	-1.300	-0.360E-01	0.750	0.15000E-03	K₁	$K_{3}^{3} K_{4}^{4} K_{5}^{3} K_{6}^{6}$
40	8.900	6.0000	-1.000	-0.360E-01	0.750	0.15000E-03	K₁⊓	$K_3 K_4 K_5 K_6$
41	12.400	5.0000	-2.100	-0.360E-01	0.750	0.15000E-03	K₁⊓	$K_3 K_4 K_5 K_6$
42	12.700	5.0000	-1.900	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
43-44	-	-	-	-	-	-	٠.	-
45	9.500	5.0000	-0.800	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
46	12.700	5.0000	-0.300	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
47	13.000	5.0000	-2.100	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
48	14.610	8.0000	-0.700	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
49	14.800	8.0000	-2.200	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
50	14.900	6.0000	-2.100	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
51	14.700	8.0000	-1.000	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
52	14.200	5.0000	-2.100	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
53	15.400	5.0000	-2.300	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
54	8.700	8.0000	-1.000	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
55	15.000	5.0000	-2.200	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
56	12.100	6.0000	-1.900	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
57	14.200	5.0000	-2.400	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$

Table 2.18: (continued)

station number	K <sub>1</sub>	K <sub>2</sub>	K <sub>3</sub>	K <sub>4</sub>	<b>K</b> <sub>5</sub>	K <sub>6</sub>	coe vari	efficients led
58 59 60	11.900 11.300	5.0000 5.0000	0.100 -2.100	-0.360E-01 -0.360E-01	0.750 0.750	0.15000E-03 0.15000E-03	K₁ K₁	$K_3 K_4 K_5 K_6 K_3 K_4 K_5 K_6$
61 62 63 64 65	13.750 8.400 11.000 11.200	8.0000 5.0000 5.0000 8.0000	-2.500 -0.700 -2.300 -1.300	-0.360E-01 -0.360E-01 -0.360E-01 -0.360E-01	0.750 0.750 0.750 0.750	0.15000E-03 0.15000E-03 0.15000E-03 0.15000E-03	K <sub>1</sub> K <sub>1</sub> K <sub>1</sub>	$\begin{array}{c} K_3 \; K_4 \; K_5 \; K_6 \\ K_3 \; K_4 \; K_5 \; K_6 \\ K_3 \; K_4 \; K_5 \; K_6 \\ K_3 \; K_4 \; K_5 \; K_6 \end{array}$
66 67 68 69 70 71 72 73 74 75 76	10.800 10.300 10.900 11.720 13.600 15.000 11.700 7.300 12.800 9.900 12.820	5.0000 5.0000 6.0000 5.0000 5.0000 5.0000 5.0000 8.0000 5.0000 10.0000	-1.700 -1.500 -2.300 -2.200 -2.300 -1.200 -1.300 -0.700 -1.800 -0.200 -2.300	-0.360E-01 -0.470E-01 -0.360E-01 -0.360E-01 -0.360E-01 -0.360E-01 -0.360E-01 -0.360E-01 -0.360E-01 -0.360E-01	0.750 0.750 0.750 0.750 0.750 0.750 0.750 0.750 0.750 0.750 0.750	0.15000E-03 0.15000E-03 0.15000E-03 0.15000E-03 0.15000E-03 0.15000E-03 0.15000E-03 0.15000E-03 0.15000E-03	K <sub>1</sub> K <sub>1</sub> K <sub>1</sub> K <sub>1</sub> K <sub>1</sub> K <sub>1</sub> K <sub>1</sub>	K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub>
77 78 79 80 81-144 145 146-147	- 10.600 6.500 14.500	5.0000 5.0000 10.0000 - 7.0000	-1.500 -0.300 -0.900 -	-0.360E-01 -0.360E-01 -0.600E-01 -	0.750 0.750 0.750 0.700 - 0.750	0.15000E-03 0.15000E-03 0.15000E-03 - 0.15000E-03	K₁ K₁ K₁	K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub> K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub> - - - K <sub>3</sub> K <sub>4</sub> K <sub>5</sub> K <sub>6</sub>

<u>Table 2.19:</u> Dissolved oxygen Niskin bottle samples flagged as -9 for dissolved oxygen calibration. Note that this does not necessarily indicate a bad bottle sample - in many cases, flagging is due to bad CTD dissolved oxygen data.

station	rosette	station	rosette
number	position	number	position
7	4	47	21,20,19
9	5	56	17
11	11	58	20
14	22	62	21,20
15	22,21	67	17
18	21,19	70	8
19	21,20,19,1	76	23
20	22,21,20	78	22
23	24	79	24,23,22
24	22	80	23,21
25	23,21,19		
26	22,20		
32	23		
34	24		
45	21		

<u>Table 2.20:</u> Questionable dissolved oxygen Niskin bottle sample values (not deleted from hydrology data file).

stn no.	rosette position
17	14
101	5,3

Table 2.21: Questionable nutrient sample values (not deleted from hydrology data file).

PHOSPHA	ATE	NITRAT	Έ	SILICAT	E
station number	rosette position	station number	rosette position	station number	rosette position
		12	9,8		
				24	7-17
26	6	26	6	26	6
34	22,11,7				
40	5				
				47	6,3
53	20				
				57	whole stn
58	12				
62	7				
74	whole stn				
		79	9-12		
				96	whole stn
		101	12		
118	5	118	5	118	5
		126	7		
		133	12		
		135	21		
144	3	144	10		

<u>Table 2.22:</u> Protected and unprotected reversing thermometers used (serial numbers are listed).

protected them station numbers 1 to 144 145 to 147	rosette position 24 thermometers 12095,12096 12095	rosette position 12 thermometers 12094 12094,12096	rosette position 2 thermometers 12119,12120 12119,12120
unprotected the station numbers 1 to 92 93 to 147	nermometers	rosette position 12 thermometers 11992 11993	rosette position 2 thermometers 11993 11992

<u>Table 2.23:</u> Calibration coefficients and calibration dates for CTD serial numbers 1103 and 1193 (unit nos 7 and 5 respectively) used during RSV Aurora Australis cruise AU9604. Note that an additional pressure bias term due to the station dependent surface pressure offset exists for each station (eqn A2.1 in the CTD methodology). Also note that platinum temperature calibrations are for the ITS-90 scale.

	CTD serial 1103	3 (unit no. 7)		CTD serial 119	3 (unit no. 5)
		value of coefficient		coefficient	value of coefficient
pressu	re calibration coe	fficients	pressur	e calibration coe	efficients
	Calibration Facil			Calibration Faci	
		-2.065725e+01		pcal0	-9.105560
	pcal1	1.002878e-01		pcal1	1.008189e-01
	pcal2	4.951104e-09		pcal2	2.773686e-10
	pcal3	4.500981e-14		pcal3	0.0
	pcal4	-4.514384e-19		pcal4	0.0
•	•	alibration coefficients			alibration coefficients
CSIRC	Calibration Facil		CSIRO	Calibration Faci	
	Tcal0	0.23396e-01		Tcal0	-0.46860e-01
	Tcal1	0.49983e-03		Tcal1	0.49879e-03
	Tcal2	0.35049e-11		Tcal2	0.27541e-11
pressu	re temperature ca	alibration coefficients	pressur	e temperature c	alibration coefficients
CSIRC	Calibration Facil	ity - 10/07/1996	CSIRO	Calibration Faci	lity - 09/11/1995
	Tpcal0	1.713678e+02		Tpcal0	1.167581e+02
		-4.239208e-03		Tpcal1	-2.450758e-03
	Tpcal2	1.481513e-08		Tpcal2	0.0
	Tpcal3	0.0		Tpcal3	0.0
coeffici	•	ure correction to coeffici	ents for t pressu	•	rection to
CSIRC	Calibration Facil	ity - 10/07/1996	CSIRO	Calibration Faci	lity - 09/11/1995

preliminary polynomial coefficients applied to fluorescence (fl) (Antarctic Division, January 1996) and photosynthetically active radiation (par) (supplied by manufacturer) raw digitiser counts for fluorometer set to 0-30 mg/m3 range (i.e. prior to 02/02/96):

20.00

-1.474830e-05

-7.847037e-02

f0 -3.345252e+01 f1 1.020700e-03 f2 0.0 fluorometer set to 0-10 mg/m3 range

for fluorometer set to 0-10 mg/m3 range (i.e. from 02/02/96 onwards):

f0 -1.115084e+01 f1 3.402400e-04 f2 0.0

20.00

-9.196843e-06

-7.818015e-02

par0 -4.499860

par1 1.373290e-04 par2 -3.452156e-23

## APPENDIX 2.1 Hydrochemistry Laboratory Report

Seawater samples were analysed for nutrient concentrations (nitrate plus nitrite, silicate, and phosphate), salinities, and dissolved oxygen concentrations. The methods used are described in Eriksen (1997). A new nutrient autoanalyser data logging system, methods of examining intra-run quality checks (tops), basic inter-run quality checks, and improved temperature control and monitoring were implemented on this cruise.

Number of samples analysed:

Nutrients (nitrate plus nitrite, silicate, phosphate): 2470

Salinities: 2500

Dissolved oxygens: 2450

#### A2.1.1 NUTRIENTS

#### General

The same TACS cadmium reduction coil was used for all but the first run.

Nitrate + nitrite and phosphate were calibrated with first order curves, and silicate with second order.

At the end of the cruise samples were run as part of the National Low Level Nutrient Collaborative Trials (NLLNCT).

Standards were made fresh every day. They were stored at around 4\_C between runs. Tops and nitrites were made fresh every couple of days, and were also stored at around 4 C.

#### New datalogging system

A new datalogging system was used for the first time, to replace the old DOS based 'DAPA' program. The system consisted of a Labtronics (Canada) 103 analogue to digital (A/D) board, and a Windows software package by Astoria-Pacific (USA), Faspac 1.2. Data was logged using both the Labtronics/Faspac system, and DAPA. The new program, while having some good points, was far from perfect, as summarised below. Many of the problems were to be fixed in later versions (1.30, 1.31).

## Some comments on Faspac

#### - Good Points

- \* Generally, easy and quick to get to different parts of the program, and to use; especially when compared to the awkwardness of DAPA.
- \* Real time display of the trace is good. It is easy to look at earlier parts of a run while the run is still in progress.
- \* The display and calculation of calibration standards is excellent. It is real time so this aspect of machine performance can be observed before samples are opened. It is easy to delete outliers, and to see how that affects the correlation of the fitted curve, and the standard deviation of the residual between calculated and observed points.

- \* Real time calculation of concentrations is good, so it's possible to see if sample concentrations look reasonable.
- \* Keeps track of the baseline reasonably well.
- \* Correcting the peak height position for spikes is easy (in contrast to DAPA).

#### - Fatal Points

- \* Crashes, from a number of different areas in different circumstances. A warning box stating that Windows has become unstable generally appears. Mostly time is lost, as data processing needs to be repeated.
- \* Crashes during a run with large sample numbers. Get a 'Peak Num = 6553' error message. Have lost data this way.
- \* Does not handle interpolation of multiple standards correctly.

#### - Bad Points

- \* Problems in 'peak search':
- -peak smoothing does not function.
- -does not always find top of peaks.

These work in peak search window, but do not work on real data. This is both during a run, or doing a 'rerun' of data.

- \* Starting Faspac causes an oscillating voltage, which is seen on the chart recorder. To reduce the problem, the following steps are performed:
- Stop run, save run, exit Faspac, close 'Data logger' program, restart data logger and Faspac, 'Resume' run.
- \* Doesn't write Excel files properly. On reading, Excel crashes ('General protection error'). Excel also had difficulty reading text files. Excel 4 was used.
- \* Doesn't have a mouse driven 'Zoom' function. It is possible to zoom in on peaks, but only by inefficiently varying the horizontal and vertical scales.
- \* It is not exactly clear how the special symbol 'W' is used to define the baseline. It depends on the context of other W's nearby.

## **Problems**

There was a problem with the A/D board (SN 35/91, 'original') at the mid-point voltage, where a 'glitch' was observed. It can be observed by looking at a ramped voltage input from a signal generator (see Figure A2.1.1). This affected a number of nitrate + nitrite values. The gain of the nitrate detector was reduced so that the maximum signal did not reach the voltage of the 'glitch'.

There was a problem with the phosphate channel. On a number of runs, high phosphate values were seen for seawater samples, but not for standards prepared in saline solution. The raw output for standards was the same for different runs, indicating that the seawater samples were being read as high. On the nitrate vs phosphate plot the phosphates were seen to be high, while the nitrates were about normal. The problem seemed to be correlated with ageing of ammonium molybdate stock solution. If fresh ammonium molybdate was used the problem seemed to be reduced. At the end of the cruise some nutrient trial samples were run. The results from these indicated that the phosphate channel was running reasonably well. Affected samples were rerun.

On the silicate channel, a precipitate in the ammonium molybdate reagent was observed a few days after preparation of fresh reagent. Generally the solution was replaced to reduce the risk of particles travelling through the system.

After a pump tube change there was no response from the nitrate channel. This was traced to a faulty blocked Bran and Luebe tube.

On run 7 Faspac crashed. No reliable results were produced for silicates, and only some results from the early part of the run for nitrates and phosphates. The nitrate and phosphate samples were rerun. Silicate, which does not store well, was calculated by hand from the chart. To verify that the hand and Faspac methods of calculation produced similar results, some of the usable nitrate results from Faspac were compared to hand calculated ones, with an average difference of around 0.6% (hand calculations larger).

## Tops

'Tops' are used as a check of changes in instrument responsiveness during a run. They are the same concentration as the top standard, but are made separately. They are placed at the start of a run and after every block of 12 samples.

The tops macro within A9604.XLM was used to extract tops from each \*.XLS run file, calculate statistics, and collate these statistics. The rsd % and range % for the nitrate + nitrite, silicate, and phosphate channels are shown in Figure A2.1.3.

The nitrate and phosphate channels had average ranges of 2.7% and 1.8% respectively. Variations in silicate were greater, with an average range of 4.2%. The silicates had about 20 runs with tops ranges greater than 5%. These 20 were examined, and some had obvious outliers, some appeared random, and about 7 had a time dependent drift. Examples of the worst cases of tops variations for the three channels are shown in Figure A2.1.4.

In general, correcting for tops variations could affect results by up to 1 - 4%. Corrections were not applied though, as the current method of placing tops does not allow for rigorous corrections to be made. The method of correcting for tops variation would have been to assume the first set of tops gives the correct value, and variation later in the run can be referenced to these. However, the first set of tops may not be correct, and false corrections could be made.

A better method would be to use the same solution for the top standard and for tops, and to run reference tops soon after the calibration curve. Thus an absolute concentration could reliably be placed on the tops, and corrections made by comparing tops to the nominal top value. Corrections would only be made once the error in the tops exceeded some set amount. This is because applying a correction between two points is likely to introduce a new source of error.

To get an idea of the sources of error, the error in the calibration curve was looked at for two randomly selected runs, 4 and 60. A total of four calibrations were looked at for nitrate + nitrite and phosphate. Second order calculations for silicate were not looked at. Of these four curves, for nitrate and phosphate, the maximum standard error of the slope was 0.6%, and the maximum standard error of the intercept was 1.9%. It was decided not to calculate the calibration errors for every run, thus they are not included in the total error of the samples for this cruise.

#### Quality checks

Batches of 30-40 deep seawater samples were taken to be used as quality checks to give an indication of instrument responsiveness between runs (Figure A2.1.5). Some were run fresh and the others stored frozen (Table A2.1.2). Once the value of a batch was established it could be used to see if a run and its calibration appeared normal. The QC macro in A9604.XLM was used to sort through the run \*.XLS files and extract the QC's. The QC names were prefixed by an 's'. As different batches were used this method could not effectively be used to compare runs throughout the cruise. Values could be normalised to the batch averages, but this is not likely to be reliable. Later cruises have used larger batches (~500 10ml tubes) of surface seawater.

## Nutrient data handling

The files produced by Faspac are \*.ACF. These contain the traces for all channels, settings information, calibration curves, and calculated concentrations. The original Faspac files were backed up as \*.NEW. This was important, as occasionally when Faspac crashed the previously saved copy of the file could not be worked on as it would soon crash, so it was necessary to start from original data.

Faspac produced a 'report', a spreadsheet format of nutrient concentrations. It is supposed to produce a format that can be read directly by Excel, however this format caused Excel to crash. The text format could not easily be parsed by Excel. Eventually, data was output as Lotus \*.WKS format, imported by Excel, and a macro used to convert the Lotus format to Excel format. Thus for every run there is an \*.ACF file, and a corresponding \*.XLS file containing the run sequence with concentrations calculated by Faspac.

The "Hydro" program was changed to process Faspac runs by reading \*.FAS files, extracting the sample number and concentration information, and calling the processed file \*.ACM. The information is stored in \*.DAT files, along with other data. Thus any \*.XLS files to be processed need to be copied as \*.FAS files. If only one station in a run is required for processing, then the data needs to be cut and pasted from the \*.XLS file into the \*.ACM file.

Which runs a particular station was run on is shown in Table A2.1.3. This also summarises the reason a station was repeated, and if the original or repeat run was used in the final data.

An attempt was made to observe the nutrient content of the saline solution in which standards were made up in. This was done only for the phosphate channel as it has the highest gain. A rise in the baseline was observed when switching from phosphate 'background' solution to phosphate 'colour' solution. This was attributed to phosphate in the saline solution from impurities in the original solid salt, although more work is needed to confirm it is due only to this, and not due to other contributions such as refractive index change. The value was around 0.006 µM. This value was assigned to the 'blank' in the calibration curve. It made very little impact on the final concentrations.

#### A2.1.2 DISSOLVED OXYGEN

The dissolved oxygen (D.O.) titration instrument was fairly reliable and determinations were generally within World Ocean Circulation Experiment (WOCE) guidelines. Exceptions are given below. Standardisations of sodium thiosulfate solution were within WOCE guidelines but improvements could be made by the addition of a second Dosimat unit. Blanks were not measured within WOCE guidelines.

#### Standardisations

The object of the standardisation procedure is to obtain "4 successive titres concordant to within 0.003 mL (of thiosulfate)." This was always achieved but was hampered by continual changing of the Dosimat exchange units. Often 7 or 8 titrations were required. This was time consuming and frustrating. Variations in the sodium thiosulphate titre were often due to bubble formation in the tubing of the exchange units. These are formed by the movement of the burette syringe on removal and replacement of the unit. A second Dosimat would make the standardisation simpler and faster. One unit would be used for the preparation of the standard solution while a titration was carried out on the second unit. Other advantages include:

- \* elimination of the need to continually exchange units reducing wear on the units, reducing the chance of dropping the unit in rough seas and preventing the formation of bubbles in the tubing;
- \* method may still be used on the cruise if one unit breaks down;
- \* stirring rate would remain the same for each titration (currently, the rate must be changed between preparation of the standard solution and the titration).

Potassium biiodate was added to the standard solution with the dV/dt knob set to 7.5. The rate is not specified in the current instruction manual. The rate could be set in the "DODO" software.

#### **Blank Determinations**

After concordant standardisation titres were obtained 5 blank determinations were made. These were not within WOCE guidelines. The blanks varied by 0.007 mL (of thiosulfate) for any set of 5 titrations. If 50 mL of water was used for the blank determination the titration did not work. This was increased to 60 mL and the titrations were successful. The measured variation in the blanks leads to an approximate error of 0.1% in the final results.

#### Samples

D.O. measurements in the samples were straightforward. Two or three repeats were measured for each crate of D.O. samples. The titre of the second determination was generally 0.003 - 0.006 mL (of thiosulfate) lower than the first. The greater the titre the greater the loss of volatile iodine.

After the addition of 1 mL of sulfuric acid to the sample the bottle required about 1 minute of shaking.

#### Instrumentation

The Dosimat seized up on two occasions. The first happened during the addition of 15 ml of potassium biiodate to the standard solution. This was a "time-out" error as the Dosimat was delivering the solution while the computer was trying to communicate with it. This was fixed by increasing the time the computer allowed for the addition from 20 to 40 seconds and by setting dV/Dt to 7.5. The second time the Dosimat seized up was when it was switched on when the computer was switched on. If the Dosimat was switched on after the "DODO" program was started this was not a problem.

The hydraulic ram was not used. It was more convenient to hold the sample bottles so the pipette tip was just off the bottom.

Standardisations are shown in Figure A2.1.6.

## A2.1.3 LABORATORIES

A number of work spaces were used. Nutrient and salinity analyses were performed in lab 3. The autoanalyser was set up on the forward bench, while the salinometer was set up on the outboard bench near the fume cupboard. Dissolved oxygen analysis and water purification took place in the photolab.

#### A2.1.4 TEMPERATURE MONITORING AND CONTROL

Laboratory temperature was recorded by two Tinytalk units, and measured by two mercury thermometers, an electronic thermometer, and the temperature monitor of the PID controller. An 'indoor/outdoor' electronic thermometer was used to measure fridge and freezer temperatures. One Tinytalk was positioned above the salinity crates for the duration of analysis, the other was moved around for shorter checks. One mercury thermometer was positioned above the salinity crates, the other with the DO instrumentation. An electronic thermometer was also used for spot checks. All the temperature measuring devices were placed together at the start of the cruise. The PID temperature was calibrated, and the devices agreed to within 0.5 C.

The long term Tinytalk recorded 1800 temperature points at 48 minute intervals. The file is A9604L.DTF, and the numbers have been exported to A9604L.XLS. The average temperature was 19.6 +/- 0.4 \_C. See Figure A2.1.2 and Table A2.1.1. Spatial variations in laboratory temperatures were observed. Among the instrument locations in the nutrient/salinity lab, from bench top to about one metre above the bench, the temperature had a range of 3-4 C.

<u>Table A2.1.1:</u> Laboratory temperature recorder statistics.

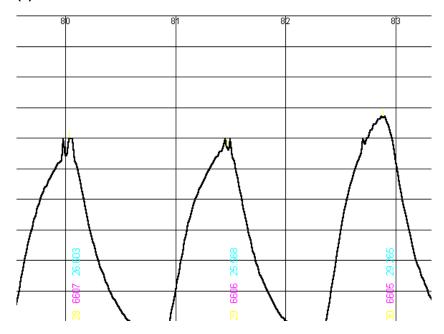
Temperature st	tatistics from Tinytalk
average	19.6 _C
stdev	0.4 _C
%rsd	1.9
min	18.5 _C
max	20.7 _C
range	2.2 _C
% range	11.3

#### Temperature control

Temperature in the nutrient/salinity laboratory was controlled with the ship's air conditioning and with a heating device. The lab was cooled with 16\_C air from the ships air conditioning, with the lab reheaters turned off. Heating was provided by a 'Cal control 9900' proportional, integral, and derivative (PID) controller/sensor controlling two simple fan heaters. The sensor was placed near the salinometer, at the height of the top of the salinometer. The setpoint was 19.6 C.

There was no temperature control in the dissolved oxygen lab besides the ship's air conditioning.







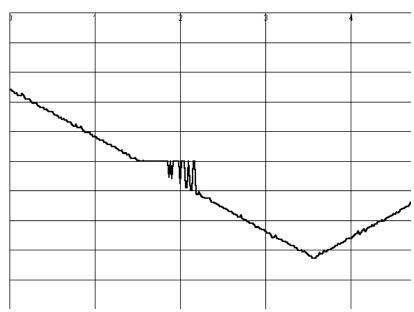
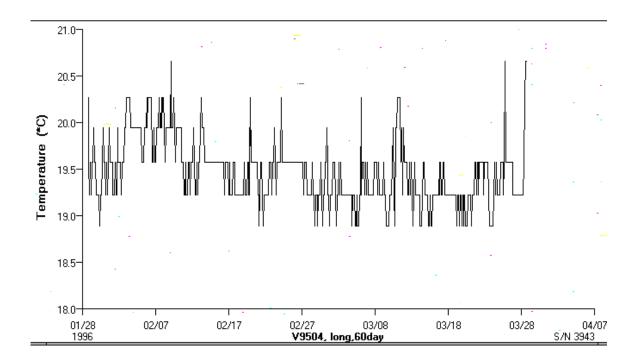
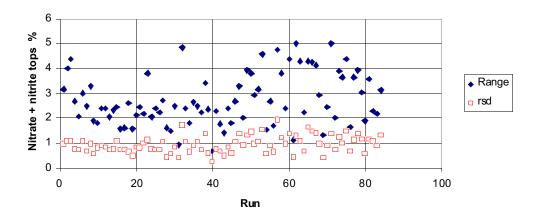
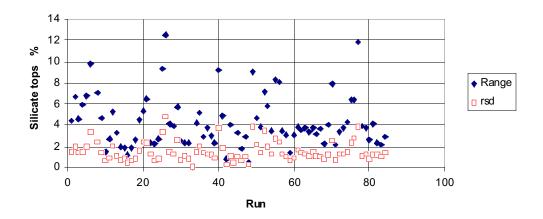


Figure A2.1.1a and b: 'Glitch' in nutrient A/D board: (a) real data, and (b) ramped voltage.



<u>Figure A2.1.2:</u> 'Tinytalk' temperature plot, 28/01/96 to 28/03/96, 48 minute time resolution; logger in film canister punctured to allow air flow, and positioned on middle of bottom shelf opposite fume cupboard in nutrient/salinity lab (lab 3).





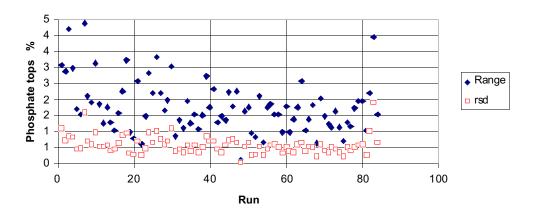


Figure A2.1.3: Statistics for tops used in nutrient analyses.

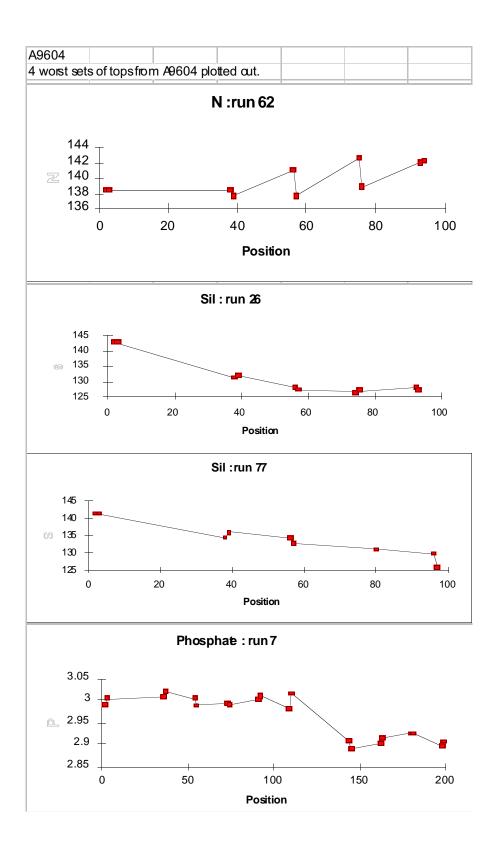


Figure A2.1.4: Worst cases of tops variations for the 3 nutrient channels.

<u>Table A2.1.2:</u> Nutrient samples run as quality checks.

			7				
A9604 nuts Output from QC.XLS, wit	th labels						
	.XLM to extract QC's (with s p	orefix in name)	<u>l</u>	<u>l</u>	1		
File	Run	Cup	QC name	QC batch	N	S	P
40004017 VI C	17	-	-6101	61	uM	uM	uM
A9604017.XLS A9604018.XLS	17 18	5	s6101 S6101	61 61	32.3 32.1	118.1 121.1	2.24 2.28
A9604019.XLS	19	5	s6101	61	32.3	118.8	2.26
A9604020.XLS	20	5	S6101	61	32.7	118.5	2.23
A9604021.XLS	21	5	s6101	61	32.2	99.3	2.29
A9604022.XLS	22	5	s6101	61	32.7	117.3	2.27
A9604022.XLS	22	47		61	32.8	115.8	2.26
A9604022.XLS	22	48		61	32.8 32.6	50.6	2.24 2.25
A9604023.XLS A9604024.XLS	23	5	s6101 s6101fridge	61 61	32.8	119.7 120.1	2.23
A9604024.XLS	24	6	s6101freezer	61	32.7	96.6	2.25
A9604025.XLS	25	5	S6101	61	32.8	79.1	2.28
A9604026.XLS	26	5	S6101	61	33.3	113.4	2.30
A9604027.XLS	27	5	s6101	61	32.5	108.2	2.25
A9604027.XLS	34	6	s6101	61	32.5	114.0	2.33
A9604028.XLS A9604029.XLS	27 28	6	s7102fresh s7102	71 71	32.8 33.0	117.5 115.8	2.27 2.40
A9604029.XLS	29	5	s7102 s7102	71	32.7	121.5	2.40
A9604030.XLS	30	5	s7102	71	32.9	116.4	2.36
A9604030.XLS	30	96		71	33.1	112.6	2.41
A9604030.XLS	30	97	s7102	71	33.1	118.4	2.36
A9604030.XLS	30	98		71	33.2	118.2	2.38
A9604031.XLS	30	99	s7102	71	33.3	119.4	2.43 2.38
A9604032.XLS A9604033.XLS	31	5	s7102 s7102	71 71	32.4 32.7	117.6 117.8	2.38 2.56
A9604033.XLS A9604034.XLS	32	5	s7102 s7102	71	32.7	117.8	2.59
A9604034.XLS	34	5	s7102	71	32.7	110.5	2.32
A9604035.XLS	35	5	s7102_fg thaw	71	32.1	87.3	2.19
A9604036.XLS	36	5	s7102 fridge thaw	71	32.9	109.5	2.34
A9604037.XLS	37		s7102 frdg thaw	71	32.6	115.3	2.35
A9604038.XLS A9604039.XLS	38	5	s7102 s7102	71 71	33.1 33.0	115.0 106.5	2.31 2.28
A9604039.XLS A9604040.XLS	40	5	s7102 s7102	71	32.7	113.7	2.28
A9604041.XLS	41	5	s7102	71	32.0	116.2	2.27
A9604042.XLS	42	5	s7102	71	33.0	116.8	2.30
A9604043.XLS	43	5	s7102	71	32.8	116.6	2.30
A9604044.XLS	44	5	s7102 air24h	71	32.4	119.2	2.29
A9604044.XLS	44	6	s7102 frid	71	32.7	116.9	2.29
A9604045.XLS	45	5	s7102 s7102	71	32.4 32.2	115.7 116.0	2.26 2.24
A9604046.XLS A9604047.XLS	40	5	s7102 s7102	71 71	32.8	118.5	2.24
A9604048.XLS	48	5	s7102 fdg,days	71	32.2	114.4	2.24
A9604048.XLS	49	86	s7102 air	71	33.4	127.5	2.25
A9604049.XLS	50	6	s7102,frd	71	32.6	100.5	2.26
A9604049.XLS	51	5	s7102	71	32.8	106.8	2.18
A9604049.XLS	48	6	s11603 fresh,fdg	116	32.7	126.2	2.26
A9604050.XLS A9604050.XLS	49	97	s11603 s11603 frsh, fdg	116 116	32.5 32.9	125.2 136.7	2.23 2.26
A9604051.XLS	50	5	s11603 iisii, idg s11603,air	116	32.2	121.6	2.31
A9604051.XLS	51	6	s11603	116	33.2	119.3	2.24
A9604051.XLS	51	60	s11603	116	33.3	125.0	2.19
A9604052.XLS	52	5	s11603	116	32.8	128.5	2.34
A9604052.XLS	52	58		116	32.7	122.7	2.37
A9604053.XLS	53	5	s11603	116	32.4	96.6	2.32
A9604053.XLS A9604053.XLS	53	59	s11603 s11603	116 116	33.0 32.3	115.5 113.2	2.35 2.35
A9604054.XLS	54		s11603	116	33.2	113.9	2.33
A9604054.XLS	54		s11603	116	33.1	122.2	2.32
A9604055.XLS	55	5	s11603	116	32.3	124.0	2.31
A9604055.XLS	55	59	s11603	116	32.2	118.3	2.30
A9604055.XLS	55	95	s11603	116	32.6	122.3	2.30
A9604056.XLS A9604056.XLS	56 56	59	s11603 s11603	116 116	32.8 32.0	110.0 122.6	2.29 2.30
A9604057.XLS	57	59	s11603	116	33.0	87.1	2.30
A9604058.XLS	58	5	s11603	116	32.6	129.2	2.34
A9604058.XLS	58	95	s11603	116	33.7	124.4	2.30
A9604059.XLS	59		s11603	116	32.0	125.2	2.27
A9604059.XLS	60	5	511005	116	32.0	124.5	2.29
A9604059.XLS	60	121	s11603 s11603	116	32.5	125.1	2.23
A9604059.XLS A9604060.XLS	62	50	s11603 s11603	116 116	31.5 32.6	89.2 86.3	2.24 2.24
A9604060.XLS	59	59	s13002 fresh	130	31.4	90.7	2.24
A9604060.XLS	59	62	s13002 fiesh	130	31.2	92.7	2.20
A9604060.XLS	59	63	s13002 fsh	130	31.5	92.6	2.20
A9604060.XLS	60	122	s13002	130	31.4	90.8	2.22
A9604061.XLS	60	123		130	31.9	90.8	2.23
A9604061.XLS	60	124	s13002	130	32.0	90.8 88.4	2.20 2.20
A9604062.XLS A9604062.XLS	61	60	s13002 s13002	130 130	32.8 32.5	88.4 89.9	2.20
A9604062.XLS	62		s13002 s13002	130	32.3	90.5	2.25
A9604063.XLS	63	5	s13002	130	31.8	89.3	2.24
A9604063.XLS	63	95	s13002	130	32.1	86.4	2.23
A9604064.XLS	64	5	s13002	130	32.3	85.4	2.24
A9604064.XLS	64	94	s13002	130	31.7	89.0	2.21
A9604065.XLS	65	58	s13002	130	33.5	72.5	2.24
A9604066.XLS A9604066.XLS	66	59	s13002 4h s13002 5h	130 130	32.2 31.1	85.4 89.4	2.24 2.24
A9604066.XLS A9604067.XLS	67	59	s13002 5h s13002 4h	130	31.1	89.4 83.8	2.24
A9604067.XLS	67	58	s13002 411 s13002	130	32.0	87.7	2.20
	67		s13002	130	31.8	88.2	2.22

A9604068.XLS	A9604068.XLS	68	5	s13002	130	32.3	86.8	2.24
A960409 XLS								
A9604069.XLS								
A9604073.XLS								
A9604070.XLS								
A9604071.XLS								
A9604071.XLS								
A9604071.XLS								
A9604071.XLS								2.20
A9604071.XLS								2.28
A9604071.KLS								2.27
A9604071.XLS								2.21
A9604071.XLS								2.22
A9604073.XLS								2.25
A9604073.XLS         71         101 s14102         141         31.9         100.7         2.21           A9604073.XLS         73         6 s14102         141         32.3         96.2         2.3           A9604073.XLS         73         60 s14102         141         31.7         100.0         2.3           A9604073.XLS         73         97 s14102         141         31.9         101.0         2.23           A9604074.XLS         74         5 s14102         141         32.4         89.8         2.3           A9604074.XLS         74         91 s14102         141         32.3         97.3         2.25           A9604075.XLS         75         5 s14102 2h         141         32.0         84.8         2.4           A9604075.XLS         75         5 s14102 2h         141         32.0         84.8         2.4           A9604075.XLS         75         74 s14102         141         32.1         61.5         2.2           A9604076.XLS         76         5 s14102 1h         141         32.1         61.5         2.2           A9604076.XLS         76         5 s14102 1h         141         32.2         100.9         2.2           A960407								2.18
A9604073.XLS								2.21
A9604073.XLS         73         97 s14102         141         31.9         101.0         2.28           A9604074.XLS         74         5 s14102         141         32.4         89.8         2.3           A9604074.XLS         74         91 s14102         141         32.3         97.3         2.25           A9604075.XLS         75         5 s14102 2h         141         32.0         84.8         2.4           A9604075.XLS         75         74 s14102         141         32.8         101.5         2.4*           A9604076.XLS         76         5 s14102 1h         141         32.1         61.5         2.2           A9604076.XLS         76         5 s14102 1h         141         32.2         100.9         2.2           A9604077.XLS         77         5 s14102         141         32.2         100.9         2.2           A9604077.XLS         77         9 s14102         141         31.7         87.4         2.3           A9604078.XLS         78         5 s14102         141         31.7         87.4         2.3           A9604078.XLS         78         67 s14102         141         32.6         96.9         2.3           A9604079.XLS	A9604073.XLS						96.2	2.33
A9604073.XLS         73         97 s14102         141         31.9         101.0         2.28           A9604074.XLS         74         5 s14102         141         32.4         89.8         2.3           A9604074.XLS         74         91 s14102         141         32.3         97.3         2.25           A9604075.XLS         75         5 s14102 2h         141         32.0         84.8         2.4           A9604075.XLS         75         74 s14102         141         32.8         101.5         2.4*           A9604076.XLS         76         5 s14102 1h         141         32.1         61.5         2.2           A9604076.XLS         76         5 s14102 1h         141         32.2         100.9         2.2           A9604077.XLS         77         5 s14102         141         32.2         100.9         2.2           A9604077.XLS         77         9 s14102         141         31.7         87.4         2.3           A9604078.XLS         78         5 s14102         141         31.7         87.4         2.3           A9604078.XLS         78         67 s14102         141         32.6         96.9         2.3           A9604079.XLS	A9604073.XLS		60	s14102			100.0	2.32
A9604074.XLS	A9604073.XLS		97	s14102	141	31.9	101.0	2.28
A9604075.XLS         75         \$ \$14102 2h         141         32.0         84.8         2.4*           A9604075.XLS         75         74 \$14102         141         32.8         101.5         2.4*           A9604076.XLS         76         5 \$14102 1h         141         32.1         61.5         2.2c           A9604076.XLS         76         59 \$14102 2h         141         32.2         100.9         2.2*           A9604077.XLS         77         5 \$14102         141         33.0         76.3         2.2*           A9604078.XLS         77         99 \$14102         141         31.7         87.4         2.3*           A9604078.XLS         78         5 \$14102         141         31.9         99.4         2.2*           A9604078.XLS         78         67 \$14102         141         32.6         96.9         2.3*           A9604078.XLS         78         104 \$14102         141         32.1         98.2         2.3*           A9604079.XLS         78         104 \$14102         141         32.1         98.2         2.3*           A9604079.XLS         79         5 \$14102         141         32.4         63.5         2.2*           A9	A9604074.XLS		5	s14102	141	32.4	89.8	2.30
A9604075.XLS         75         74 s14102         141         32.8         101.5         2.47           A9604076.XLS         76         5 s14102 lh         141         32.1         61.5         2.2           A9604076.XLS         76         59 s14102 lh         141         32.2         100.9         2.2s           A9604077.XLS         77         5 s14102         141         33.0         76.3         2.2s           A9604077.XLS         77         99 s14102         141         31.7         87.4         2.3           A9604078.XLS         78         5 s14102         141         31.9         99.4         2.2s           A9604078.XLS         78         67 s14102         141         32.6         96.9         2.3           A9604078.XLS         78         104 s14102         141         32.1         98.2         2.3           A9604079.XLS         79         5 s14102         141         31.7         88.4         2.2           A9604079.XLS         79         113 s14102         141         32.4         63.5         2.2           A9604080.XLS         80         5 s14102         141         32.4         63.5         2.2           A9604080.XLS	A9604074.XLS	74	91	s14102	141	32.3	97.3	2.25
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	A9604075.XLS	75	5	s14102 2h	141	32.0	84.8	2.45
A9604076.XLS         76         59 s14102 2h         141         32.2         100.9         2.28           A9604077.XLS         77         5 s14102         141         33.0         76.3         2.28           A9604077.XLS         77         99 s14102         141         31.7         87.4         2.31           A9604078.XLS         78         5 s14102         141         31.9         99.4         2.22           A9604078.XLS         78         67 s14102         141         32.6         96.9         2.30           A9604078.XLS         78         104 s14102         141         32.1         98.2         2.3           A9604079.XLS         79         5 s14102         141         31.7         88.4         2.22           A9604079.XLS         79         113 s14102         141         32.6         101.6         2.22           A9604080.XLS         80         5 s14102         141         32.4         63.5         2.22           A9604080.XLS         80         92 s14102         141         32.7         91.6         2.17           A9604081.XLS         81         5 s14102         141         32.3         93.9         2.22           A9604081.	A9604075.XLS	75	74	s14102	141	32.8	101.5	2.47
A9604077.XLS         77         5 s14102         141         33.0         76.3         2.28           A9604077.XLS         77         99 s14102         141         31.7         87.4         2.31           A9604078.XLS         78         5 s14102         141         31.9         99.4         2.28           A9604078.XLS         78         67 s14102         141         32.6         96.9         2.3           A9604078.XLS         78         104 s14102         141         32.1         98.2         2.3           A9604079.XLS         79         5 s14102         141         31.7         88.4         2.2           A9604079.XLS         79         113 s14102         141         32.6         101.6         2.2           A9604080.XLS         80         5 s14102         141         32.4         63.5         2.2           A9604080.XLS         80         92 s14102         141         32.7         91.6         2.1           A9604081.XLS         81         5 s14102         141         32.3         93.9         2.2           A9604081.XLS         81         111 s14102         141         32.5         97.4         2.2	A9604076.XLS	76	5	s14102 1h	141	32.1	61.5	2.26
A9604077.XLS         77         99 s14102         141         31.7         87.4         2.3           A9604078.XLS         78         5 s14102         141         31.9         99.4         2.2           A9604078.XLS         78         67 s14102         141         32.6         96.9         2.3           A9604078.XLS         78         104 s14102         141         32.1         98.2         2.3           A9604079.XLS         79         5 s14102         141         31.7         88.4         2.2           A9604079.XLS         79         113 s14102         141         32.6         101.6         2.2           A9604080.XLS         80         5 s14102         141         32.4         63.5         2.2           A9604080.XLS         80         92 s14102         141         32.7         91.6         2.1           A9604081.XLS         81         5 s14102         141         32.3         93.9         2.2           A9604081.XLS         81         111 s14102         141         32.5         97.4         2.2	A9604076.XLS	76	59	s14102 2h	141	32.2	100.9	2.28
A9604078.XLS         78         5 s14102         141         31.9         99.4         2.28           A9604078.XLS         78         67 s14102         141         32.6         96.9         2.3           A9604078.XLS         78         104 s14102         141         32.1         98.2         2.3           A9604079.XLS         79         5 s14102         141         31.7         88.4         2.2:           A9604079.XLS         79         113 s14102         141         32.6         101.6         2.2:           A9604080.XLS         80         5 s14102         141         32.4         63.5         2.2:           A9604080.XLS         80         92 s14102         141         32.7         91.6         2.1*           A9604081.XLS         81         5 s14102         141         32.3         93.9         2.2:           A9604081.XLS         81         5 s14102         141         32.3         93.9         2.2:           A9604081.XLS         81         111 s14102         141         32.5         97.4         2.2:	A9604077.XLS	77	5	s14102	141	33.0	76.3	2.28
A9604078.XLS     78     67 s14102     141     32.6     96.9     2.30       A9604078.XLS     78     104 s14102     141     32.1     98.2     2.3       A9604079.XLS     79     5 s14102     141     31.7     88.4     2.2       A9604079.XLS     79     113 s14102     141     32.6     101.6     2.2       A9604080.XLS     80     5 s14102     141     32.4     63.5     2.2       A9604080.XLS     80     92 s14102     141     32.7     91.6     2.1       A9604081.XLS     81     5 s14102     141     32.3     93.9     2.2       A9604081.XLS     81     111 s14102     141     32.5     97.4     2.2	A9604077.XLS	77	99	s14102	141	31.7	87.4	2.31
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	A9604078.XLS	78	5	s14102	141	31.9	99.4	2.28
A9604079.XLS     79     5 s14102     141     31.7     88.4     2.2       A9604079.XLS     79     113 s14102     141     32.6     101.6     2.2       A9604080.XLS     80     5 s14102     141     32.4     63.5     2.2       A9604080.XLS     80     92 s14102     141     32.7     91.6     2.1       A9604081.XLS     81     5 s14102     141     32.3     93.9     2.2       A9604081.XLS     81     111 s14102     141     32.5     97.4     2.2	A9604078.XLS	78	67	s14102	141	32.6	96.9	2.30
A9604079.XLS     79     113 s14102     141     32.6     101.6     2.2       A9604080.XLS     80     5 s14102     141     32.4     63.5     2.2       A9604080.XLS     80     92 s14102     141     32.7     91.6     2.1       A9604081.XLS     81     5 s14102     141     32.3     93.9     2.2       A9604081.XLS     81     111 s14102     141     32.5     97.4     2.21	A9604078.XLS	78	104	s14102	141	32.1	98.2	2.30
A9604080.XLS         80         5 s14102         141         32.4         63.5         2.24           A9604080.XLS         80         92 s14102         141         32.7         91.6         2.17           A9604081.XLS         81         5 s14102         141         32.3         93.9         2.24           A9604081.XLS         81         111 s14102         141         32.5         97.4         2.21			5	s14102			88.4	2.23
A9604080.XLS         80         92 \$14102         141         32.7         91.6         2.17           A9604081.XLS         81         5 \$14102         141         32.3         93.9         2.24           A9604081.XLS         81         111 \$14102         141         32.5         97.4         2.21	A9604079.XLS	79	113	s14102	141		101.6	2.23
A9604081.XLS         81         5 s14102         141         32.3         93.9         2.2c           A9604081.XLS         81         111 s14102         141         32.5         97.4         2.2c	A9604080.XLS		5	s14102			63.5	2.24
A9604081.XLS 81 111 s14102 141 32.5 97.4 2.21	A9604080.XLS		92	s14102				2.17
								2.24
A9604082.XLS 82 5 s14102 141 30.1 96.7 2.20	A9604081.XLS	81	111	s14102	141	32.5	97.4	2.21
	A9604082.XLS	82	5	s14102	141	30.1	96.7	2.26

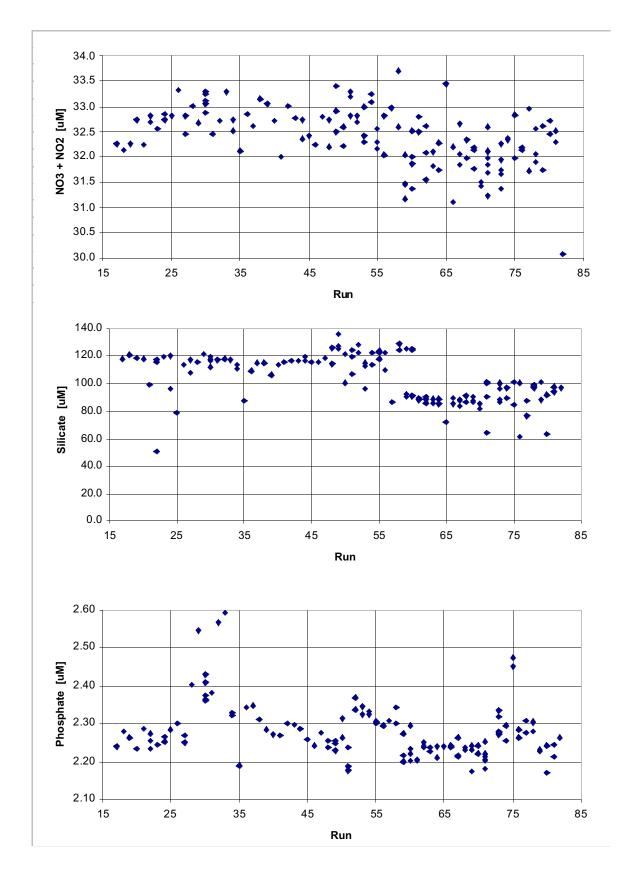


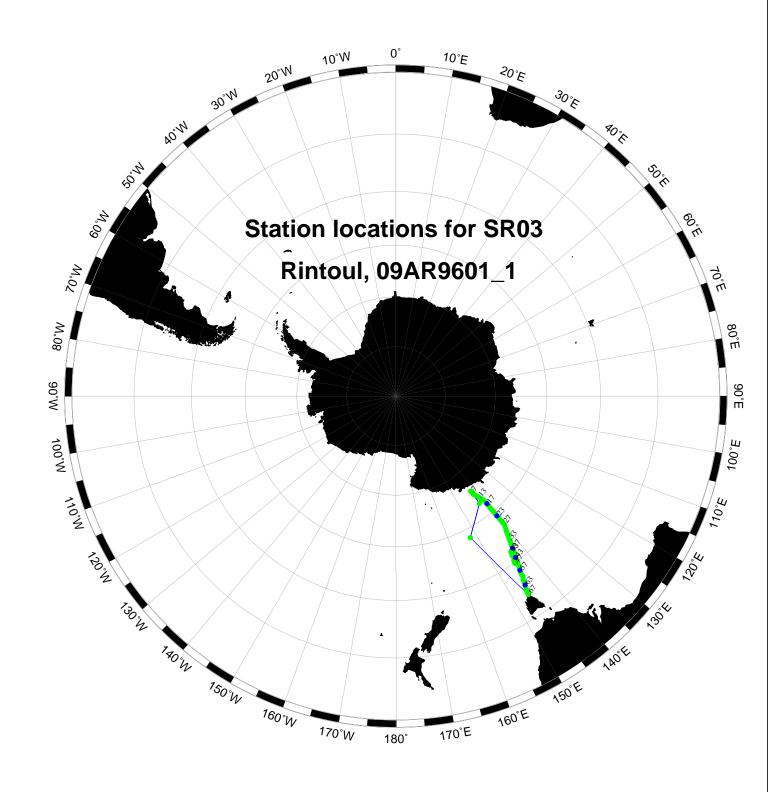
Figure A2.1.5: Nutrient samples run as quality checks.

<u>Table A2.1.3:</u> Nutrient analysis run numbers on which stations were run.

		_						_	1		
A9604 nuts											
run vs stn											
Shows problen	ns										
Stn	Run	Run	Probs	Stn	Run	Run	Probs	Stn	Run	Run	Probs
	first	repeat			first	repeat			first	repeat	
1	ns			61	23			120	55		
2	ns			62	17			121	52		
3	1		Ph	63	18			122	56		
4	ns			64	24			123	57		
5	ns			65				124	54		
6	115			66	24			125	56		
7	2				28		Ph	125	60		
	2			67							
8				68	28	79	Ph	127	60		
	2			69	28	77	Ph	128	59		
10	2			70	28	77	Ph	129	60		
11	2			71	27			130	59		
12			Ph	72	27			131	60		
13	3		Ph	73	29		Ph	132	60		
14	3	62	Ph	74	31		Ph	133	63		
15	3	63	Ph	75	30		Ph	134	64		
16	ns			76	30		Ph	135	65		
17	4	64	Ph	77	ns			136	ns		
18	Δ	66		78	34	81	Ph	137	67		
19	Δ		Ph	79	32		Ph	138	68		
20	7		Ph	80	33		S Ph	139	69		
21	ns	/0	111	81	35		5 111	140	69		
22	IIS	70	P?		33			140	71		
	3			82							
23		25		83	35			142	73		
24	7	25	Sx Ph	84	37			143	72		
25	7		Sx Ph	85	37			144	74		
26	7		Sx Ph	86				145	75	81	Ph
27	8	71	Ph N	87	39			146			
28	8	75	Ph	88	36			147	ns		
29	ns			89	37						
30	9	73	Ph N	90	41			N	Nitrate + nitr	rite	
31	9	74	Ph N	91	43	58	S	S	Silicate		
32	5			92	38			P	Phosphate		
33	11	81	Ph N	93	39			h	high		
34	12	78		94	43			X	Lost data		
35	6	70		95				ns	No sample		
36	14			96	40	<b>.</b>		Bold	indicates cha	.mm al/a	
37	14			96	40			Doid		illiei/s	
	9	ļ							of repeated	in final dere	
38	- 6	<b> </b>		98	43				station used	ın finai data.	
39	18			99	42						
40	18			100	45						
41	19			101	47						
42	7	29	Sx Ph	102	47						
43	ns			103	48						
44	19			104	48						
45	20			105	49						
46				106	49						
47	21			107	49						
48	10	77	Ph	108	50						
49	11	77	Ph	109	51	<b>i</b>					
50	11	77	Ph	110	44						
51	11	78			44						
			Ph N Ph	111							
52	12	-/9	rn	112		1	<b>.</b>				
53	22			113	51						
54	13			114	46						
55	13			115	47						
56	14			116	53						
57	23			117	53						
58	15			118	55						
59	16			119							
	ns	1		117	****						
									1		

1st sh applied to  1604	uise	Number	Sheet	Stn	Std	Blank	Date	Biiodate ba	tch
9804								2	
9804									
19604   3									
9804 4 14 19 9 4.439 0.0053 3.Feb-96 9804 5 20 26 4.435 0.0068 9.Feb-96 9804 6 27 34 4.429 0.0068 9.Feb-96 9.9904 7 33 40 4.431 0.0060 10-Feb-96 9.9904 8 36 44 4.432 0.0056 12-Feb-96 9.9904 9 39 47 4.434 -0.0052 13-Feb-96 9.9904 10 46 54 4.431 -0.0052 13-Feb-96 9.9904 11 53 62 4.428 -0.0050 17-Feb-96 9.9904 11 53 62 4.428 -0.0050 17-Feb-96 9.9904 12 56 66 4.437 0.0022 24-Feb-96 9.9904 12 56 66 64 4.437 0.0050 17-Feb-96 9.9904 13 65 75 4.435 0.0050 25-Feb-96 9.9904 14 71 82 4.433 0.0068 29-Feb-96 9.9904 15 80 93 4.440 0.0054 4-Mar-96 9.9904 16 86 98 4.437 0.0044 2-Mar-96 9.9904 17 92 104 4.436 0.0054 6-Mar-96 9.9904 18 99 111 4.428 0.0042 7-Mar-96 9.9904 19 104 117 4.427 0.0076 13-Mar-96 9.9904 19 104 117 4.427 0.0076 13-Mar-96 9.9904 20 110 124 4.423 0.0052 15-Mar-96 9.9904 22 119 133 4.424 0.0028 17-Mar-96 9.9904 24 130 145 4.424 0.0053 20-Mar-96 9.9904 24 130 145 4.424 0.0053 20-Mar-96 9.9904 24 130 145 4.424 0.0053 20-Mar-96 9.9904 22 119 133 4.424 0.0053 24-Mar-96 9.9904 23 124 139 4.423 0.0053 22-Mar-96 9.9909 9.9901 27 6 5 4 4.366 0.0040 28-Mar-96 9.9901 27 6 5 4 4.366 0.0040 28-Mar-96 9.9901 27 6 5 5 4 4.366 0.0040 28-Mar-96 9.9901 27 6 5 4 4.366 0.0040 28-Mar-96 9.9901 28 9 7 4.374 0.0010 15-Sep-96 10p up spb 18-8-96 not 9.9901 30 23 18 4.384 0.00070 31-Aup-96 9.9901 30 23 18 4.384 0.00070 31-Aup-96 9.9901 30 23 18 4.384 0.00070 13-Sep-96 10p up spb 18-8-96 not 9.9901 30 23 18 4.384 0.00070 13-Sep-96 10p up spb 18-8-96 not 9.9901 30 23 18 4.384 0.00070 13-Sep-96 10p up spb 18-8-96 not 9.9901 30 23 32 22 25 4.373 0.00050 13-Sep-96 10p up spb 18-8-96 not 9.9901 30 30 33 31 4.3867 0.00030 13-Sep-96 10p up spb 18-8-96 not 9.9901 30 30 33 31 4.3867 0.00030 13-Sep-96 10p up spb 18-8-96 not 9.9901 30 30 30 31 34 344 34 34 34 34 34 34 34 34 34 34 34									
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-0.005	_	5	**	**	<del>.   . • • •</del>	* * *	* . * · ·	=	+
-0.005	훋	0		•	<b>T</b>	1			+
	<u>=</u>						<b>'</b>   '	•	+
_0.01	<b>—</b> .0.00		<b>*</b>						-
-0.01 0 5 10 15 20 25 30 35 40	-0.00		* '					_	

Figure A2.1.6: Dissolved oxygen standardisations.



# Part 3 Aurora Australis Marine Science Cruise AU9601 - Oceanographic Field Measurements and Analysis

## **ABSTRACT**

Oceanographic measurements were conducted along WOCE Southern Ocean meridional section SR3 between Tasmania and Antarctica from August to September 1996. A total of 71 CTD vertical profile stations were taken, most to near bottom. Over 1500 Niskin bottle water samples were collected for the measurement of salinity, dissolved oxygen, nutrients, dissolved inorganic carbon, alkalinity, carbon isotopes, primary productivity, and biological parameters, using a 24 bottle rosette sampler. Near surface current data were collected using a ship mounted ADCP. Measurement and data processing techniques are summarised, and a summary of the data is presented in graphical and tabular form.

## 3.1 INTRODUCTION

Marine science cruise AU9601, the sixth oceanographic cruise of the Cooperative Research Centre for the Antarctic and Southern Ocean Environment (Antarctic CRC), was conducted aboard the RSV Aurora Australis from August to September 1996. The major constituent of the cruise was the collection of oceanographic data relevant to the Australian Southern Ocean WOCE Hydrographic Program, along WOCE section SR3 (Figure 3.1). This was the seventh occupation of section SR3 (and the last by the Aurora Australis under the WOCE program), and the second during a southern winter. Previous occupations of SR3 are summarised in Part 1 of this report. A further occupation of the northern half of SR3 took place in March to April of 1997 by the SCRIPPS ship R.V. Melville (principal investigators R.Watts, S. Rintoul, J. Richman, B. Petit, D. Luther, J. Filloux, J. Church, A. Chave).

This report describes the collection of oceanographic data from the SR3 section, and summarises the chemical analysis and data processing methods employed. All information required for use of the data set is presented in tabular and graphical form.

## 3.2 CRUISE ITINERARY

En route to Macquarie Island at the start of the cruise, the ship steamed in a straight line over the Tasmanian continental shelf for calibration tests of the ADCP. Three test CTD casts were also taken en route. Following cargo operations at Macquarie Island, the ship steamed southwest towards the southern end of the SR3 transect, taking a deep and a shallow test CTD cast on the way. A full day was spent penetrating southward into the ice before commencing the SR3 transect at the Antarctic shelf break east of Dumont D'Urville (Figure 3.1). The transect was then completed on the northward journey back to Hobart. Station spacing was decreased in the region of the Subantarctic Front, with casts taken over a series of inverted echo sounder and current meter moorings. The transect proper was interrupted briefly here for completion of several CTD casts over the eastern group of moorings in the larger mooring array (Figure 3.1) (Table 3.4). Further north, the SR3 station at latitude ~47.15°S was shifted ~5 nautical miles west of the transect line to avoid the pronounced steep bathymetry encountered at this latitude on previous cruises. Following completion of the SR3 transect, two further casts were taken to test another CTD before returning to Hobart.

## 3.3 CRUISE SUMMARY

In the course of the cruise, 71 CTD casts were completed along the SR3 section (Figure 3.1) (Table 3.2), plus additional test locations, with most casts reaching to within 20 m of the sea floor (Table 3.2). Over 1500 Niskin bottle water samples were collected for the measurement of salinity, dissolved oxygen, nutrients (orthophosphate, nitrate plus nitrite, and reactive silicate), dissolved inorganic carbon, alkalinity, carbon isotopes (<sup>14</sup>C and <sup>13</sup>C), primary productivity, and biological parameters, using a 24 bottle rosette sampler. Table 3.3 summarises samples drawn at each station. For all stations, the different samples were drawn in a fixed sequence (see previous data reports). Casts taken over mooring locations are summarised in Table 3.4. Principal investigators for the various water sampling programmes and cruise participants are listed in Tables 3.5a and b.

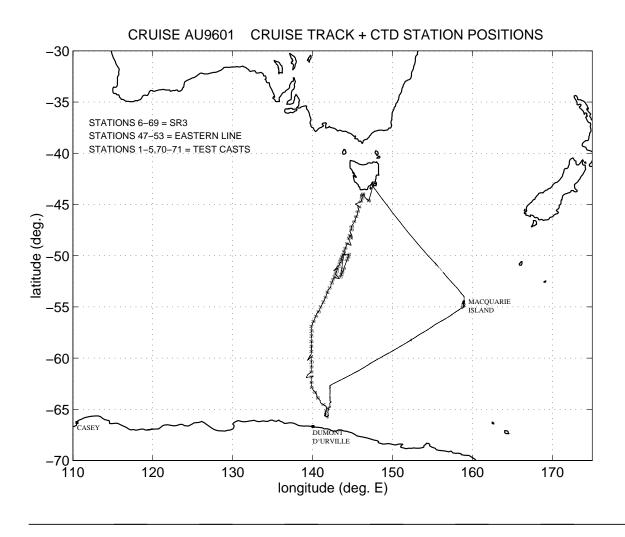


Figure 3.1: Cruise track and CTD station positions for RSV Aurora Australis cruise AU9601.

## Table 3.1: Summary of cruise itinerary.

Expedition Designation
Cruise AU9601 (cruise acronym WASTE), encompassing WOCE section SR3

Chief Scientist
Steve Rintoul, CSIRO

Ship RSV Aurora Australis

Ports of Call
Macquarie Island

Cruise Dates
August 22 to September 22 1996

Table 3.2 (following 2 pages): Summary of station information for RSV Aurora Australis cruise AU9601. The information shown includes time, date, position and ocean depth for the start of the cast, at the bottom of the cast, and for the end of the cast. The maximum pressure reached for each cast, and the altimeter reading at the bottom of each cast (i.e. elevation above the sea bed) are also included. Missing ocean depth values are due to noise from the ship's bow thrusters interfering with the echo sounder. For casts which do not reach to within 100 m of the bed (i.e. the altimeter range), or for which the altimeter was not functioning, there is no altimeter value. For station names, TEST is a test cast and EL is the eastern line (the meridional section over the eastern part of the mooring array). Note that all times are UTC (i.e. GMT). CTD unit 7 (serial no. 1103) was used for stations 4 to 69; CTD unit 5 (serial no. 1193) was used for stations 1 to 2 and 70 to 71; CTD unit 6 (serial no. 2568) was used for station 3.

station			STA	RT		maxP		ВС	TTOM				EN	D	
number	time	date	latitude	longitude	depth(m)	(dbar)	time	latitude	longitude	e depth(n	n) altimeter	time	latitude	longitude	depth(m)
1 TEST	0715 2	24-AUG-96	50:48.64S	155:26.04E	4597	1026	0757	50:49.31	S 155:27.15	E 4604	-	0829	50:49.72S	155:27.89E	4589
2 TEST	0903 2	25-AUG-96	54:47.52S	159:02.91E	4607	154	0912	54:47.62	S 159:03.13	E -	-	0917	54:47.67S	159:03.19E	4607
3 TEST	1048 2	25-AUG-96	54:56.43S	158:56.37E	3071	840	1137	54:56.48	S 158:57.54	·E -	-	1156	54:56.43S	158:57.67E	-
4 TEST	0536 2	27-AUG-96	58:14.95S	152:18.29E	2355	2564	0702	58:15.12	S 152:17.62	E -	30.1	0814	58:15.03S	152:17.35E	-
5 TEST	0230 2	29-AUG-96	62:50.62S	142:10.90E	3993	344	0252	62:50.62	S 142:11.17	Έ -	-	0304	62:50.67S	142:11.37E	-
6 SR3	0726 3	30-AUG-96	65:44.59S	141:51.94E	761	764	0812	65:44.37	S 141:51.07	E 773	-	0904	65:44.04S	141:50.28E	768
7 SR3	0554 3	31-AUG-96	65:34.50S	141:34.66E	1019	970	0636	65:34.30	S 141:34.24	E 973		0727	65:34.09S	141:33.73E	951
8 SR3				141:35.62E	-	1486	1017	65:30.10	S 141:35.08	E 1505		1114	65:29.89S	141:34.48E	1494
9 SR3	1252 3	31-AUG-96	65:25.68S	141:37.33E	2125	2100	1402	65:25.45	S 141:36.58	E 2099	8.8	1521	65:25.15S	141:35.43E	2077
10 SR3				141:41.76E		2544	2001	65:10.37	S 141:40.14	E 2529		2115	65:10.20S	141:38.34E	2551
11 SR3	0106	1-SEP-96	64:52.96S	141:51.58E	2965	2950	0241	64:52.77	S 141:48.58	E -	10.0	0414	64:52.54S	141:45.55E	2920
12 SR3	0949	1-SEP-96	64:30.67S	141:20.56E	3506	3518	1136	64:30.10	S 141:16.15	E 348	1 4.6	1329	64:29.44S	141:11.59E	3462
13 SR3	2219	1-SEP-96	63:53.74S	140:39.16E	3716	3746	2356	63:52.72	S 140:38.22	E 3732		0127	63:51.87S	140:38.40E	3726
14 SR3	0622	2-SEP-96	63:22.44S	140:18.76E	3801	3836	0757	63:21.22	S 140:21.04	E 380	-	0944	63:20.08S	140:22.33E	3801
15 SR3	1442	2-SEP-96	62:51.01S	139:52.91E	3225	3262	1613	62:50.88	S 139:53.65	E 3246		1729	62:50.76S	139:54.28E	3251
16 SR3	2115	2-SEP-96	62:21.73S	139:50.56E	3952	3988	2254	62:21.45	S 139:49.95	iΕ -	9.9	0032	62:21.81S	139:49.38E	3963
17 SR3	0403	3-SEP-96	61:50.89S	139:51.19E	4300	4344	0543	61:51.33	3 139:50.61	E -	11.0	0731	61:52.07S	139:50.25E	-
18 SR3	2101	3-SEP-96	61:21.18S	139:50.16E	4336	4392	2253	61:21.76	S 139:49.39	E -	15.5	0031	61:22.25S	139:49.42E	-
19 SR3	0348	4-SEP-96	60:50.89S	139:50.83E	4392	4460	0527	60:51.16	S 139:49.81	E -	3.6	0657	60:51.19S	139:49.78E	-
20 SR3	0956	4-SEP-96	60:20.95S	139:51.04E	4443	4488	1134	60:21.13	S 139:51.04	E -	18.0	1312	60:21.36S	139:51.30E	-
21 SR3	1847	4-SEP-96	59:51.21S	139:51.34E	4474	4534	2038	59:51.85	S 139:51.84	E -	15.3	2233	59:52.24S	139:52.74E	-
22 SR3	1547	5-SEP-96	59:21.15S	139:50.92E	4146	4174	1730	59:21.99	S 139:51.21	E -	15.3	1902	59:22.30S	139:51.51E	-
23 SR3				139:50.56E		3962	0026	58:51.22	S 139:50.50	E -	15.4	0146	58:51.42S	139:51.24E	-
24 SR3	1247	6-SEP-96	58:21.01S	139:51.16E	3942	4084	1422	58:22.00	S 139:51.25	E -	18.8	1554	58:22.23S	139:50.38E	-
25 SR3				139:51.00E		4168	2052	57:51.67	S 139:51.69	E -	15.3	2227	57:52.14S	139:52.12E	-
26 SR3	0714	7-SEP-96	57:20.92S	139:52.03E	4100	4212	0859	57:21.07	3 139:52.35	E -	16.9	1047	57:21.00S	139:51.26E	-
27 SR3	1328	7-SEP-96	56:55.95S	139:51.10E	4100	4272	1514	56:55.93	3 139:52.32	E -	19.5	1641	56:55.89S	139:52.98E	-
28 SR3	2324	7-SEP-96	56:25.80S	140:05.89E	3910	3950	0105	56:25.45	S 140:07.06	iΕ -	15.3	0228	56:25.06S	140:07.39E	-
29 SR3	0602	8-SEP-96	55:55.80S	140:24.49E	3730	3640	0751	55:55.113	3 140:25.27	Έ -	16.5	0930	55:54.72S	140:25.78E	-
30 SR3	1738	8-SEP-96	55:29.97S	140:44.03E	3890	3900	1919	55:29.57	S 140:44.95	E -	16.1	2054	55:29.13S	140:45.64E	-
31 SR3	0004	9-SEP-96	55:00.93S	141:01.35E	3225	3238	0131	55:00.55	S 141:01.78	E -	12.4	0250	55:00.33S	141:01.88E	-
32 SR3	0603	9-SEP-96	54:31.92S	141:19.86E	2815	2896	0734	54:32.61	S 141:19.04	E -	14.5	0857	54:32.91S	141:19.33E	-
33 SR3	1207	9-SEP-96	54:03.91S	141:36.09E	2559	2666	1205	54:03.92	S 141:36.06	iE -	16.9	1429	54:04.21S	141:36.90E	-
34 SR3	1736	9-SEP-96	53:34.68S	141:51.63E	2503	2672	1901	53:34.20	S 141:49.77	Έ -	18.3	2025	53:33.50S	141:48.66E	-
35 SR3	2308	9-SEP-96	53:07.98S	142:08.17E	3122	3244	0039	53:08.43	S 142:10.83	E -	23.5	0155	53:08.45S	142:12.03E	-
36 SR3	0510 1	10-SEP-96	52:40.03S	142:23.22E	3378	3396	0641	52:40.15	3 142:24.16	E -	16.8	0807	52:40.16S	142:24.31E	-

station			STA	\RT		maxP		ВС	TTOM				EN	D	
number	time	date	latitude	longitude	depth(m)	(dbar)	time	latitude	longitude	depth(m)	altimeter	time	latitude	longitude	depth(m)
					• • •	,				, , ,					• • •
37 SR3	1010 1	0-SEP-96	52:21.93S	142:31.92E	3481	3608	1146	52:21.93	3 142:32.61	-	20.4	1308	52:22.36S	142:33.11E	-
38 SR3	1521 1	0-SEP-96	52:04.98S	142:42.34E	3481	3544	1652	52:05.62	3 142:42.69	-	15.2	1814	52:05.89\$	142:43.00E	-
39 SR3	0344 1	1-SEP-96	51:48.52S	142:50.68E	3686	3782	0530	51:48.49	3 142:50.71	≣ -	16.0	0655	51:48.60S	142:51.04E	-
40 SR3	0843 1	1-SEP-96	51:32.14S	142:59.19E	3686	3834	1035	51:32.07	3 142:59.26	≣ -	18.8	1214	51:32.16S	142:59.35E	-
41 SR3	1422 1	1-SEP-96	51:15.70S	143:07.74E	3737	3832	1548	51:15.76	S 143:07.71I	≣ -	16.2	1713	51:15.76S	143:07.93E	-
42 SR3	0348 1	2-SEP-96	51:00.49S	143:16.03E	3870	3884	0517	50:59.68	S 143:16.84I	-	18.1	0643	50:58.99S	143:17.54E	-
43 SR3	0904 1	2-SEP-96	50:40.89S	143:25.14E	3583	3556	1048	50:40.16	S 143:29.77I	-	16.7	1219	50:39.58S	143:32.34E	-
44 SR3	2111 1	2-SEP-96	50:23.87S	143:32.09E	3580	3580	2258	50:23.71	S 143:33.09I	-	16.5	0022	50:23.82S	143:33.30E	-
45 SR3	0253 1	3-SEP-96	50:09.63S	143:40.07E	3563	3740	0436	50:09.18	S 143:40.57I	≣ -	17.9	0602	50:08.77S	143:40.54E	-
46 SR3	0827 1	3-SEP-96	49:53.17S	143:48.27E	3768	3788	1010	49:53.08	S 143:48.40I	≣ -	23.1	1130	49:52.99S	143:47.92E	-
47 EL	1443 1	3-SEP-96	49:53.16S	144:33.90E	3768	3888	1610	49:53.13	S 144:34.54I	<b>-</b>	18.5	1735	49:53.32S	144:34.66E	-
48 EL				144:27.34E		3884			S 144:27.33I		15.9			144:27.38E	
49 EL				144:17.95E		3198			S 144:18.28I		13.0			144:19.02E	
50 EL				143:54.24E		3794			S 143:54.22I		17.2			143:54.34E	
51 EL				143:46.65E		3780			S 143:46.60I		17.9			143:46.75E	
52 EL				143:37.95E		3646			S 143:37.89I		5.8			143:38.16E	
53 EL				143:29.43E		3564			S 143:29.52I		16.9			143:29.52E	
54 SR3				143:55.95E		3730			S 143:55.93I		18.9			143:56.02E	
55 SR3				144:06.03E		4422			5 144:05.71		18.5		-	144:06.22E	
56 SR3				144:18.94E		4148			3 144:19.39		15.0	_		144:19.74E	
57 SR3				144:32.00E		4126			S 144:32.23I		15.1	_		144:32.43E	
58 SR3				144:40.33E		4412	_		3 144:40.25		17.3			144:40.45E	
59 SR3				144:53.80E		4384			S 144:52.12I		25.6			144:50.88E	
60 SR3				144:54.19E		4882			S 144:53.08I		20.8			144:52.51E	
61 SR3				145:15.19E		3434			S 145:15.01I		21.1			145:14.89E	
62 SR3				145:28.15E	_	2754			S 145:28.41I		14.6			145:28.57E	
63 SR3				145:39.82E		2098			S 145:39.82I		15.6			145:39.93E	
64 SR3				145:50.89E		2892			3 145:49.78		14.7			145:49.69E	
65 SR3				146:03.04E		3222		_	S 146:03.82I		17.0			146:04.75E	
66 SR3				146:11.37E		2348			3 146:11.82		17.1			146:11.95E	
67 SR3				146:13.33E		1000			S 146:13.29I		17.5	_		146:13.39E	
68 SR3				146:17.21E		478			S 146:18.09I		17.4			146:18.52E	
69 SR3				146:19.17E		190			S 146:19.48I		12.0			146:19.83E	
70 TEST				147:00.22E	-	318	_		S 147:00.37I		-	-		147:00.47E	
71 TEST	1248 2	1-SEP-96	44:37.02S	147:00.21E	2559	2564	1415	44:37.13	S 147:00.82I	-	28.5	1534	44:37.415	147:00.97E	-

<u>Table 3.3:</u> Summary of samples drawn from Niskin bottles at each station, including salinity (sal), dissolved oxygen (do), nutrients (nut), dissolved inorganic carbon (dic), alkalinity (alk), carbon isotopes (Ctope), fluorometry (fl), and pigments (pig); Seacat casts are also listed. Note that 1=samples taken, 0=no samples taken, 2=surface sample only (i.e. from shallowest Niskin bottle or from seawater outlet).

1         1         1         1         1         1         1         1         0	station	sal do nut	dic alk Ctope fl	pig SEACAT
3         0				
4         1         1         1         0				
5         1         1         1         0				
6				
7         1         1         1         1         2         1				
8       1       1       1       1       2       1       1       1       1       9       0        0       0       0       0       0       0       0       0       0       0       0       0       0       0       0        0       0       0       0       0       0       0       0       0       0       0       0       0       0       0        0       0       0       0       0       0       0       0       0       0       0       0       0       0       0        0       0       0       0       0       0       0       0       0       0       0       0       0       0       0        0       0       0       0       0       0       0       0       0       0       0       0       0       0       0        0       0       0       0       0       0       0       0 </td <td></td> <td></td> <td></td> <td></td>				
9				
11       1				
12       1       1       1       1       2       1       1       1         133       1       1       1       1       2       1       1       1         144       1       1       1       1       1       2       1       1       1         155       1       1       1       1       1       0       1       1         166       1       1       1       1       1       1       0       1       1         17       1       1       1       1       1       1       1       1       1         18       1       2       2       1       1       1 </td <td>10</td> <td>1 1 1</td> <td></td> <td>1 1</td>	10	1 1 1		1 1
13       1       1       1       1       2       1       1       1         14       1       1       1       1       2       1       1       1         15       1       1       1       1       1       1       1       1       1         16       1       2       2       1       1       1       1       2       2 <td< td=""><td></td><td></td><td></td><td></td></td<>				
14       1       1       1       1       2       1       1       1         15       1       1       1       1       1       0       1       1         16       1       1       1       1       1       1       1       1       1         17       1       2       2       1       1       1 <td< td=""><td></td><td></td><td></td><td></td></td<>				
15       1       1       1       1       1       0       1       1         16       1       1       1       1       2       1       1       1         17       1       1       1       1       1       2       1       1       1         18       1       2       2       1       1       1       1       2       2       1       1       1       1       2       2       1       1       1       2       2       1       1       1 <td< td=""><td></td><td></td><td></td><td></td></td<>				
16       1       1       1       1       2       1       2       2       1       1       1       1       2       2       1       1       1       1       2       2       2       1       1       1       1       2       2       1       1				
17       1       1       1       1       2       1       2       2       1       1       1       1       1       2       2       1       1       1       1       2       2       1       1       1       1       2       2       1       1       1       1       2       2       1       1       1       1       2       2       1       1       1       1       2       2       1       1				
18       1       2       0       1       1       1       1       2       0       1       1       1       1       2       2       2       1       1       1       1       2       2       2       1       1       1       1       2       2       2       1       1       1       1       2       2       2       1       1       1       1       2       2				
19       1       1       1       1       2       2       1       1       1         20       1       1       1       1       0       0       1       1         21       1       1       1       1       1       1       1       1         21       1       1       1       1       1       1       1       1         22       1       1       1       1       1       1       1       1         23       1       1       1       1       1       2       0       1       1         24       1       1       1       1       1       0       1       1         24       1       1       1       1       1       0       1       1         25       1       1       1       1       1       0       1       1         26       1       1       1       1       1       2       1       1       1         27       1       1       1       1       1       2       1       1       1         28       1       1				
21       2       2       2       1       1       1       1       3       3       1       1       1       1       1				
22       1       1       1       1       2       0       1       1         23       1       1       1       1       2       1       1       1         24       1       1       1       1       1       1       1       1       1         25       1 <td< td=""><td>20</td><td>1 1 1</td><td>1 1 0 0</td><td>1 1</td></td<>	20	1 1 1	1 1 0 0	1 1
23       1       1       1       1       2       1       1       1         24       1       1       1       1       1       0       1       1         25       1       1       1       1       1       0       1       1         26       1       1       1       1       2       1       1       1         27       1       1       1       1       2       1       1       1         28       1       1       1       1       2       0       1       1         29       1       1       1       1       2       1       1       1         29       1       1       1       1       2       1       1       1         30       1       1       1       1       1       1       1       1         31       1       1       1       1       1       1       1       1       1         32       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1				
24       1       1       1       1       1       0       1       1         25       1       1       1       1       1       1       1       1         26       1       1       1       1       2       2       1       1       1       1         27       1       1       1       1       1       2       1       1       1       1       2       1       1       1       1       2       2       1       1       1       1       2       2       1       1       1       1       2       2       1 <td< td=""><td></td><td></td><td></td><td></td></td<>				
25       1       1       1       2       2       2       1       1       1       1       1       2       2       2       1       1       1       1       2       1				
26       1       1       1       1       2       1				
27       1 1 1 1 1 1 2 0 1 1 1         28       1 1 1 1 1 1 2 1 1 1         29       1 1 1 1 1 1 2 1 1 1         30       1 1 1 1 1 1 1 0 1 1         31       1 1 1 1 2 2 2 1 1 1         32       1 1 1 1 1 2 1 1 1 1         33       1 1 1 2 2 2 2 0 1 1 1         34       1 1 1 1 2 2 2 2 0 1 1         35       1 1 1 2 2 2 2 1 1 1         36       1 1 1 1 2 2 1 1 1         37       1 1 1 1 1 2 0 1 1         38       1 1 1 2 2 2 0 1 1         39       1 1 1 1 1 1 1 1 1 1 1 1 1 1         40       1 1 1 1 1 1 2 1 1 1         41       1 1 1 1 1 1 2 1 1 1         42       1 1 1 1 1 1 2 1 1 1         43       1 1 1 1 1 1 2 1 1 0         44       1 1 1 1 1 1 2 1 1 0         44       1 1 1 1 1 1 0 1 0 1 0         45       1 1 1 1 1 1 0 1 0 1 0         46       1 1 1 1 1 1 0 1 0 1 0         47       1 1 1 2 2 0 0 0 0 0         48       1 1 1 1 2 2 0 0 0 0         49       1 1 1 1 2 2 0 0 0				
28       1       1       1       1       2       1       1       1         29       1 <td></td> <td></td> <td></td> <td></td>				
29       1       1       1       1       2       1       1       1         30       1 <td></td> <td></td> <td></td> <td></td>				
30       1				
32       1       1       1       1       2       1       1       1       1       33       1		1 1 1		
33       1       1       1       2       2       2       0       1       1         34       1       1       1       1       1       1       0       1       1         35       1       1       1       2       2       2       1       1       1         36       1       1       1       1       2       1       1       1       1         37       1       1       1       1       2       0       1       1       1         38       1       1       1       2       2       2       0       1       1         39       1				
34       1				
35       1       1       1       2       2       2       1       1       1         36       1       1       1       1       2       1       1       1       1         37       1       1       1       1       1       2       0       1       1         38       1       1       1       2       2       2       0       1       1         39       1       1       1       1       1       1       1       1       1         40       1				
36       1       1       1       1       2       1       1       1       1         37       1       1       1       1       2       0       1       1         38       1       1       1       2       2       2       0       1       1         39       1       1       1       1       1       1       1       1       1         40       1				
37       1       1       1       1       2       0       1       1         38       1       1       1       2       2       2       0       1       1         39       1       1       1       1       1       1       1       1       1         40       1       1       1       1       1       1       1       1       1         41       1       1       1       1       2       1				
38       1       1       1       2       2       2       0       1       1         39       1       1       1       1       1       1       1       1       1       1         40       1       0       1       1       1       0       0       0       0       0       0       0       0       0       0       0       0       0       0       0        0				
39       1       0			2 2 2 0	
40       1       1       1       1       2       1       0       1       1       1       0			1 1 1 1	
41       1       1       1       1       2       0       1       1         42       1       1       1       1       2       1       1       0         43       1       1       1       1       1       0       1       1       0         44       1       1       1       1       1       0       1       1       0         45       1       1       1       1       1       1       0       0         46       1       1       1       1       0       1       0       0         47       1       1       1       2       2       0       0       0         48       1       1       1       2       2       0       0       0         49       1       1       1       2       2       0       0       0	40	1 1 1	1 1 2 1	1 1
43       1       1       1       1       0       1       1       0         44       1       1       1       1       0       1       1       0         45       1       1       1       1       1       1       0       0         46       1       1       1       1       0       1       0       0         47       1       1       1       2       2       0       0       0       0         48       1       1       1       2       2       0       0       0       0         49       1       1       1       2       2       0       0       0       0			1 1 2 0	
44       1       1       1       1       0       1       1       0         45       1       1       1       1       2       1       1       0         46       1       1       1       1       0       1       0       0         47       1       1       1       2       2       0       0       0       0         48       1       1       1       2       2       0       0       0       0         49       1       1       1       2       2       0       0       0       0				
45     1     1     1     1     2     1     1     0       46     1     1     1     1     0     1     0     0       47     1     1     1     2     2     0     0     0     0       48     1     1     1     2     2     0     0     0     0       49     1     1     1     2     2     0     0     0     0				
46       1       1       1       1       0       1       0       0         47       1       1       1       2       2       0       0       0       0         48       1       1       1       2       2       0       0       0       0         49       1       1       1       2       2       0       0       0       0				
47       1 1 1 1 2 2 0 0 0 0         48       1 1 1 2 2 0 0 0 0         49       1 1 1 2 2 0 0 0				
48				
49 1 1 1 2 2 0 0 0 0				
50 1 1 1 2 2 0 0 0 0			2 2 0 0	

Table 3.3: (continued)

station	sal	do	nut	dic	alk	Ctope	e fl	pig	SEACAT
51	1	1	1	2	2	0	0	0	0
52	1	1	1	2	2	0	0	0	0
53	1	1	1	2	2	0	0	0	0
54	1	1	1	1	1	0	1	1	1
55	1	1	1	1	1	1	0	1	1
56	1	1	1	2	2	0	0	1	1
57	1	1	1	1	1	2	1	1	1
58	1	1	1	1	1	0	0	1	1
59	1	1	1	1	1	1	0	1	0
60	1	1	1	1	1	0	1	1	0
61	1	1	1	1	1	2	1	1	1
62	1	1	1	1	1	0	1	1	1
63	1	1	1	1	1	0	1	1	1
64	1	1	1	2	2	2	1	1	1
65	1	1	1	1	1	1	0	1	1
66	1	1	1	2	2	0	0	1	1
67	1	1	1	1	1	0	1	1	1
68	1	1	1	0	0	0	1	1	1
69	1	1	1	1	1	0	0	0	0
70	0	0	0	0	0	0	0	0	1
71	1	0	0	0	0	0	0	0	0

<u>Table 3.4:</u> CTD stations over current meter (CM) and inverted echo sounder (IES) moorings along SR3 transect in the vicinity of the Subantarctic Front. Note that bottom depths (at the start of each CTD cast) are calculated using a sound speed of 1498 ms<sup>-1</sup>. For CTD station positions, see Table 3.2.

CTD station no.	start time	bottom depth (m)	mooring number
38	15:21, 10/09/96	3481	I18 (IES)
39	03:44, 11/09/96	3686	116 (IES)
40	08:43, 11/09/96	3686	114 (IES)
41	14:22, 11/09/96	3737	I12 (IES)
42	03:48, 12/09/96	3870	I10 (CM+IES)
43	09:04, 12/09/96	3583	I9 (CM+IES)
44	21:11, 12/09/96	3580	I8 (CM+IES)
45	02:53, 13/09/96	3563	16 (IES)
46	08:27, 13/09/96	3768	14 (IES)
47	14:43, 13/09/96	3768	13 (IES)
48	20:37, 13/09/96	3730	15 (IES)
49	03:44, 14/09/96	3420	17 (IES)
50	14:00, 14/09/96	3737	I11 (IES)
51	18:55, 14/09/96	3686	113 (IES)
52	00:28, 15/09/96	3481	I15 (IES)
53	05:52, 15/09/96	3532	117 (IES)
54	05:07, 16/09/96	3665	I2 (IES)
58	14:14, 17/09/96	4116	I1 (IES)

<u>Table 3.5a:</u> Principal investigators (\*=cruise participant) for rosette water sampling programmes.

measurement	name		affiliation
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CTD, salinity, O<sub>2</sub>, nutrients \*Steve Rintoul/Nathan Bindoff CSIRO/Antarctic CRC

D.I.C., alkalinity, carbon isotopes \*Bronte Tilbrook CSIRO

fluorometry \*Peter Strutton(PhD student) Flinders University biological sampling Harvey Marchant/\*Simon Wright Antarctic Division

Table 3.5b: Scientific personnel (cruise participants).

name	measurement	affiliation
Muhammad Evri Helen Phillips Steve Rintoul Marie Robert Mark Rosenberg	CTD CTD CTD CTD	BPPT (Indonesia) Antarctic CRC CSIRO Antarctic CRC Antarctic CRC
Serguei Sokolov Annie Wong Fadli Syamsudin	CTD CTD CTD	CSIRO Antarctic CRC BPPT (Indonesia)
Stephen Bray Ana Costalunga Neale Johnston	salinity, oxygen, nutrients oxygen salinity, oxygen, nutrients	Antarctic CRC Antarctic CRC Antarctic CRC
Rebecca Esmay Mark Pretty Bronte Tilbrook Alison Walker	D.I.C., alkalinity, C isotopes D.I.C., alkalinity, C isotopes D.I.C., alkalinity, C isotopes D.I.C., alkalinity, C isotopes	CSIRO CSIRO CSIRO CSIRO
Raechel Waters Simon Wright	biological sampling biological sampling, voyage leader	Antarctic Division Antarctic Division
Simon Evans Robert Geier Stewart Graham Alan Poole Sandra Potter Peter Strutton Andrew Tabor Wojciech Wierzbicki Karen Wilson	programmer programmer doctor electronics deputy voyage leader, fishing underway data, fluorometry gear officer, fishing electronics fishing	Antarctic Division Antarctic Division Antarctic Division CSIRO Antarctic Division Antarctic Division/Flinders University Antarctic Division Antarctic Division Marine Studies Centre (Tasmania)
Steve Oakley	returnee	Antarctic Division

## 3.4 FIELD DATA COLLECTION METHODS

### 3.4.1 CTD and hydrology measurements

CTD and hydrology instrumentation, data collection and processing methods are as described in Part 2 of this report. The hydrology laboratory report for this cruise can be found in Appendix 3.1. Preliminary results of the CTD data calibration, along with data quality information, are presented in Section 3.6. Calibration information for CTD sensors are presented in Table 3.22. Note that no photosynthetically active radiation (p.a.r.) sensor or fluorometer were attached to the rosette package for this cruise. P.a.r. and fluorescence data were collected by a Seabird "Seacat" CTD, which was deployed separately (Table 3.3) (these data are not discussed further in this report).

The following updates apply to the CTD data processing and hydrology analytical techniques:

- (i) in the conductivity calibration for stations 10 to 21, an additional term was applied to remove the pressure dependent conductivity residual;
- (ii) salinity bottle samples were analysed using a Guildline Autosal model 8400B (YeoKal salinometers had been used on all previous cruises); substandard measurements were not required, owing to the stability of the Autosal; international seawater standards were measured at the start and end of each day's analysis.

# 3.4.2 Underway measurements

Underway data collection is as described in previous data reports; data files are described in Part 5. Note that a sound speed of 1498 ms<sup>-1</sup> is used for all depth calculations.

#### 3.4.3 ADCP

The acoustic Doppler current profiler (ADCP) instrumentation is described in previous data reports. Logging parameters are summarised in Table 3.6, while data results for this cruise will be discussed in a future report.

## Table 3.6: ADCP logging parameters.

ping parameters bottom track ping parameters

no. of bins: 60 no. of bins: 128 bin length: 8 m bin length: 4 m pulse length: 8 m pulse length: 32 m

delay: 4 m

ping interval: minimum ping interval: same as profiling pings

reference layer averaging: bins 8 to 13 ensemble averaging duration: 3 min.

# 3.5 MAJOR PROBLEMS ENCOUNTERED

After completion of station 6 at the southernmost end of the SR3 transect, the ship encountered thick pack ice while attempting to head northward. At one point the ship became stuck on top of an ice pressure ridge. Ballast waters were shifted and the vessel was freed after a total delay of 15 hours. No major logistical problems were encountered for the remainder of the voyage, with all scheduled work being completed.

The only significant problem with the instrumentation was the large amount of unusable CTD dissolved oxygen data. These bad data often occurred near the bottom of casts. Figure 3.2 summarises the spatial coverage of good CTD dissolved oxygen data (note that bottle dissolved oxygen data is good for the entire transect).

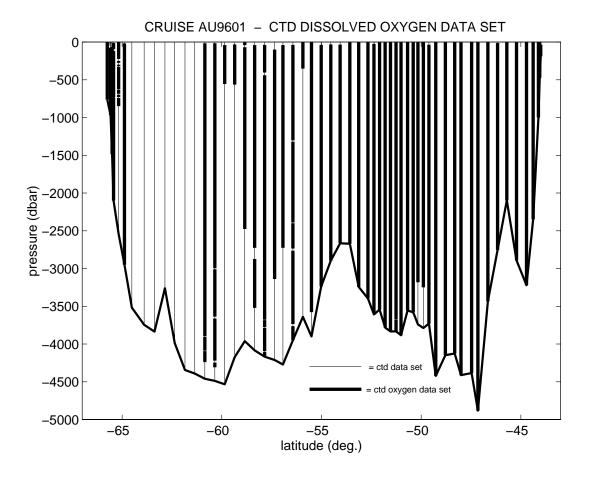


Figure 3.2: CTD dissolved oxygen data coverage along SR3 transect for cruise AU9601.

## 3.6 CTD RESULTS

This section details information relevant to the creation and quality of the final CTD and hydrology data set. For actual use of the data, the following is important:

```
CTD data - Tables 3.14 and 3.15, and Table 3.7; hydrology data - Tables 3.19 and 3.20.
```

Historical data comparisons are made in Part 4 of this report. Data file formats are described in Part 5.

#### 3.6.1 CTD measurements - data creation and quality

The final calibration results for conductivity/salinity and dissolved oxygen, along with the performance check for temperature, are plotted in Figures 3.3 to 3.6 (see Part 1 of this report for further details of the parameters plotted). For conversion to WOCE data file formats, see Part 5 of this report.

#### 3.6.1.1 Conductivity/salinity

The conductivity calibration for CTD 1103 (stations 4 to 69) was of high quality (Figures 3.4 and 3.5), due in part to stable performance of the new Guildline salinometer. Note that for stations 10 to 21, the CTD conductivity cell was slightly fouled (the fouling was not discovered until after completion of station 21). This fouling resulted in a pressure dependent conductivity residual after initial calibration. An extra fit (Table 3.9) was applied to remove this residual, following the same method as described in Part 1 (section 1.6.1.1) of this report.

A small discontinuity of the order 0.0018 (PSS78) may exist in the CTD salinity data between stations 1-23 and stations 24-69 due to differences in International Standard Seawater batches, as described in section 3.6.2 below.

For test stations 1 and 2 using CTD 1193, CTD salinity accuracy is diminished (accurate to ~0.01 (PSS78)) as the only salinity samples available for calibration were collected from a single depth at station 1. For the test stations 3, 70 and 71, no bottle data are available for calibration of the CTD.

At ~580 dbar on the downcast of station 62, the ship's engine shutdown and all power was lost, leaving the ship adrift. The downcast was resumed approximately 2 hours later without retrieving the CTD. A small discontinuity at ~580 dbar may therefore be present in all parameters due to any local horizontal gradients.

# 3.6.1.2 Temperature

Platinum temperature sensor performance of the CTD's was stable throughout the cruise, with a moderate mean offset between thermometer and CTD temperature values (Figure 3.3).

#### 3.6.1.3 Dissolved oxygen

The final standard deviation value of the dissolved oxygen residuals (Figure 3.6) is less than 1% of full scale values (where full scale is approximately equal to 250  $\mu$ mol/l for pressure > 750 dbar, and 350  $\mu$ mol/l for pressure < 750 dbar). Unusual calibration coefficient values were found for some stations (Table 3.17), in particular for station 30 where the coefficient K<sub>5</sub> >> 1. CTD dissolved oxygen calibration for this station was of a lower quality than for other stations.

## 3.6.1.4 Summary of CTD data creation

Information relevant to the creation of the calibrated CTD data is tabulated, as follows:

- \* Surface pressure offsets calculated for each station are listed in Table 3.8.
- \* CTD conductivity calibration coefficients, including the station groupings used for the conductivity calibration, are listed in Tables 3.9 and 3.10.
- \* CTD raw data scans flagged for special treatment are listed in Table 3.11.
- \* Missing 2 dbar data averages are listed in Table 3.12.
- \* 2 dbar bins which are linearly interpolated from surrounding bins are listed in Table 3.13.
- \* Suspect 2 dbar averages are listed in Tables 3.14 and 3.15.
- \* CTD dissolved oxygen calibration coefficients are listed in Table 3.16. The starting values used for the coefficients prior to iteration, and the coefficients varied during the iteration, are listed in Table 3.17.
- \* The different protected and unprotected thermometers used for the stations are listed in Table 3.21.
- \* The pressure and temperature laboratory calibration coefficients for the CTD's used are listed in Table 3.22.

#### 3.6.1.5 Summary of CTD data quality

CTD data quality cautions for the various parameters are summarised in Table 3.7.

Table 3.7: Summary of cautions to CTD data quality.

station no.	CTD parameter	caution
1,2	salinity	test cast - all bottles fired at same depth; salinity accuracy reduced
10-21	salinity	additional correction applied for pressure dependent conductivity residual
30	oxygen	oxygen calibration fit fairly poor
62	all	ship broke down - will be a discontinuity in downcast due to horizontal drift
1-23/24-69	salinity	discontinuity in salinity data of 0.0018 (PSS78) between the 2 station groups due to ISS batch difference
1-40	oxygen	values larger than for remaining stations by ~4μmol/l

## 3.6.2 Hydrology data

Quality control information relevant to the hydrology data is tabulated, as follows:

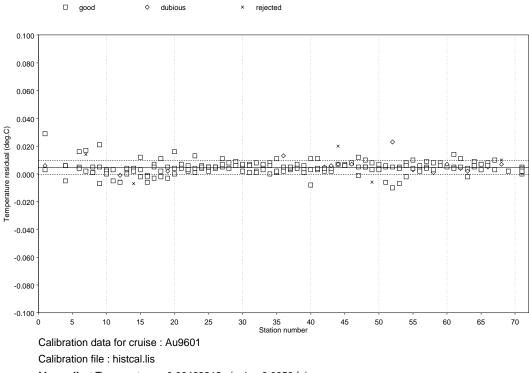
- \* Dissolved oxygen Niskin bottle samples flagged with the code -9 (rejected for CTD dissolved oxygen calibration) are listed in Table 3.18.
- \* Questionable dissolved oxygen and nutrient Niskin bottle sample values are listed in Tables 3.19 and 3.20 respectively. Note that questionable values are included in the hydrology data file, whereas bad values have been removed.

Laboratory temperature on the ship was stable, with lab temperatures at the times of nutrient analyses having a most common value of 20°C.

International Standard Seawater (ISS) batch P128 (18th July 1995)) was used for salinity sample analyses of stations 1-23, while batch P130 (21st March 1996) was used for stations 24-69. Standardisation values on the salinometer were consistently different for these two ISS batches, indicating a problem with one of the batches. A discontinuity is therefore present in salinity bottle values, with station 24-69 values higher than station 1-23 values by 0.0018 ±0.0003 (PSS78). It is not known which ISS batch is at fault.

For dissoved oxygen data, stations 1 to 40 bottle values (and therefore CTD values also) are ~4µmol/l larger than for the remaining stations 41 to 69. Note that a jump in standardisation values for the laboratory analyses occurred between stations 40 and 41, accounting for the two groups of dissolved oxygen data. See Part 4 of this report for a more detailed discussion.

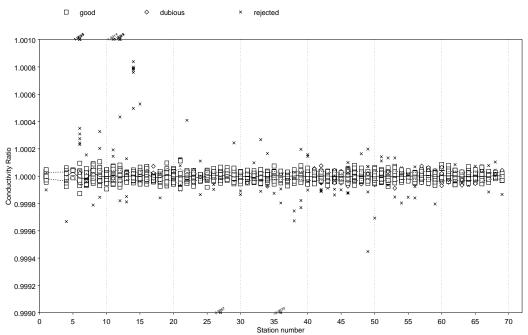
For stations 16 and 17 nutrient data, autoanalyser peak heights were measured manually.



Mean offset Temperature = 0.00463312c (s.d. = 0.0050 °c)

Number of samples used = 187 out of 193

<u>Figure 3.3:</u> Temperature residual ( $T_{therm}$  -  $T_{cal}$ ) versus station number for cruise au9601. The solid line is the mean of all the residuals; the broken lines are  $\pm$  the standard deviation of all the residuals (see CTD methodology). Note that the "dubious" and "rejected" categories refer to the conductivity calibration.

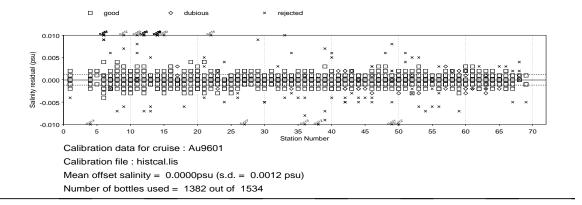


Calibration data for cruise : Au9601

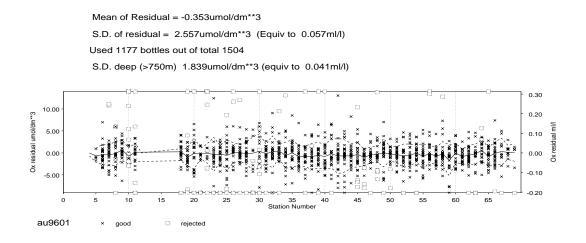
Calibration file : histcal.lis Conductivity s.d. = 0.00003

Number of bottles used = 1382 out of 1534 Mean ratio for all bottles = 1.00000

<u>Figure 3.4:</u> Conductivity ratio  $c_{btl}/c_{cal}$  versus station number for cruise au9601. The solid line follows the mean of the residuals for each station; the broken lines are  $\pm$  the standard deviation of the residuals for each station (see CTD methodology).



<u>Figure 3.5:</u> Salinity residual ( $s_{btl}$  -  $s_{cal}$ ) versus station number for cruise au9601. The solid line is the mean of all the residuals; the broken lines are  $\pm$  the standard deviation of all the residuals (see CTD methodology).



<u>Figure 3.6:</u> Dissolved oxygen residual ( $o_{btl}$  -  $o_{cal}$ ) versus station number for cruise au9601. The solid line follows the mean residual for each station; the broken lines are  $\pm$  the standard deviation of the residuals for each station (see CTD methodology).

<u>Table 3.8:</u> Surface pressure offsets (as defined in the CTD methodology).

stn	surface p	stn	•		surface p offset (dbar)		surface p
no.	offset (dbar)	no.	offset (dbar)				offset (dbar)
1	0.78	19	-2.68	37	-2.92	55	-2.66
2	0.61	20	-3.07	38	-2.84	56	-2.70
3	0.77	21	-2.73	39	-2.42	57	-3.18
4	-2.55	22	-2.20	40	-2.50	58	-3.08
5	-2.06	23	-2.71	41	-3.00	59	-2.69
6	-2.41	24	-2.60	42	-2.03	60	-2.77
7	-2.31	25	-2.65	43	-2.61	61	-3.19
8	-2.16	26	-2.85	44	-2.95	62	-2.81
9	-2.27	27	-2.69	45	-2.78	63	-3.15
10	-2.67	28	-2.52	46	-2.64	64	-3.01
11	-2.57	29	-2.99	47	-2.96	65	-3.02
12	-2.83	30	-2.89	48	-2.68	66	-3.13
13	-2.71	31	-3.25	49	-3.11	67	-3.13
14	-2.68	32	-2.88	50	-2.59	68	-3.35
15	-2.80	33	-3.28	51	-2.74	69	-3.15
16	-2.54	34	-2.59	52	-3.07	70	0.89
17	-2.70	35	-3.05	53	-3.31	71	0.41
18	-2.67	36	-2.69	54	-2.47		

<u>Table 3.9:</u> CTD conductivity calibration coefficients.  $F_1$ ,  $F_2$  and  $F_3$  are respectively conductivity bias, slope and station-dependent correction calibration terms. n is the number of samples retained for calibration in each station grouping;  $\sigma$  is the standard deviation of the conductivity residual for the n samples in the station grouping (see CTD methodology);  $\sigma$  is the correction applied to CTD conductivities due to pressure dependence of the conductivity residuals (see eqn 1.1 in Part 1 of this report).

stn grouping	F <sub>1</sub>	$F_2$	$F_3$	n	σ	α
001 to 001	74396631	0.98848575E-03	0	19	0.000758	-
002 to 002	74396631	0.98848575E-03	0	19	0.000758	-
003 to 003	-			-	-	-
004 to 009	0.38105131E-01	0.10026968E-02	17129059E-07	109	0.001151	-
010 to 012	0.29464364E-01	0.10029643E-02	42023366E-07	63	0.001082	-1.72220E-06
013 to 014	0.22334088E-01	0.10031561E-02	28439980E-07	38	0.000808	-2.89414E-06
015 to 017	0.25912709E-01	0.10022619E-02	0.54122684E-07	71	0.000975	-3.23843E-06
018 to 021	0.17743922E-01	0.10042234E-02	38849067E-07	89	0.001224	-1.25810E-06
022 to 023	0.10979836E-02	0.10062176E-02	14796191E-07	45	0.000810	-
024 to 033	12532344E-01	0.10063905E-02	61267260E-10	224	0.000741	-
034 to 037	0.20512016E-02	0.10060457E-02	32684513E-08	83	0.000750	-
038 to 040	27578964E-01	0.10069364E-02	12822740E-08	60	0.000879	-
041 to 042	24668828E-01	0.10063144E-02	0.13021786E-07	41	0.000940	-
043 to 047	19096958E-01	0.10068804E-02	42245725E-08	106	0.000944	-
048 to 049	20424480E-01	0.10065386E-02	0.38684723E-08	40	0.000814	-
050 to 053	34297624E-01	0.10072630E-02	15337700E-08	86	0.001002	-
054 to 056	18440140E-01	0.10073180E-02	11331976E-07	61	0.000756	-
057 to 059	19465081E-01	0.10061536E-02	0.94647529E-08	68	0.000993	-
060 to 061	17832191E-01	0.10045096E-02	0.35861141E-07	45	0.001197	-
062 to 065	18907083E-01	0.10069848E-02	42532668E-08	89	0.000932	-
066 to 069	19880267E-01	0.10067129E-02	0.65647745E-09	45	0.001026	-
070 to 070	74396631	0.98848575E-03	0	19	0.000758	-
071 to 071	74396631	0.98848575E-03	0	19	0.000758	-

<u>Table 3.10:</u> Station-dependent-corrected conductivity slope term ( $F_2 + F_3$ . N), for station number N, and  $F_2$  and  $F_3$  the conductivity slope and station-dependent correction calibration terms respectively.

stn	$(F_2 + F_3 . N)$						
no.		no.		no.		no.	
1	0.98848575E-03	19	0.10034853E-02	37	0.10059247E-02	55	0.10066947E-02
2	0.98848575E-03	20	0.10034465E-02	38	0.10068877E-02	56	0.10066834E-02
3	-	21	0.10034076E-02	39	0.10068864E-02	57	0.10066931E-02
4	0.10026283E-02	22	0.10058920E-02	40	0.10068851E-02	58	0.10067025E-02
5	0.10026112E-02	23	0.10058772E-02	41	0.10068483E-02	59	0.10067120E-02
6	0.10025940E-02	24	0.10063891E-02	42	0.10068613E-02	60	0.10066612E-02
7	0.10025769E-02	25	0.10063890E-02	43	0.10066988E-02	61	0.10066971E-02
8	0.10025598E-02	26	0.10063890E-02	44	0.10066946E-02	62	0.10067211E-02
9	0.10025426E-02	27	0.10063889E-02	45	0.10066903E-02	63	0.10067169E-02
10	0.10025441E-02	28	0.10063888E-02	46	0.10066861E-02	64	0.10067126E-02
11	0.10025021E-02	29	0.10063888E-02	47	0.10066819E-02	65	0.10067084E-02
12	0.10024601E-02	30	0.10063887E-02	48	0.10067243E-02	66	0.10067563E-02
13	0.10027864E-02	31	0.10063886E-02	49	0.10067281E-02	67	0.10067569E-02
14	0.10027579E-02	32	0.10063886E-02	50	0.10071863E-02	68	0.10067576E-02
15	0.10030737E-02	33	0.10063885E-02	51	0.10071848E-02	69	0.10067582E-02
16	0.10031278E-02	34	0.10059345E-02	52	0.10071833E-02	70	0.98848575E-03
17	0.10031819E-02	35	0.10059313E-02	53	0.10071817E-02	71	0.98848575E-03
18	0.10035242E-02	36	0.10059280E-02	54	0.10067060E-02		

<u>Table 3.11:</u> CTD raw data scans flagged for special treatment (see previous data reports for explanation).

oxpia.iaii.				
station	approximate		action	reason
number	pressure (dbar)	numbers	taken	
	22	44044 44000 44000 44400		
4	98	14011-14220,14392-14422	•	wake effect in steep gradient
4	106	15123-15275	ignore	wake effect in steep gradient
5	6-41	8352-13559	ignore	preliminary dip to 41 dbar
5	110	17848-18017	ignore	wake effect in steep gradient
6	3-30	2605-8552	ignore	preliminary dip to 30 dbar
6	11-16	2633-9148	ignore	fouling of cond. cell
7	8-22	2313-6115	ignore	preliminary dip to 22 dbar
8	9-28	1534-5118	ignore	preliminary dip to 28 dbar
9	9-40	6951-13639	ignore	preliminary dip to 40 dbar
11	10-158	11617-31172	ignore	preliminary dip to 158 dbar
12	9-31	3185-8956	ignore	preliminary dip to 31 dbar
14	9-25	1987-6352	ignore	preliminary dip to 25 dbar
17	9-33	3939-9105	ignore	preliminary dip to 33 dbar
19	7-39	4544-9809	ignore	preliminary dip to 39 dbar
20	8-35	3049-7411	ignore	preliminary dip to 35 dbar
28	1302-1354	74227-76421	ignore	fouling of cond. cell
29	8-30	5451-9404	ignore	preliminary dip to 30 dbar
34	576	57543-57686	ignore	fouling of cond. cell
58	329	30437-30772	ignore	fouling of cond. cell
62	199	19731-19995	ignore	fouling of cond. cell
66	226	22795-22871	ignore	fouling of cond. cell
71		81471-7,81548-81620,8168		
71		81780-2,81753-81768	ignore	bad data
71		125721-3,126067-126114	ignore	bad data

<u>Table 3.12:</u> Missing data points in 2 dbar-averaged files. "1" indicates missing data for the indicated parameters: T=temperature; S=salinity,  $\sigma_T$ , specific volume anomaly and geopotential anomaly; O=dissolved oxygen. Note that jmin is the minimum number of data points required in a 2 dbar bin to form the 2 dbar average (see CTD methodology).

station	pressures (dbar)				reason
numbe	· · · · · · · · · · · · · · · · · · ·	Т	S	0	
	3				
1,2	entire profile			1	no bottles for oxygen calibration
3	entire profile	1	1	1	no calibration data
4	2	1	1		bad data
4	entire profile			1	CTD oxygen hardware fault
5	2,4	1	1		bad data
5	2-14			1	bad data
6	2	1	1		bad data
7	2-8	1	1		bad data
7	2,22-32,46-72			1	bad data
8	2-58			1	bad data
9	2-8	1	1		bad data
9	2-12,98-116			1	bad data
10	226-248,278-298,324-328			1	bad data
10	626-630,688-696,730-738			1	bad data
10	852-bottom			1	bad data
11	2	1	1	•	bad data
11	2-16	•	•	1	bad data
12	2,4	1	1	•	bad data
14	2,4	1	1		bad data
15-18	2	1	1		bad data
12-18	entire profile	•	•	1	bad data
19	2-14,3898-3902,4090-4092			1	bad data
19	4242-bottom			1	bad data
20	2	1	1	ı	bad data
20	2-14,2998-3008,3640-3660	'	'	1	bad data
20				1	
21	4222-4244,4310-bottom 2	1	1	1	bad data
21		ı	'	4	bad data
22	2-38,558-bottom 2	1	1	1	bad data
22		ı	'	4	bad data bad data
	2-30,566-bottom	4	4	1	
23	2,4	1	1	4	bad data
23	2,44-66,2478-bottom	4	4	1	bad data
24	2,4	1	1		bad data
24	2-38,2728-2872,3524-bottom			1	bad data
25	2-36,406-438,3680-3682	00		1	bad data
25	3780-3786,4096-4102,4162-410	08		1	bad data
26	2-98,3142-bottom			1	bad data
27	2-38,2728-bottom		4	1	bad data
28	2	1	1		bad data
28	1304-1318	1	1		fouling of conductivity cell
28	2-36,1304-1318,3738-3762			1	bad data
28	2392-2398,2738-2762			1	bad data
29	354-bottom			1	bad data
30	2	1	1		bad data
30	2,3580-bottom			1	bad data
31	2,4	1	1		bad data
31	2-36			1	bad data
32	2	1	1		bad data
32	2-30			1	bad data
33	2-32			1	bad data

Table 3.12: (continued)

station	pressures (dbar)				reason
number	where data missing	Т	S	0	
24	0	4	4	4	had data
34	2 2	1 1	1 1	1	bad data
36 37		- 1	ı	1	bad data
	4-24,3588-bottom 2	1	4	1	bad data
38		- 1	1	1	bad data
39 39	2,4	4	4	1	bad data
39 40	3782 2	1 1	1	1	no. of data pts in 2dbar bin < jmin bad data
40 41		- 1	1	1	
41 42	3678 2	4	1	1 1	bad data
42 45	2	1	1	ı	bad data
45 45		'	1	1	bad data bad data
45 46	2,3184-bottom			1 1	bad data bad data
40 47,48	2,3252-bottom 2	1	1	ı	bad data
47,40	3400-bottom	1	1	1	bad data
40 49		1	1	ı	bad data bad data
49 50	2,4 2	1	1		bad data
50	2,3352-bottom	'	1	1	bad data
50 52-54	2,3332-50110111	1	1	1	bad data
52-5 <del>4</del> 52	2,4	'	'	1	bad data
53	2,4			1	bad data
54	2-34			1	bad data
5 <del>4</del> 58	2	1	1	'	bad data
58	2,4	'	'	1	bad data
60	2			1	bad data
62	2	1	1	'	bad data
62	2-10	'	•	1	bad data
64	2	1	1	1	bad data
67	2	1	1	'	bad data
69	2	1	1		bad data
69	2-32	'	'	1	bad data
70	entire profile	1	1	1	no calibration data
70 71	entire profile	1	1	1	no calibration data
, ,	orano promo	•	•	•	no balloration data

<u>Table 3.13:</u> 2 dbar averages interpolated from surrounding 2 dbar values, for the indicated parameters.

station	interpolated	parameters
number	2 dbar values	interpolated
20	3692	T, S

<u>Table 3.14a:</u> Suspect 2 dbar salinity averages (+ temperature where indicated). Note: for suspect salinity values, the following are also suspect:  $\sigma_T$ , specific volume anomaly, and geopotential anomaly.

station	suspect 2 db	oar values (dbar)	reason
number	•	guestionable	
4	-	90,92	salinity spike in steep local gradient
5	-	98,100,106	salinity spike in steep local gradient
5	-	114,116,120	salinity spike in steep local gradient
6	-	6-10	possible fouling of conductivity cell
7	-	800-804,820,82	8 salinity spike in steep local gradient
7	826	-	salinity spike in steep local gradient
14	70	-	salinity spike in steep local gradient
15	76	-	salinity spike in steep local gradient
15	-	78,80	salinity spike in steep local gradient
17	110	-	salinity spike in steep local gradient
19	-	136-142	salinity spike in steep local gradient
20	-	100-106,114	salinity spike in steep local gradient
20	-	128,130,136	salinity spike in steep local gradient
22	-	150,152,162,16	4 salinity spike in steep local gradient
39	144	-	salinity spike in steep local gradient
43	656,692	2 -	salinity spike in steep local gradient
52	-	178,292	salinity spike in steep local gradient
60	-	1160,1276-1280	0 salinity spike in steep local gradient
60	-	1322-1326	salinity spike in steep local gradient
65	-	1010,1014	salinity spike in steep local gradient
65	1012	-	salinity spike in steep local gradient

<u>Table 3.14b:</u> Suspect 2 dbar-averaged data from near the surface (applies to all parameters other than dissolved oxygen, except where noted).

stn	suspec	t 2dbar values	•	stn	suspec	t 2dbar values
no.	bad	<u>questionable</u>		<u>no.</u>	bad	<u>questionable</u>
4	-	4-10		52	4	-
5	-	6		53	-	4
6	-	6-10		54	-	4
8	2	-		56	2	-
11	-	4		58	-	4
12	-	6,8		59	2	-
16	-	4 (T okay)		60	-	2 (T okay)
18	-	4,6		61	-	2
19	2-6	-		62	-	4
20	4,6	-		63	-	2
21	4-8	10-14		65	-	2
22	4	-		66	2	4
24	6	-		67	-	4
25	-	2		68	-	2,4
26	-	2,4		69	-	4
27	-	2				
29	2	-				
35	2	4,6				
37	-	2-6				
41	-	2				
42	4	6-10				
44	-	2				
46	2	-				
47	-	4				
48	4	-				
50	4	-				

Table 3.15: Suspect 2 dbar-averaged dissolved oxygen data.

stn s	suspect 2	dbar values(dbar)	stn su	spect 2	dbar values(dbar)
no.	bad o	questionable	no.	bad (	questionable
6	-	4	41	-	2
20	-	58-62,80-82	42	-	4,6,12-34
23	6-18	-	43	-	2
29	-	2-8	44	2-10	-
30	-	4-56,2176-3578	46	-	4-10
34	-	4-8	50	-	12-32
35	-	38,40,52,54,68	51	-	2-6
36	-	4	56	-	2
37	-	34,36	57	-	2-34
38	-	14-18	60	-	4-10
39	-	12-24			
40	-	4,6			

<u>Table 3.16:</u> CTD dissolved oxygen calibration coefficients.  $K_1$ ,  $K_2$ ,  $K_3$ ,  $K_4$ ,  $K_5$  and  $K_6$  are respectively oxygen current slope, oxygen sensor time constant, oxygen current bias, temperature correction term, weighting factor, and pressure correction term. dox is equal to 2.8 $\sigma$  (for  $\sigma$  as defined by eqn A2.24 in the CTD methodology); n is the number of samples retained for calibration in each station or station grouping.

station	$K_1$	$K_2$	$K_3$	$K_{\!\scriptscriptstyle 4}$	$K_5$	$K_6$	dox	n
numbe	r							
1-4	-	-	-	-	-	-	-	-
5	7.977	5.00	-0.903	-0.15206	0.65057	0.19386E-03	0.086	07 4
6	2.216	5.00	0.250	-0.13008	0.25629	0.53099E-04	0.145	67 24
7	0.922	5.00	0.502	-0.12390	0.11961	0.12705E-04	0.149	44 22
8	0.942	5.00	0.632	-0.22443	0.48146	0.19279E-04	0.169	80 19
9	3.650	8.00	0.315	-0.31208	0.74841	0.45625E-04	0.145	80 24
10	1.181	5.00	0.484	-0.10030	0.20991	-0.46710E-04	0.113	10 10
11	7.372	8.00	-0.984	-0.03645	0.12896	0.13085E-03	0.131	12 18
12-18	-	-	-	-	-	-		-
19	9.970	5.00	-1.309	-0.13446	0.71125	0.10492E-03	-	24 20
20	10.893	5.00	-1.574	-0.10461	0.68169	0.10988E-03		49 20
21	8.782	7.00	-1.164	-0.10375	0.27859	0.23859E-03	0.077	
22	10.780	8.00	-1.159	-0.18501	0.74659	-0.30282E-03	0.136	
23	13.095	5.00	-1.881	-0.14275	0.71999	0.12092E-03		83 18
24	13.788	8.00	-2.059	-0.15753	0.45006	0.11444E-03		85 21
25	15.839	8.50	-2.414	-0.17273	0.61228	0.12524E-03		87 21
26	10.964	6.00	-1.593	-0.08905	0.50065	0.13016E-03		54 18
27	14.482	6.00	-2.076	-0.17650	0.51565	0.63161E-04		09 22
28	11.079	6.00	-1.659	-0.04909	1.23120	0.15427E-03		71 23
29	11.232	8.00	-1.723	-0.02111	0.71090	0.28299E-03	0.233	
30	12.399	5.00	-1.917	-0.04067	3.41140	0.21041E-03		99 15
31	13.137	5.00	-1.984	-0.09521	0.92360	0.14840E-03		21 23
32	12.151	5.00	-1.818	-0.07098	0.31861	0.12694E-03		56 21
33	11.447	5.00	-1.684	-0.06222	0.20779	0.12393E-03		20 22
34	14.974	7.00	-2.250	-0.14137	0.93157	0.14922E-03		63 22
35	13.503	5.00	-2.034	-0.10348	1.55730	0.18499E-03		44 23
36	13.167	5.00	-1.952	-0.11089	0.93079	0.14698E-03		66 22
37	12.810	5.00	-1.897	-0.09934	0.92874	0.14852E-03	-	93 22
38	13.964	5.00	-2.049	-0.14110	1.10950	0.14467E-03		74 22
39	12.315	5.00	-1.779	-0.11737	1.15650	0.14835E-03		01 22
40	12.799	5.00	-1.872	-0.10613	0.84008	0.12872E-03		78 22
41	13.666	5.00	-2.016	-0.12765	0.92883	0.13385E-03	0.202	48 23

Table 3.16: (continued)

station number	. K <sub>1</sub>	$K_2$	$K_3$	K <sub>4</sub>	K <sub>5</sub>	K <sub>6</sub>	dox	n
42	13.239	5.00	-1.985	-0.11293	0.88499	0.15201E-03	0.251	77 24
43	12.990	5.00	-1.931	-0.11076	0.91703	0.15071E-03	0.231	18 24
44	12.650	8.00	-1.860	-0.10660	0.91335	0.13240E-03	0.178	77 23
45	11.968	5.00	-1.835	-0.05606	0.39845	0.16464E-03	0.174	34 20
46	11.624	5.00	-1.703	-0.08886	0.93062	0.15078E-03	0.115	77 20
47	11.238	5.00	-1.651	-0.07039	0.76785	0.14245E-03	0.113	52 23
48	10.654	5.00	-1.527	-0.07438	0.89526	0.14189E-03	0.113	96 20
49	10.460	5.00	-1.513	-0.06562	1.00040	0.15150E-03	0.202	95 22
50	13.487	5.00	-2.003	-0.13628	1.12640	0.16671E-03	0.099	98 22
51	11.429	5.00	-1.674	-0.07639	0.87000	0.14268E-03		57 24
52	13.893	5.00	-2.011	-0.16381	1.21440	0.15485E-03	0.161	97 22
53	11.973	5.00	-1.723	-0.09890	0.99061	0.13249E-03	0.161	67 24
54	8.123	5.00	-1.096	-0.03568	0.97237	0.12951E-03	0.121	16 22
55	10.257	5.00	-1.441	-0.07503	0.92291	0.12490E-03	0.185	00 24
56	13.329	5.00	-2.015	-0.10473	0.80404	0.14212E-03	0.123	78 22
57	11.954	5.00	-1.764	-0.09596	0.91435	0.14067E-03	0.124	76 24
58	14.906	5.00	-2.207	-0.15879	1.00730	0.13214E-03	0.174	53 23
59	12.717	8.00	-1.914	-0.09111	0.77570	0.14559E-03	0.218	16 24
60	14.505	5.00	-2.192	-0.13230	0.92839	0.14503E-03	0.138	44 22
61	11.118	5.00	-1.613	-0.08351	0.90790	0.14216E-03	0.110	00 24
62	10.148	5.00	-1.437	-0.08017	1.05690	0.15153E-03	0.142	61 23
63	9.048	5.00	-1.232	-0.06994	1.18910	0.11739E-03	0.138	47 19
64	11.613	8.00	-1.851	-0.05570	0.79147	0.15911E-03	0.153	17 22
65	10.876	5.00	-1.562	-0.07559	0.92785	0.14065E-03	0.139	97 23
66	10.325	5.00	-1.345	-0.11909	1.18150	0.10524E-03	0.157	32 23
67	10.556	5.00	-1.583	-0.05825	0.93328	0.18770E-03	0.193	00 11
68-69	5.606	5.00	-0.384	-0.03367	0.95645	0.57658E-04	0.110	08 15

<u>Table 3.17:</u> Starting values for CTD dissolved oxygen calibration coefficients prior to iteration, and coefficients varied during iteration (see CTD methodology). Note that coefficients not varied during iteration are held constant at the starting value.

station numbe	r K <sub>1</sub>	K <sub>2</sub>	K <sub>3</sub>	$K_{4}$	<b>K</b> <sub>5</sub>	$K_{6}$	coe vari	efficients ed
1-4	-	-	-	-	-	-	,	-
5	8.900	5.0000	-0.700	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
6	5.200	5.0000	1.000	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
7	4.000	5.0000	1.300	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
8	3.600	5.0000	1.300	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
9	3.400	8.0000	0.900	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
10	2.100	5.0000	0.700	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
11	7.420	8.0000	-0.960	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
12-18	-	-	-	-	-	-		-
19	10.240	5.0000	-1.100	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
20	12.500	5.0000	-1.300	-0.400E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
21	10.800	7.0000	-0.800	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
22	9.800	8.0000	-0.900	-0.450E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
23	12.700	5.0000	-1.500	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
24	8.300	8.0000	-0.350	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$

Table 3.17: (continued)

station numbe	K <sub>1</sub>	K <sub>2</sub>	K <sub>3</sub>	$K_4$	K <sub>5</sub>	$K_6$	coe vari	fficients ed
25	15.600	8.5000	-2.200	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
26	11.900	6.0000	-1.400	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
27	13.900	6.0000	-1.900	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
28	11.200	6.0000	-1.600	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
29	11.200	8.0000	-1.700	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
30	12.150	5.0000	-1.800	-0.370E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
31	14.100	5.0000	-1.700	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_{3}^{3} K_{4}^{4} K_{5}^{3} K_{6}^{6}$
32	13.800	5.0000	-1.400	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
33	12.900	5.0000	-1.300	-0.360E-01	0.750	0.15000E-03	K₁ .	$K_3 K_4 K_5 K_6$
34	14.000	7.0000	-1.700	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
35	14.900	5.0000	-1.700	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
36	13.800	5.0000	-1.700	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
37	14.100	5.0000	-1.700	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
38	14.900	5.0000	-2.100	-0.360E-01	0.900	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
39	13.500	5.0000	-1.900	-0.380E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
40	13.110	5.0000	-1.600	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
41	14.100	5.0000	-2.000	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
42	13.700	5.0000	-1.800	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
43	13.600	5.0000	-1.800	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
44	13.550	8.0000	-1.850	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
45	12.300	5.0000	-1.800	-0.400E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
46	12.900	5.0000	-1.450	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$
47	12.500	5.0000	-1.200	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
48	12.000	5.0000	-1.050	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
49	12.600	5.0000	-1.400	-0.360E-01	0.770	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
50	14.400	5.0000	-2.100	-0.550E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
51	12.900	5.0000	-1.400	-0.360E-01	0.750	0.15000E-03	K <sub>1</sub>	$K_3 K_4 K_5 K_6$
52	14.500	5.0000	-2.000	-0.700E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
53	12.800	5.0000	-1.500	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
54	8.000	5.0000	-1.100	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
55	11.700	5.0000	-1.200	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
56 57	13.800	5.0000	-2.000	-0.360E-01	0.550	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
57 58	13.000	5.0000	-1.700	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
	16.200	5.0000	-2.350 -1.800	-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
59	14.300	8.0000		-0.360E-01	0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
60 61	14.500 12.300	5.0000 5.0000	-2.100 -1.300	-0.360E-01 -0.360E-01	0.750	0.15000E-03 0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
62	11.600	5.0000	-1.100	-0.360E-01	0.750 0.750	0.15000E-03	K₁	$K_3 K_4 K_5 K_6$
63	10.700	5.0000	-1.100	-0.360E-01	0.750	0.15000E-03	K₁ K₁	$K_3 K_4 K_5 K_6$ $K_3 K_4 K_5 K_6$
64	11.400	8.0000	-1.900	-0.360E-01	0.750	0.15000E-03	K₁ K₁	$K_3 K_4 K_5 K_6$ $K_3 K_4 K_5 K_6$
65	12.500	5.0000	-1.200	-0.360E-01	0.730	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$ $K_3 K_4 K_5 K_6$
66	11.400	5.0000	-1.200	-0.360E-01	0.740	0.15000E-03	K₁ K₁	$K_3 K_4 K_5 K_6$ $K_3 K_4 K_5 K_6$
67	10.000	5.0000	-1.800	-0.360E-01	0.750	0.15000E-03	K₁ K₁	$K_3 K_4 K_5 K_6$
68-69	5.600	5.0000	-0.400	-0.360E-01	0.750	0.15000E-03	$K_1$	$K_3 K_4 K_5 K_6$ $K_3 K_4 K_5 K_6$

<u>Table 3.18:</u> Dissolved oxygen Niskin bottle samples flagged as -9 for dissolved oxygen calibration. Note that this does not necessarily indicate a bad bottle sample - in many cases, flagging is due to bad CTD dissolved oxygen data.

station	rosette	station	rosette
number	position	number	position
7	21,9	38	8
8	24,23,22,21,20	39	21,19
10	24,21,13,11-1	40	17
11	24,21,20,19,18,	6 41	18
18	24,20	45	18,3,2,1
19	24,5,2,1	46	15,3,2,1
20	24,21,2,1	47	12
21	24,15-1	48	19,3,2,1
22	20,15-1	49	20
23	6,5,4,3,2,1	50	2,1
24	24,2,1	52	21,20
25	24,20,18	54	24,19
26	24,23,22,21,2,1	56	19,18
27	24,1	58	23
28	24	62	24
29	17-1	63	5,4,3,2,1
30	23,19,7,5,4,3,2,	1 64	7,4
31	24	65	18
32	24	66	19
33	24,19	67	14
34	18	69	12
37	24,1		

<u>Table 3.19:</u> Questionable dissolved oxygen Niskin bottle sample values (not deleted from hydrology data file).

stn no.	rosette position
11	6
13	23
19	5
38	8
64	7,4

Table 3.20: Questionable nutrient sample values (not deleted from hydrology data file).

PHOSPHATE		NITRATE		SILICATE	
station	rosette	station	rosette	station	rosette
number	position	<u>number</u>	position	<u>number</u>	position
6	15,14,13	6	8		
		7	7,5		
				10	6
13	23	13	23	13	23
24	3	24	3		
26	2				
27	9	27	9		
29	22	29	22		
31	4	31	4		
32	4				
		35	2		
		38	9		
		60	4		

<u>Table 3.21:</u> Protected and unprotected reversing thermometers used (serial numbers are listed).

protected thermometers

station rosette position 24 rosette position 12 rosette position 2 numbers thermometers thermometers thermometers 1 to 70 12095,12096 12094 12119,12120

71 12095 (pos. 24); 12096 (pos.17); 12094 (pos.12); 12120 (pos. 7); 12119 (pos. 2)

unprotected thermometers

station rosette position 12 rosette position 2 numbers thermometers thermometers

 1 to 27
 11993
 11992

 28 to 71
 11992
 11993

<u>Table 3.22:</u> Calibration coefficients and calibration dates for CTD serial numbers 1103 and 1193 (unit nos 7 and 5 respectively) used during RSV Aurora Australis cruise AU9601. Note that an additional pressure bias term due to the station dependent surface pressure offset exists for each station (eqn A2.1 in the CTD methodology). Also note that platinum temperature calibrations are for the ITS-90 scale.

CTD serial 1103 (unit no. 7)

CTD serial 1193 (unit no. 5)

coefficient value of coefficient value of coefficient

pressure calibration coefficients pressure calibration coefficients
CSIRO Calibration Facility - 10/07/1996 CSIRO Calibration Facility - 05/0

CSIRO Calibration Facility - 05/07/1996 -1.107604e+01 pcal0 -1.851190e+01 pcal0 pcal1 1.002735e-01 pcal1 1.008327e-01 6.097416e-09 pcal2 pcal2 0.0 pcal3 0.0 pcal3 0.0 0.0 0.0 pcal4 pcal4

platinum temperature calibration coefficients platinum temperature calibration coefficients CSIRO Calibration Facility - 27/06/1996 CSIRO Calibration Facility - 26/06/1996

 Tcal0
 0.28797e-01
 Tcal0
 -0.46860e-01

 Tcal1
 0.49988e-03
 Tcal1
 0.49879e-03

 Tcal2
 0.35049e-11
 Tcal2
 0.27541e-11

pressure temperature calibration coefficients pressure temperature calibration coefficients CSIRO Calibration Facility - 10/07/1996 CSIRO Calibration Facility - 05/07/1996

 Tpcal0
 1.713678e+02
 Tpcal0
 1.299013e+02

 Tpcal1
 -4.239208e-03
 Tpcal1
 -2.541029e-03

 Tpcal2
 1.481513e-08
 Tpcal2
 -7.814892e-09

Tpcal3 0.0 Tpcal3 0.0

coefficients for temperature correction to coefficients for temperature correction to pressure pressure

CSIRO Calibratio	on Facility - 10/07/1996	CSIRO Calibration	n Facility - 05/07/1996
$T_0$	20.00	$T_0$	20.00
S <sub>1</sub>	-9.196843e-06	S <sub>1</sub>	-1.578863e-05

S<sub>1</sub> -9.196843e-06 S<sub>1</sub> -1.5/8863e-05 S<sub>2</sub> -7.818015e-02 S<sub>2</sub> -6.349700e-02

# **APPENDIX 3.1** Hydrochemistry Laboratory Report

Seawater samples were analysed for nutrient concentrations (nitrate plus nitrite, silicate, and phosphate), salinities, and dissolved oxygen concentrations. The methods used are described in Eriksen (1997). A new type of salinometer, improvements to nutrient autoanalyser chemistries, improvements to inter-run quality checks, and improvements to dissolved oxygen methods were implemented on this cruise.

Number of samples analysed:

Nutrients (nitrate plus nitrite, silicate, phosphate): 1520

Salinities: 1560

Dissolved oxygens: 1610

## A3.1.1 NUTRIENTS

The Alpkem auto-analyser performed well on this cruise as did the new version (1.31) of Faspac software. Phosphate, silicate and nitrate + nitrite were analysed for all sites. Nitrate and nitrite were not analysed separately as only three channels could be run concurrently.

A 20 L carbuoy of seawater was filtered through a GFF filter, mixed and sub sampled into 10 ml tubes, then frozen immediately. At least two of these samples were run with each run and used as an in-house quality control. It was found that this sample was stable for the duration of the trip. See Figure A3.1.2 and Table A3.1.2.

The sample racks were covered with aluminium foil when in the sampler, making sure that it was not in contact with the sample. This served to reduce splashing, sample carryover and the possibility of airborne contamination.

On a couple of occasions there was a shift in the baseline on one or more of the channels. This was generally due to either foreign matter or a bubble becoming lodged in the flow cell. For these runs the affected peaks were either measured manually from the chart or repeated.

The temperature of the laboratory near the Auto-analyser was stable, remaining in the range of 19.5 to 20.5 for the voyage.

All channels were run without the colour reagent for at least six sites (approximately 150 samples) to calculate an average background matrix correction. For both nitrate + nitrite and silicate channels there was no significant background matrix, but for phosphate a background matrix of 0.088  $\mu$ mol/l was measured. There has been no correction applied to the phosphate results: this facilitates comparisons with previous cruise results as no corrections have been applied in the past (see Part 4 of this report).

Some modifications were made to the methodology used in previous cruises, as follows.

#### Nitrate + Nitrite

The nitrate + nitrite channel was unstable for the first ten runs, with the bubble pattern breaking down in the cadmium tube. This resulted in poor peak shape and inconsistent results for the QC (quality check) and duplicate samples. The cadmium tube was replaced with a new tube and the duplicate samples were run for the nitrate + nitrite results only. The new cadmium tube resulted in a much better flow pattern with no problems with either duplicate or QC samples.

**Sample :-** Flow rate 0.32 ml/min **Nitrogen :-** Flow rate 0.23 ml/min

Reagent 1:- Imidazole (4.25 g/L) + Hydrochloric acid (1.15 ml/L) + Brij (0.5 ml/L)

Flow rate 0.32 ml/min

Reagent 2:- Sulphanilamide (3.12 g/L) + Hydrochloric acid (31 ml/L) + Brij (0.5 ml/L)

Flow rate 0.16 ml/min

Reagent 3:- N-1 Naphthylethylene di-amine di-hydrochloride (0.31 g/L) + Brij (0.5 ml/L)

Flow rate 0.16 ml/min

**Debubbler:-** Flow rate 0.42 ml/min

## Phosphate

The reagent for the phosphate was changed from a single mixed reagent to two reagents. The ammonium molybdate and sulphuric acid were in reagent one and the ascorbic acid and antimony potassium tartrate were in reagent two. This was done to prolong the working life of the reagents from about 8 hours to at least 24 hours. It also made it easier to do the background matrix correction run. The pH of the system was lowered slightly from what had been used in the past because the buffering effect of the seawater resulted in the pH of the system being raised to a level where the silicate may have interfered with the phosphate chemistry.

On the first couple of runs there was a great deal of peak diffusion, with the trace not coming back to baseline between samples. The system was rebuilt with all tubing connections being checked and redone if necessary. This did not fix the problem to any degree. It was noticed that the heating coil being used was for a silicate channel. This was changed for a phosphate module, which fixed the problem. Although it seems that the heating coils are constructed of the same type of tubing (PEEK) with the phosphate coil being of greater length (which would not account for the problem), and although the sales rep advised that there was no difference that he was aware of, it appears to be the source of the problem.

It was noticed that while there was a need for wetting agent to be used for the system to run smoothly, an excess of the wetting agent caused the baseline both to become noisy and to gradually shift. The wetting agent currently in use is dowfax, which is lauryl sulphate based. It may be worth using straight lauryl sulphate which is in use in other laboratories - it has been noted to depress the sensitivity if in excess, but not to affect the baseline.

On one occasion the Eppendorf syringe used to add the sulphuric acid appeared to have affected the baseline noise level, possibly by plasticisers or contamination being introduced to the reagent. After replacing the syringe the baseline noise returned to its previous level.

Sample :- Flow rate 0. 80 ml/min
Air :- Flow rate 0.23 ml/min
Reagent 1 :- Dowfax (2 ml/L)

Flow rate 0.80 ml/min

Reagent 2:- Ammonium molybdate (5.04 g/L) + Sulphuric acid (56 ml/L)

Flow rate 0.23 ml/min

Reagent 3:- Ascorbic acid (4.56 g/L) + Antimony potassium tartrate (0.1275 g/L)

Flow rate 0.23 ml/min

**Debubbler:-** Flow rate 0. 42 ml/min

#### Silicate

The silicate channel did not give any problems for the duration of the cruise, the only modification to the system being that no acetone was used in the reagent. The silicate channel is currently being heated to 37\_C to stabilise the baseline and improve the duplicate and replicate results. Some more work needs to be done to rule out interferences, such as from phosphate, or other possible errors.

Sample :- Flow rate 0.23 ml/min
Air :- Flow rate 0.23 ml/min

Reagent 1:- Ammonium molybdate (10 g/L) + Sulphuric acid (2.8 ml/L) + Dowfax (1 ml/L)

Flow rate 0.42 ml/min

Reagent 2:- Oxalic acid (50 g/L) + Dowfax (0.5 ml/L)

Flow rate 0.32 ml/min

Reagent 3:- Ascorbic acid (17.6 g/L)

Flow rate 0.42 ml/min

**Debubbler:-** Flow rate 0.60 ml/min

**Sampler :-** Total pumping rate of artificial seawater into the sampler = 3.39 ml/min

Total pumping rate of artificial seawater out of the sampler 5.78 ml/min

Artificial Seawater :- Sodium Chloride (39 g/L)

The oscillating baseline problem which occurs when Faspac is started is still present. Some work was done looking at grounding of detectors and computers, looking at the wiring of ground to the A/D board, and at further shielding, with no success.

The 'glitch' problem with the A/D board at the mid-point voltage was fixed by purchasing a new A/D board from Labtronics. Although the 'glitch' is still present, it is now negligible.

The version of data logging software used, Faspac 1.31, was an improvement on that used on cruise AU9604 (Faspac 1.2). It did not crash, and produced Excel files which did not cause Excel to crash. The Excel files had a text format, which the output from Faspac 1.2 did not have, so Hydro was modified to convert the cells to numbers, using the 'VALUE' command.

The method of making tops was improved. Previously, standards were made up in six 100 ml volumetric flasks, and tops were made up in a 500 ml volumetric flask. The top standard and the 'tops' were nominally the same concentration, but small differences were possible since they were made up separately. Now all the standards but the top standard are made up as previously. The top standard is made in a 500 ml volumetric flask, and this is also used to make the 'tops'. Thus the 'tops' and top standard have the same source, and the only variation should be due to the process of pouring into 10 ml sample tubes. A comparison was made between the top standard made in a 100 ml flask and a 500 ml flask. No difference was seen. The advantage of making the top standard and 'tops' together is that if a run is found to be unstable, corrections can be made by equating 'tops' values with the top standard.

As usual 'tops' were used to monitor intra-run stability of the system. All the tops for all three channels were examined manually by the operator and found to be satisfactory.

A variation from normal data processing was used. As usual Faspac produced .ACF files, and exported data as .XLS files. Normally the .XLS files represent runs, and can have tops extracted to examine run stability, or have the error in the calibration curve. However on this cruise data was cut and pasted from these .XLS files, thus destroying the integrity of run information. If further examination of the data were required it would be necessary to repeat the export process from Faspac. Care would be needed to separate the new intact .XLS files from the old fragmented .XLS files.

## A3.1.2 SALINITIES

A Guildline 'Autosal' salinometer, SN 62549, was used. This was the first time the CRC had used this instrument. The reliability of the instrument was excellent, in contrast to experience with Yeo-Kal salinometers. The instrument was stable enough so that a secondary 'substandard' was not necessary.

A peristaltic pump from Ocean Scientific was used to pump in samples. Pump speeds 1, 2, or 3 were used. There was no difference to the result between these pump speeds if the samples were temperature equilibrated.

The salinometer has a capability of logging data directly to a computer, but this was not used as an interface was not built in time.

The "Hydro" program was modified so that the double conductivity ratio given by the Guildline salinometer could be entered and converted to salinity.

The biggest problem was with bubbles forming on the electrodes of the conductivity cell. These collected mostly in the first and last electrodes. We had been advised by Guildline that the bubbles had no effect, and by Ocean Scientific that a few bubbles would have no effect, but that a lot of bubbles might. Causes of error would be restricting electrical current flow, and changing the volume of seawater within the cell. A quick test showed that a few bubbles made no difference, and CSIRO users have also found this. However, it is not clear to what extent bubbles may eventually affect results, and the cell was debubbled after every crate of 24 samples, and before every standardisation. The cell was debubbled by rinsing with ethanol or ethanol with Brij. Both were equally effective. The ethanol was found to corrode the inlet and outlet tubes of the peristaltic pump, so the inbuilt air pump was used for pumping ethanol. Methanol was also tried, but was not as effective as ethanol.

Two sets of standards were used, P128 and P130. The standards were compared by standardising the instrument with one standard, measuring the other standard, and comparing it with its nominal value. It was found that P128 read 0.0018 +/- 0.0003 (PSS78) higher than P130. The cause of this difference is not known. If the cause is that P128 is more concentrated than its nominal value, then any samples measured with the salinometer standardised with P128 would appear lower than they really are. It is also assumed that any errors in standardisation will result in an offset across the range of measured salinities. If this is also true, then any samples measured with the salinometer standardised with P128 would appear 0.0018 (PSS78) lower than they really are. This would mean a correction of 0.0018 (PSS78) would need to be added on (no correction was applied to the data).

The standardisation values are in Figure A3.1.3. The comparison of P128 and P130 is in Table A3.1.3.

A crate of 24 samples were analysed for calibration of the underway thermosalinograph. This was entered into Hydro as station 300.

#### A3.1.3 DISSOLVED OXYGEN

Dissolved oxygen analyses generally went well. Problems are described below.

By using the READVOLT.BAS program the factors which most affected the current across the electrodes could be observed. It was seen that the position of the beaker and the stirring rate had profound effects, whereas the addition of sodium thiosulfate or potassium biiodate had only moderate effects. This indicated that effort was needed to keep the stirring rate and position of electrodes in the beaker constant.

The magnetic stirrer which had previously been used for the salinity substandard was used for stirring during preparation of the biiodate standard. This meant that the stirring rate control knob on the Dosimat could be left at the same value. Previously stirring of the biiodate standard had been done with the Dosimat magnetic stirrer, so that the actual titration speed always varied slightly, as the stirring rate of standards and samples is different.

The "Newwink" program was modified so that blanks could be done entirely with the single Dosimat base unit. Previously, the 1 mL of biiodate had been added using a manual dispenser. "Hydro" was modified in the handling of sample repeats. It now has the first value as the default value.

As with other cruises there were problems with standardising to WOCE precision. One of the Optifix dispensers had had some extra tubing placed on the end of the tip. Taking this off seemed to improve precision. As has been noted previously, a second Dosimat base unit for dispensing standards would improve the procedure.

Standardisations are shown in Figure A2.1.6 of Appendix 2.1.

# A3.1.4 LABORATORIES

Nutrients, salinities, and dissolved oxygens were analysed in the wet lab, with water purification in the 'photolab.' Nutrients and salinities were performed on the aft bench, on the inboard and outboard sides respectively. Dissolved oxygens were performed over the inboard sink.

## A3.1.5 TEMPERATURE CONTROL AND MEASUREMENT

There were two temperature control units. The first was the lab air conditioner. This was set at around 19\_C. The second was the PID temperature controller, which had a set point of 20.1\_C. The temperature sensor was placed above the salinity crates. The ships air conditioning outlets above the instruments were taped closed. The sea door access to the trawl deck was kept shut. Laboratory temperature was recorded by two Tinytalk units, and measured by two mercury thermometers, an electronic thermometer, and the temperature monitor of the PID controller. An 'indoor/outdoor' electronic thermometer was used to measure fridge and freezer temperatures. One Tinytalk was positioned above the salinity crates for the duration of analysis, the other was moved around for shorter checks. One mercury thermometer was positioned above the salinity crates, the other with the DO instrumentation. An electronic thermometer was also used for spot checks. All the temperature measuring devices were placed together at the start of the cruise. The PID temperature was calibrated, and the devices agreed to within 0.5 C.

The mercury thermometer with the DO instrumentation was in the range of 19.5 to 20.5 C.

The long term Tinytalk recorded 1342 temperature points at 24 minute intervals. The average temperature was 20.9 +/- 0.4 \_C. See Figure A3.1.1 and Table A3.1.1. There was some spatial variation, which had a range of +/- 2\_C among the instrument locations. This was from the bench top to the height of the top of the salinometer.

Table A3.1.1: Laboratory temperature recorder statistics.

Temperature Tinytalk	statistics from
average	20.9
stdev	0.4
%rsd	1.7
min	19.6
max	22.0
range	2.4
% range	11.5

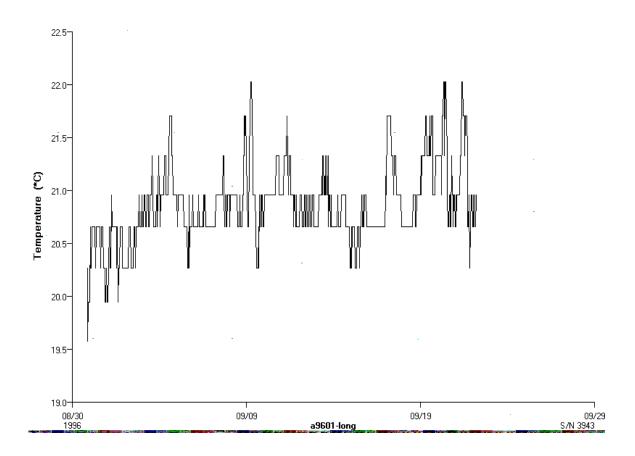


Figure A3.1.1: 'Tinytalk' temperature plot, 24 minute time resolution.

<u>Table A3.1.2:</u> Nutrient samples run as quality checks.

A9601	1	1	_	<b>T</b>	1	1	1
QC's extracted			_	-	_	+	+
QC s extracted	Run	NO3+NO2	-	Sil	_	Phos	_
	Kuii		uM	Volts	uM	Volts	uM
	-	Volts	ulvi	VOITS	uivi	VOITS	uivi
		+	30,52		39.32	+	1.97
average	-						
stdev		+	0.54		0.70	+	0.05
%rsd	-		1.8		1.8	-	2.7
		+	20.47		27.57	+	1.00
min			29.47		37.57		1.88
max			31.94		40.91		2.11
range			2.46		3.33		0.23
range%			8.1		8.5	_	11.6
10404004 1604		2 - 22	24.0	0.44	20.0	0.10	1.00
A9601004.ACM	4	2.62	31.0	2.66	39.9	2.49	1.98
A9601004.ACM	4	2.59	30.6	2.66	40.0	2.49	1.97
A9601005.ACM	5	2.53	30.9	2.66	39.8	2.48	1.96
A9601005.ACM	5	2.47	30.1	2.66	39.8	2.48	1.96
A9601006.ACM	6	2.55	31.0	2.59	40.3		1.93
A9601006.ACM	6	2.49	30.1	2.58	40.0		1.92
A9601007.ACM	7	5.31	30.8	2.58	38.9	2.42	1.98
A9601007.ACM	7	5.22	30.2	2.60	39.2	2.47	2.04
A9601008.ACM	8	5.21	30.2	2.58	38.5	2.42	1.97
A9601008.ACM	8	5.45	31.9	2.62	39.5	2.44	2.00
A9601010.ACM	10	5.57	30.7	2.51	39.0	2.47	2.05
A9601010.ACM	10	5.65	31.2	2.55	40.0	2.52	2.10
A9601015.ACM	15	5.84	31.4	2.67	39.3	2.78	2.11
A9601015.ACM	15	5.76	31.0	2.65	39.7	2.78	1.94
A9601015.ACM	15	5.74	30.8	2.69	40.5	2.79	1.95
A9601016.ACM	16	5.71	30.2	2.56	38.8	2.62	1.94
A9601016.ACM	16	5.87	31.2	2.60	39.9	2.71	2.03
A9601016.ACM	16	5.66	29.9	2.58	39.3	2.58	1.89
A9601016.ACM	16	5.79	30.7	2.65	40.9	2.67	2.00
A9601017.ACM	17	5.57	31.4	2.51	38.1	2.69	1.97
A9601017.ACM	17	5.55	31.3	2.49	37.6	2.67	1.95
A9601019.ACM	19	5.57	29.5	2.33	38.9	2.61	1.91
A9601019.ACM	19	5.71	30.4	2.32	38.6	2.66	1.97
A9601021.ACM	21	5.63	30.4	2.51	38.8	2.56	1.89
A9601021.ACM	21	5.59	30.1	2.50	38.6	2.56	1.89
A9601022.ACM	22	5.71	30.4	2.44	39.1	2.57	1.90
A9601022.ACM	22	5.68	30.2	2.43	38.8	2.54	1.88
A9601023.ACM	23	5.40	30.2	2.52	38.4	2.64	1.95
A9601023.ACM	23	5.34	29.8	2.53	38.6	2.62	1.93
A9601051.ACM	51	5.66	30.0	2.71	39.2	2.67	2.00
A9601051.ACM	51	5.66	30.0	2.71	39.2	2.66	1.99
A9601051.ACM	51	5.65	30.0	2.66	39.9	2.49	1.98
A9601051.ACM	51	5.62	29.8	2.66	40.0	2.49	1.97
A9601052.ACM	52	5.67	30.5	2.66	39.9	2.80	2.01
A9601052.ACM	52	5.72	30.8	2.66	40.0	2.82	2.03
A9601053.ACM	53	5.68	30.4	2.58	38.9	2.75	2.01
A9601053.ACM	53	5.68	30.4	2.60	39.2	2.74	1.99
A9601053.ACM	53	5.70	30.4	2.62	39.5	2.74	1.97
A JOUI UJJ. A CIVI	23	5.70	130.3	4.02	■ J7.J	14.70	1.7/

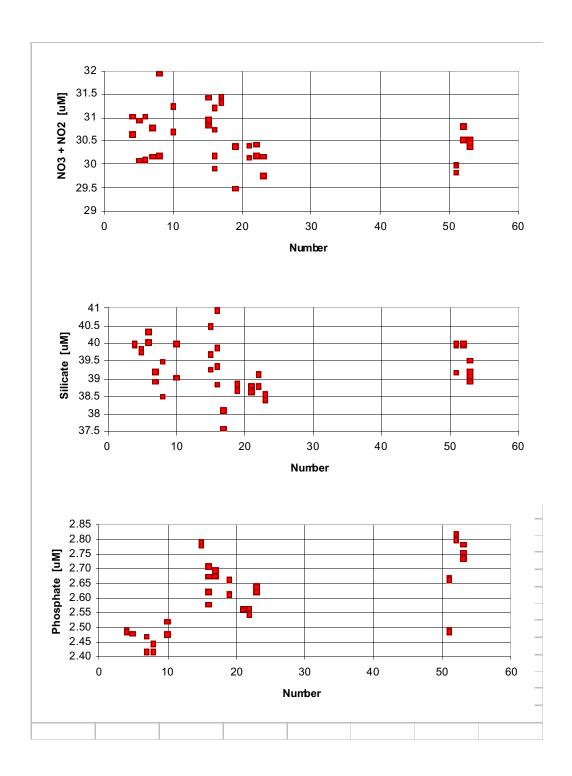


Figure A3.1.2: Nutrient samples run as quality checks.

Calibration of SN 62 549								
	unto on otal a	1:-1-0.002.0	004 nou					
.01 = 1-2 co	unts on stat	11al=0.002-0. □	004 psu		_			
	01.1		0.1	LADOO			A.I	
Date	Std	Lab	Sal	IAPSO	No		Nom	Location
		temp	temp	batch	Sa		Sal	
40.4 00	4 40	40		D400	1R		2R	00100
13-Aug-96	4.49	19		P126		0.99987	1.99974	
24-Aug-96		18	21	P126		0.99987	1.99974	
25-Aug-96				P128		0.99986	1.99972	
29-Aug-96				P128		0.99986	1.99972	
1-Sep-96				P128		0.99986	1.99972	
2-Sep-96				P128		0.99986	1.99972	
3-Sep-96				P128		0.99986	1.99972	
4-Sep-96				P128		0.99986	1.99972	
7-Sep-96		20.1		P128		0.99986	1.99972	
9-Sep-96				P128		0.99986	1.99972	
9-Sep-96		20.1		P130		0.99997	1.99994	
10-Sep-96		20.1		P130		0.99997	1.99994	
11-Sep-96				P130		0.99997	1.99994	
12-Sep-96				P130		0.99997	1.99994	
13-Sep-96				P130		0.99997	1.99994	
14-Sep-96		20.1		P130		0.99997	1.99994	
15-Sep-96				P130		0.99997	1.99994	
17-Sep-96				P130		0.99997	1.99994	
18-Sep-96				P130		0.99997	1.99994	
20-Sep-96				P130		0.99997	1.99994	
21-Sep-96	4.525	20.1	21	P130		0.99997	1.99994	
4.65					•••			
4.55			,	•		'		
	20100		-		-			
4.5	SIRU							
4.45		■ A9	601		ı			
4.4								
35290	35295	35300 35	353° 353°	10 353	315 3	5320	35325 353	330 —

Figure A3.1.3: Salinometer standardisation values.

			s on A9601.											
Salstan	dardise	d wifhon∈	estd, and the	ot her one	then measure	ed.								
heet	St d	St d	Measured	St dse	Measured value		Nominal value			Dff (meas-nom)		Diff, abs		
	num.			value	R	2R	Т	R	2R	psu	2R	psu	psu	
16	4	P128	P130	4.44	0.99993	1.99985	21	0.99997	1.9999	34999	-0.00009	-34.9988	34.9988	
16	5	P128	P130	4.44	0.99993	1.99985	21	0.99997	1.9999	34999	-0.00009	-34.9988	34.9988	
21	3	P128	p130	4.44	0.99993	1.99985	21	0.99997	1.9999	34999	-0.00009	-34.9988	34.9988	
22	3	P128	p130	4.52	0.99993	1.99986	21	0.99997	1.9999	34.999	-0.00008	-34.9988	34.9988	
25	3	P130	p128	4.61	0.99990	1.99979	21	0.99986	1.9997		0.00007	-34.9945	34.9945	
	4	p130	p128	4.61	0.99992	1.99983	21	0.99986	1.9997	34.994	0.00011	-34.9945	34.9945	
29	3	p130	p128	4.61		1.99983			1.9997	34.994	0.00011	-34.9945	34.9945	
29	4	p130	p128	4.61	0.99991	1.99982	21	0.99986	1.9997	34994	0.00010	-34.9945	34.9945	
												av	34.9967	DSII
128 is	0.0018	8 +/- Q.C	0003 psu high	erthan P	1 30							st dev	0.0023	
5 10	5. 50 1		J J J J J J J J J J J J J J J J J J J									%rsd		%

Table A3.1.3: Comparison of ISS batches P128 and P130.

## Part 4

# Aurora Australis Southern Ocean Oceanographic Cruises, 1991 to 1996 - Inter-cruise Comparisons and Data Quality Notes

#### 4.1 INTRODUCTION

Marine science cruise AU9601 aboard the RSV Aurora Australis was the seventh and last in a series of oceanographic cruises from 1991 to 1996, taking CTD measurements along Southern Ocean transects, mostly under the WOCE program (Table 4.1). In this part of the report, brief data comparisons are made between the cruises, and data quality notes relevant to the cruise set are discussed.

<u>Table 4.1:</u> RSV Aurora Australis Southern Ocean oceanographic cruises, 1991 to 1996. Note the following: PET=Princess Elizabeth Trough section, FORMEX=Formation Experiment, MARGINEX=Antarctic Margin Experiment; au9309 and au9391 were part of the same cruise; the southern end of SR3 was occupied as part of MARGINEX.

cruise	transect	occupation date di	irection of occupation
au9101	SR3 (WOCE)	October 1991 2	2/3 north to south, 1/3 south to north north to south  west to east then north to south north to south south to north  by west to east south to north  south to north
au9309	SR3 (WOCE)	March 1993	
au9391	P11 (WOCE)	April 1993	
au9407	SR3 (WOCE)	January 1994	
au9407	PET	January 1994	
au9404	S4 (WOCE)	Dec. 1994 - Jan. 199	
au9404	SR3 (WOCE)	January-February 19	
au9501	SR3 (WOCE)	July-August 1995	
au9501	FORMEX	August 1995	
au9604	MARGINEX	January-March 1996	
au9601	SR3 (WOCE)	August-September 1	
auguu I	SK3 (WOCE)	August-September is	330 SOULIT LO HOLLIT

#### 4.2 INTER-CRUISE DATA COMPARISONS

In this section, a brief comparison of salinity, dissolved oxygen and nutrient data is made between the seven cruises. Most of the discussion refers to data from the SR3 section. The primary aim of the comparison is to assess the inter-cruise compatibility of measurements and data quality for the entire data set. Comparisons with earlier data sets are discussed in Rosenberg et al. (1995a).

## 4.2.1 Salinity

#### Inter-cruise comparisons

Inter-cruise salinity comparisons in earlier data reports (Rosenberg et al., 1995a, 1995b and 1996) revealed significant variation in salinity measurements for the different cruises. The YeoKal salinometers used (Table 4.2) were identified as the most likely source of error. For cruise AU9601, the last cruise in the series, a Guildline salinometer was used for the first time, with a manufacturer-quoted salinity accuracy of 0.001 (PSS78) as compared to 0.003 (PSS78) for the YeoKal instruments. As a result, high quality CTD salinity data were obtained for this cruise (see Part 3 of this report). To assess inter-cruise errors in salinity measurements, salinity data from each cruise are compared to data from AU9601. Specifically, the meridional variation of the salinity maximum (i.e. for Lower Circumpolar Deep Water as defined by Gordon, 1967) along the SR3 section for each cruise is compared to the equivalent values for AU9601 (Figures 4.1a and b). For the comparison, 2 dbaraveraged CTD data are used i.e. CTD salinity at the nearest 2 dbar bin to the salinity maximum for

each station. Note that in the Figure 4.1 comparison of cruises au9601 and au9101, au9601 data are linearly interpolated to the au9101 station positions. For the other cruises in the figure, salinity differences are only formed between station pairs which are separated by less than 1.5 nautical miles of latitude.

<u>Table 4.2:</u> Summary of International Standard Seawater (ISS) batches and salinometers used for salinity sample analyses on cruises, including RV Melville cruise me9706.

au9101 au9309 au9391 au9407 au9407 au9404 au9501 au9604	P115 (6th Feb. 1991) P121 (8th Sept. 1992) P121 (8th Sept. 1992) P123 (10th June 1993) P121 (8th Sept. 1992) P123 (10th June 1993) P121 (8th Sept. 1992) P123 (10th June 1993) P121 (8th Sept. 1992) P126 (29th Nov. 1994) P128 (18th July 1995)	station numbers 1-35 1-63 1-64 1-79 80-102 1-85 86-107 1-208 1-25, 69-74, 110-145
au9604	P126 (29th Nov. 1994)	26-68, 75-109
au9601 au9601	P128 (18th July 1995) P130 (21st March 1996)	1-23 24-69
me9706	P130 (21st March 1996)	2-49
11103700	1 100 (213t Walter 1000)	2 43
cruise	salinometer serial number	station numbers
au9101	601003 (YeoKal)	1-35
au9309	601003 (YeoKal)	1-63
au9391	601003 (YeoKal)	1-64
au9407	601855 (YeoKal)	1-86
0110407		1 00
au9407	601003 (YeoKal)	87-102
au9404	601855 (YeoKal)	87-102 1-107
	601855 (YeoKal) 601830 (YeoKal)	87-102 1-107 1-208
au9404 au9501 au9604	601855 (YeoKal) 601830 (YeoKal) 601003 (YeoKal)	87-102 1-107 1-208 1-23, 43-47, 139-141
au9404 au9501 au9604 au9604	601855 (YeoKal) 601830 (YeoKal) 601003 (YeoKal) 601439 (YeoKal)	87-102 1-107 1-208 1-23, 43-47, 139-141 24-25
au9404 au9501 au9604 au9604 au9604	601855 (YeoKal) 601830 (YeoKal) 601003 (YeoKal) 601439 (YeoKal) 601855 (YeoKal)	87-102 1-107 1-208 1-23, 43-47, 139-141 24-25 26-42, 48-68, 142-145
au9404 au9501 au9604 au9604 au9604	601855 (YeoKal) 601830 (YeoKal) 601003 (YeoKal) 601439 (YeoKal) 601855 (YeoKal) 601440 (YeoKal)	87-102 1-107 1-208 1-23, 43-47, 139-141 24-25 26-42, 48-68, 142-145 69-138
au9404 au9501 au9604 au9604 au9604 au9604 au9601	601855 (YeoKal) 601830 (YeoKal) 601003 (YeoKal) 601439 (YeoKal) 601855 (YeoKal) 601440 (YeoKal) 62549 (Guildline)	87-102 1-107 1-208 1-23, 43-47, 139-141 24-25 26-42, 48-68, 142-145 69-138 1-69
au9404 au9501 au9604 au9604 au9604	601855 (YeoKal) 601830 (YeoKal) 601003 (YeoKal) 601439 (YeoKal) 601855 (YeoKal) 601440 (YeoKal)	87-102 1-107 1-208 1-23, 43-47, 139-141 24-25 26-42, 48-68, 142-145 69-138

The following approximate mean salinity differences for data along the SR3 transect at the deep salinity maximum are evident from Figures 4.1 and 4.2:

cruise comparison	approximate mean salinity difference (PSS78)
au9601-au9101	-0.005 (south of ~49.5°S)
au9601-au9309	-0.008
au9601-au9407	-0.001
au9601-au9404	-0.004
au9601-au9501	0.001
au9601-au9604	insufficient data for comparison
au9601-me9706	-0.002

These values summarise the inter-cruise compatibility of salinity data. No significant correlation is evident between ISS batch numbers used and the observed salinity differences between cruises, and the salinometers remain the most likely source of error. A further partial occupation of the SR3 transect down to 57°S was made by the RV Melville in March to April 1997 (cruise me9706, principal investigators R.Watts, S. Rintoul, J. Richman, B. Petit, D. Luther, J. Filloux, J. Church, A. Chave). Guildline salinometers were used for salinity analyses (Table 4.2), with the hope of determining whether inter-cruise compatibility improves using these more stable salinometers. Comparing the

meridional variation of the deep water salinity maximum for cruises au9601 and me9706 (Figure 4.2), a mean difference au9601-me9706 of ~-0.002 is clearly observed. This difference is less variable than for other cruises (Figure 4.1), due to stable performance of the Guildlines. Nevertherless this difference is clearly significant, and indicates that 0.002 (PSS78) is at the limit of achievable salinity accuracy when comparing different cruises.

## Small scale variance of salinity signal

Close examination of vertical CTD profiles reveals a small scale structuring, at vertical scales of the order 2 dbar, which is not consistent between different cruises. To assess whether this variability is a real oceanic feature, salinity and temperature vertical profile data variance was investigated for all cruises, as follows. Vertical salinity and temperature 2 dbar-averaged profiles were smoothed by calculating a running mean of width 12 dbar (i.e. ±3 pressure bins), centered on each pressure bin. A mean "variance" V around the smoothed profiles was then calculated for each vertical salinity profile (and similarly for temperature):

$$V_s = \left[ \sum_{i=1001}^{\text{bottom}} (|s_{\text{smooth}} - s|)_i \right] / n$$
 (eqn 4.1)

for  $s_{smooth}$  the smoothed salinity, the ith 2 dbar pressure bin, and n equal to the number of 2 dbar pressure bins from 2002 dbar to the bottom of the profile. Note that only data below 2000 dbar were examined, to avoid steep vertical gradients and regions of high mixing. To allow a realistic comparison between different cruises, equivalent station positions along the SR3 transect were investigated. Variances were calculated for stations lying within the two latitude ranges 45 to 50°S and 54 to 58°S - choice of these two latitude ranges excludes stations lying within the major frontal regions where greater inter-cruise variability might occur. (Note that cruise au9391 is an exception, as it lies along the P11 transect - for this cruise, significant horizontal frontal structure was observed in the 54 to 58°S latitude range, and the results are not directly comparable to SR3 data.) The results in Table 4.3 show values of  $V_s$  and  $V_t$  (for salinity and temperature respectively) averaged over the specified station groups for each cruise.

<u>Table 4.3:</u> Vertical variance of CTD salinity and temperature data below 2000 dbar, for given latitude ranges along the SR3 transect (with the exception of cruise au9391, along the P11 transect). For the CTD's, "B" and "C" indicate a MarkIIIB and MarkIIIC respectively. "c-cell" is the condition of the CTD conductivity cell.

		latitude 45°S		latitude 54°S to 58°S					
cruise	stn	CTD c-cell	mean V <sub>s</sub>	mean V <sub>t</sub>	stn	CTD	c-cell	mean V <sub>s</sub>	mean V <sub>t</sub>
	nos.	no.	(PSS78)	(°C)	nos.	no.		(PSS78)	(°C)
0000	0.45	44070	0.00004	0.00000	05.00	4407D		0.00004	0.00000
au9309	6-15	1197B used	0.00031	0.00089	25-33	1197B	used	0.00031	0.00082
au9391	19-28	1073B used	0.00022	0.00065	<i>37-44</i>	1073B	used	0.00024	0.00079
au9407	7-22	2568C used	0.00026	0.00086	34-45	2568C	used	0.00025	0.00072
au9404	92-102	1193C suspect	0.00025	0.00087	74-80	1193C	suspect	0.00038	0.00076
au9501	6-17	1103C new	0.00047	0.00078	30-37	1193C	suspect	0.00023	0.00070
au9601	46,54-64	1103C new	0.00045	0.00083	25-33	1103C	new	0.00041	0.00071
me9706	3-4,6-7,								
	40-43	1013B new	0.00024	0.00087	19-26	1013B	new	0.00028	0.00078

 $V_s$  values are unlikely to be affected by pressure noise. Firstly, if any noise is present in the raw pressure signal, this would be averaged out in the 2 dbar binning. Moreover for CTD 1103, where the highest  $V_s$  values occur, the pressure signal is significantly less noisy than for other instruments. Secondly, for casts taken in either calm conditions or in the ice, and where pressure reversals are therefore minimal, no drop in  $V_s$  values are evident.

 $V_t$  values within each latitude range are fairly consistent between cruises compared with  $V_s$  values, which show much more variation. In particular,  $V_t$  values are consistently lower in the 54-58°S region than in the 45-50°S region - this suggests that the fine structure is a real measurement, not an electronic artifact of the instrumentation.

The magnitude of V<sub>s</sub> appears to be dependent on:

- \* the magnitude of V,;
- \* the condition of the conductivity cell;
- \* the particular instrument in use.

Firstly, inspection of individual stations reveals that when  $V_s$  exceeds a certain threshold level, there is a strong dependence of  $V_s$  on the magnitude of  $V_t$  (Figure 4.3). Below this value, there is no significant dependence. This however does not account for the high inter-cruise variation of  $V_s$  evident in Table 4.3. The results for cruise au9501 (Figure 4.4) demonstrate a dependence of  $V_s$  on the condition of the conductivity cell:  $V_s$  is significantly higher for the 45-50°S latitude range where a new cell is in use, compared to the southern stations where a suspect cell was used. In addition, comparing the 54-58°S values for cruises au9501 and au9601,  $V_t$  values are comparable, whereas  $V_s$  is much lower for the suspect conductivity cell. In fact from Figure 4.3, there is a different dependency of  $V_s$  on  $V_t$  for the suspect conductivity cell. Lastly, there also appears to be a dependence of  $V_s$  on the instrument in use. The most striking difference is between  $V_s$  values for cruises me9706 and au9601, even though new conductivity cells were used in both cases (and note that  $V_t$  values for the two cruises are comparable). Apparently some instruments are more reponsive than others - this may be related to differences between MarkIIIB and MarkIIIC CTD's, or simply differences between individual instruments.

To summarise, new conductivity cells appear to be more responsive to fine structure in the water column, however the quantitative value of small scale vertical salinity variations may also depend on the CTD in use. In more extreme cases, this fine structure includes small vertical density inversions, with typical magnitudes in the range 0.001 to 0.005 kg.m<sup>-3</sup>.

## 4.2.2 Dissolved oxygen

Dissolved oxygen bottle data along the SR3 transect for cruises au9407 and onwards are compared in Figures 4.5a and b. For all these cruises, oxygen bottle samples were analysed using the automated titration system developed by Woods Hole Oceanographic Institution (Knapp et al., 1990). Data from the earlier cruises au9101, au9309 and au9391, where samples were analysed using a manual titration method (Eriksen and Terhell, in prep.), are discussed in previous data reports (Rosenberg et al., 1995a and b). Note that in Figure 4.5, axes limits do not include the entire data set, focussing rather on deep and intermediate water masses to allow easier visual comparison between cruises. Also note that for cruise au9604, data from the longitude range 128 to 150°E are plotted to provide more points for comparison.

In summary, the following dissolved oxygen data appear to be consistent:

au9407 au9404 au9501 stations 22 and onwards au9604 au9601 stations 41 and onwards

The following inconsistencies are apparent:

```
au9501 stations 1-21: values smaller by ~6μmol/l au9601 stations 1-40: values larger by ~4μmol/l
```

Note that the above deviation values are approximate averages only - deviations for individual samples may vary slightly with the magnitude of dissolved oxygen concentration. Examination of standardisation values for the laboratory analyses reveals the source of error: for cruise au9501, a drift in standardisation values was noted up until station 21, however restandardisations were not carried out; for cruise au9601, a jump in standardisation values occurred after station 40 (see Appendix 3.1). Clearly, standardisation values for dissolved oxygen analyses must be examined more closely during future cruises.

## Phosphate and nitrate+nitrite

Phosphate and nitrate+nitrite data for cruises au9404 and onwards are compared in Figure 4.6 while data for all cruises are summarised in Figure 4.7. Note that the inconsistent results for cruise au9101 (Figure 4.7), due to higher phosphate values, are discussed in Rosenberg et al. (1995a).

The nitrate+nitrite to phosphate ratio is mostly consistent for cruises au9309 and au9407 (Figure 4.7), and for cruises au9404, au9501 and au9604 (Figures 4.6a and b); however the ratio differs for cruise au9601 (Figure 4.6c). Comparison of vertical nutrient profiles at equivalent station positions for different cruises reveals that the difference is due to phosphate, rather than nitrate+nitrite data. Phosphate values for au9601 are lower than the values for other cruises by ~0.1µmol/l. As discussed in Appendix 3.1 of this report, the phosphate carryover effect is believed to have been minimised for cruise au9601 by alterations to the analysis techniques. For au9601, the autoanalyser peaks for phosphate analyses very nearly return to the baseline level from where peak integration occurs, minimising any carryover error. For previous cruises, autoanalyser peaks for phosphate analyses do not return all the way to the baseline level. This carryover error artificially increases peak height values, and could be a cause for slightly higher phosphates for previous cruises compared to au9601. Note that the offset is unlikely to be a constant - there may be a dependence on phosphate concentration, and on instrument settings. Phosphate measurements on future cruises using the same techniques as for cruise au9601 will confirm whether the observed difference of ~0.1µmol/l in Figure 4.6c does indeed represent an error in all the previous cruises.

## Near surface phosphate and nitrate+nitrite

From Figure 4.6b, the near surface nutrient data for au9604 clearly differs from the remaining data. Moreover, the lower the near surface nutrient value, the greater the deviation from the bestfit line. From inspection of all the cruises (Figure 4.7), this feature is apparent for data collected in Antarctic waters (i.e. south of the Polar Front) during the austral summer i.e. cruises au9407, au9404 and au9604. In addition, the feature can be seen in summer data collected by the Eltanin (Gordon et al., 1982) (Figure 4.7) along a meridional transect at 132°E. There are two possible explanations for the feature:

- (a) the phosphate carryover error, discussed in previous data reports (see section 6.2.1 in Rosenberg et al., 1995b), results in depressed phosphate values near the surface; this error is amplified where vertical phosphate gradients are steep, as is the case for near surface Antarctic waters during an austral summer;
- (b) alternatively, the feature is real, indicating a stronger depletion of phosphate relative to nitrate+nitrite by biological activity in Antarctic waters during the summer.

Note that for cruises au9407 and au9404, many surface phosphate samples were bad due to the phosphate carryover effect, and much of the relevant nitrate+nitrite to phosphate ratio data are missing for these cruises. Whether explanation a or b applies is inconclusive. As already discussed, the phosphate carryover error is believed to have been minimised for cruise au9601. Thus to confirm whether the near surface phosphate depletion is an error or a real feature, more summertime Antarctic zone nutrient data are needed using the analysis techniques of cruise au9601.

#### Matrix correction

For analysis of nutrients, samples are initially run against nutrient standards (see Appendix 3, Rosenberg et al., 1995b). The colour reagent is then removed, and samples are run again against the nutrient standards. The peak observed when run without the colour reagent is due mainly to a "matrix effect" (i.e. a detector response due to refractive properties of the sample water), and should be corrected for. The size of the matrix effect is dependent on chemistry and detection wavelength. Ideally, the magnitude of the effect should be checked for each nutrient sample. For cruise au9601,

the effect was negligible for nitrate+nitrite and silicate analyses, however a significant effect was observed for phosphates. A mean magnitude of the matrix effect for phosphates was obtained by measuring the effect for two vertical phosphate profiles, from the north and south ends of the transect. The value, equal to  $0.088~\mu mol/l$ , should be subtracted from au9601 phosphate if the matrix effect correction is desired. Note that the matrix effect was not investigated for previous cruises, so to maintain consistency of the entire data set, the correction has not been applied to cruise au9601.

#### Silicate

Silicate data along the SR3 transect for cruises au9309 and onwards are compared in Figure 4.8. Note that most of the comparisons are for stations outside the strong frontal regions. Most of the silicate data for the different cruises agree to within 5  $\mu$ mol/l, and in general no consistent offset between cruises is evident.

#### 4.2.4 Pressure

Small differences in the quality of CTD pressure data between different cruises occurs according to the CTD instrument in use. The two fundamental differences in instruments are as follows:

- (i) MarkIIIB CTD's employ a stainless steel type strain gauge for measuring pressure; there is no pressure temperature correction, and separate downcast and upcast laboratory calibrations are used to compensate for hysteresis of the pressure response. The more accurate WOCE upgraded MarkIIIC CTD's use a titanium type strain gauge, and include a pressure temperature correction the hysteresis of these sensors is small compared with the stainless steel type, and a downcast laboratory calibration only is applied to all pressure data. The manufacturer quoted accuracies of pressure data from the two types of pressure sensor are ±6.5 dbar for the Mark IIIB units (used for cruises au9101, au9309 and au9391), and ±1.2 dbar for the Mark IIIC's (used for all remaining cruises).
- (ii) The level of noise in the raw pressure signal differs for the different instruments. In general, the titanium type sensors in the MarkIIIC's display a higher noise level than the stainless steel type in the MarkIIIB's (Millard et al., 1993), and a small error may be introduced into surface pressure offset values, as described in previous data reports. Of the MarkIIIC's used, CTD 1193 was noisiest and CTD 2568 a little less so; both however were significantly noisier than CTD 1103. This pressure signal noise, up to 1 dbar in amplitude for CTD 1193, can result on occasion in 2 dbar pressure bins (for the pressure monotonically increasing data files) with too few raw data points for the formation of a 2 dbar average (see CTD methodology in Rosenberg et al. 1995b for pressure calculations). For details on individual cruises, and information on which instruments were used, see the data reports for each cruise.

## 4.2.5 Temperature

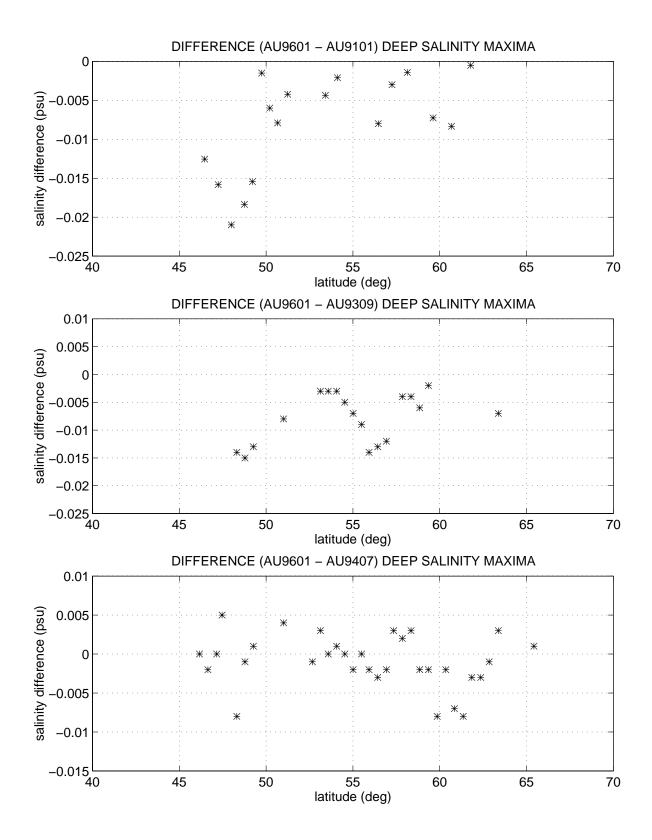
Comparison of calibrated CTD platinum temperature data  $T_{cal}$  to mercury reversing thermometer measurements  $T_{therm}$  on all the cruises allows the inter-cruise compatibility of temperatures to be assessed. Note that the same laboratory calibrations were applied to the reversing thermometers for all cruises, although a different set of thermometers was used for cruises au9309/au9391. Reversing thermometer calibrations are assumed to remain stable over the entire period. Moreover, the thermometer to CTD comparison for different cruises shows the same variation for the different thermometers used, supporting the assumption of stable thermometer calibrations. Thus any temperature errors are attributed to calibration problems for the CTD platinum temperature. For cruise au9101, insufficient thermometer measurements were made for a check of CTD temperature.

Although manufacturer quoted accuracies for the reversing thermometers are only of the order 0.01°C, thermometer resolution is usually significantly better; and given the reasonably large number of data points obtained, it is estimated that CTD temperature performance can be assessed to an accuracy of  $\sim 0.003$ °C. Mean differences ( $T_{\text{therm}}$  -  $T_{\text{cal}}$ ) are summarised in Table 4.4. The following CTD temperature calibration problems are evident:

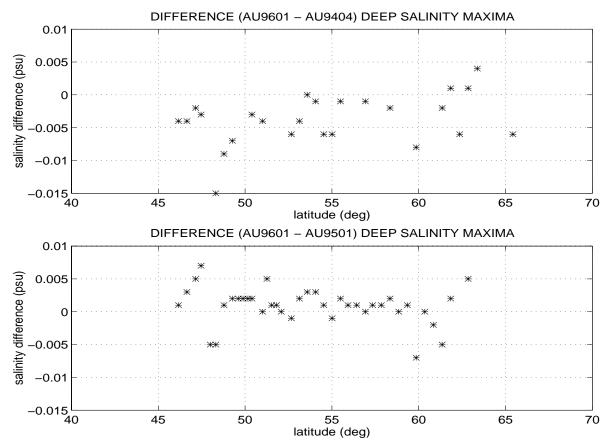
- (i) For the first half of cruise au9309, the CTD temperature is incompatible with other cruises by >0.01°C.
- (ii) For cruise au9501 where CTD 1103 was used, there is a CTD temperature calibration error of ~0.007°C (the post cruise CTD temperature calibration was used). Pre and post cruise temperature calibrations were significantly different, and a temperature error occurs when either calibration is applied (see au9501 data report).
- (iii) For cruise au9601, the difference value of ~0.005°C is large enough to be significant. In this case, a pre cruise calibration was used.
- (iv) For cruise au9407, the temperature calibration is good, except for an apparent non-linearity at lower temperatures (stations 61-82). See Rosenberg et al. (1995b) for more details.
- (v) For cruise au9404, a CTD temperature calibration error was apparent for CTD 1193 (stations 19-106). A constant correction of -0.007°C was applied to all CTD temperature data. Some error may however remain due to this assumption of a constant offset.

<u>Table 4.4:</u> Mean and standard deviation of temperature residual ( $T_{therm}$  -  $T_{cal}$ ) for different cruises.

cruise (station nos.)	CTD no.	mean of (T <sub>therm</sub> - T <sub>cal</sub> ) (deg. C)	standard dev. of $(T_{therm} - T_{cal})$ (deg. C)	no. of samples
au9309 (1-35)	1197	-0.0139	0.0110	51
au9309 (36-63)/au9391 (1-63)	1073	-0.0022	0.0109	121
au9407 (1-60 and 83-102 only)	2568	0.0014	0.0131	95
au9404 (1-106)	1193/1103	0.0017	0.0090	243
au9501 (1-29,46-103,106-208)	1103	-0.0071	0.0078	155
au9501 (30-45)	1193	0.0011	0.0041	33
au9604 (1-147)	1103/1193	0.0019	0.0068	289
au9601 (1-71)	1103/1193	0.0046	0.0050	187



<u>Figure 4.1a:</u> Variation south along the SR3 transect of the deep salinity maximum: salinity differences between cruise au9601 and cruises au9101, au9309 and au9407. For au9101 comparison, au9601 values are linear interpolations between station positions; for cruises au9309 and au9407 comparisons, differences are only formed between station pairs separated by no more than 1.5 nautical miles of latitude.



<u>Figure 4.1b:</u> Variation south along the SR3 transect of the deep salinity maximum: salinity differences between cruise au9601 and cruises au9404, au9501. Differences are only formed between station pairs separated by no more than 1.5 nautical miles of latitude.

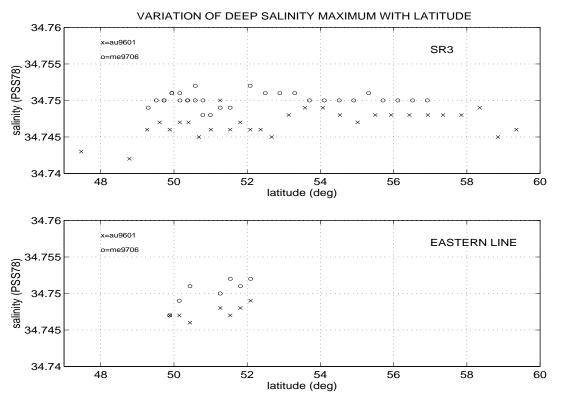


Figure 4.2: Variation south along the SR3 transect of the deep salinity maximum for cruises au9601 (Aurora Australis) and me9706 (Melville), both using Guildline salinometers.

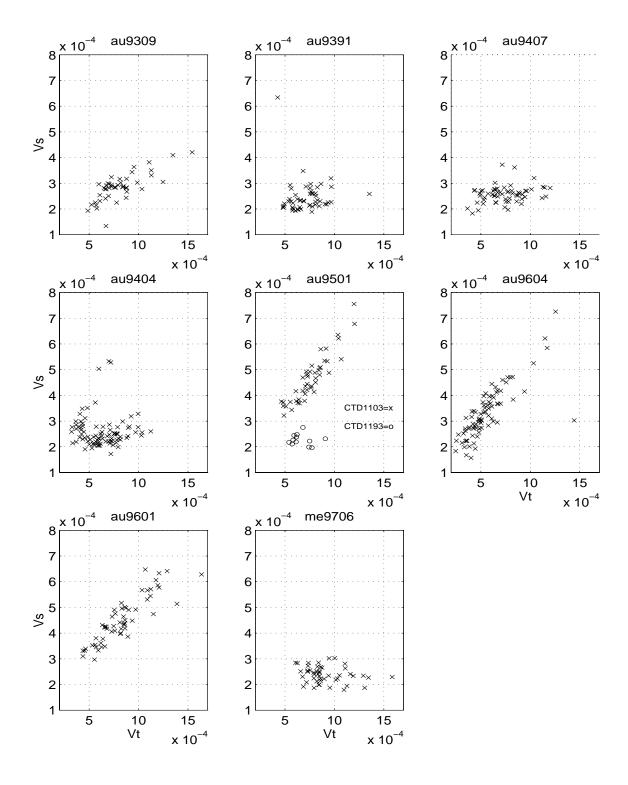
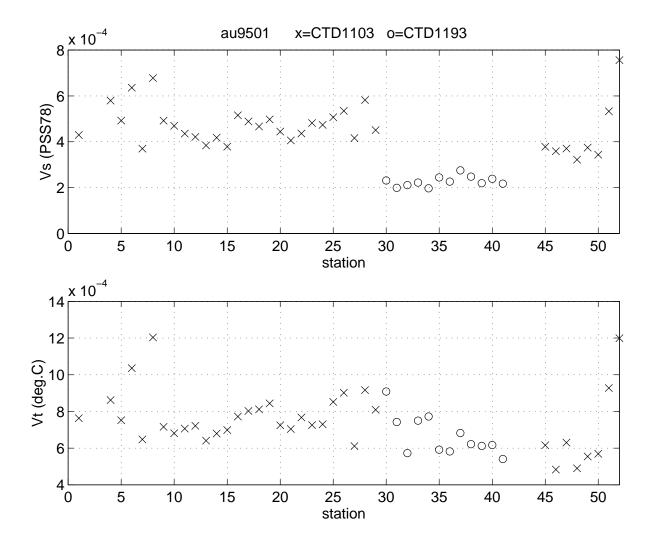
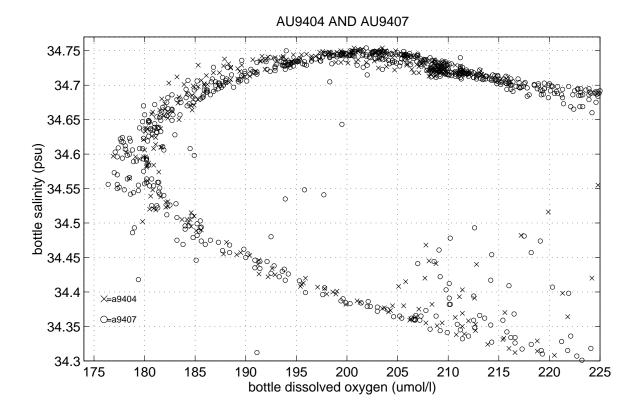
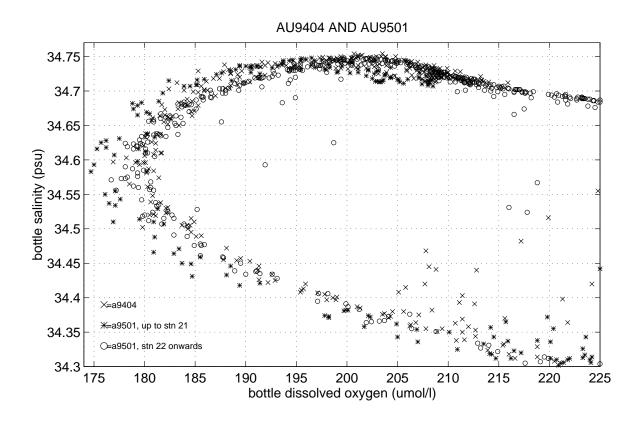


Figure 4.3:  $V_s$  versus  $V_t$  for all cruises along all transects. Note that all stations are plotted, except for a small number with large  $V_t$  values.

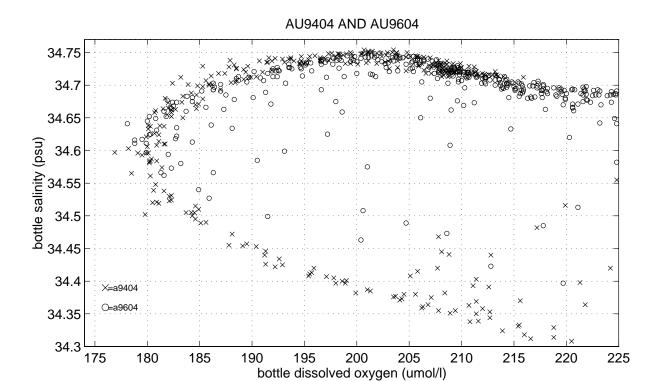


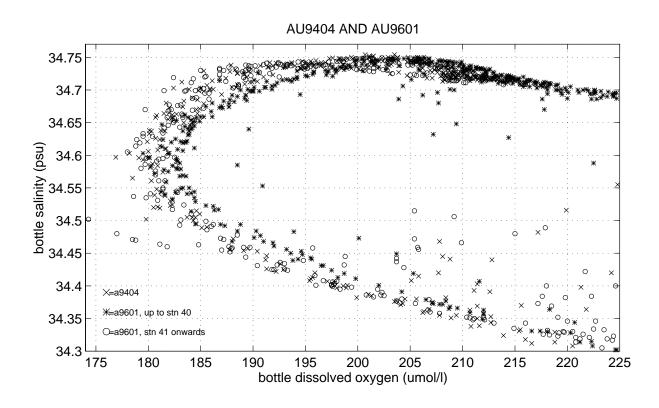
<u>Figure 4.4:</u> Variation of  $V_{\rm s}$  and  $V_{\rm t}$  for individual stations for cruise au9501, along the SR3 transect.



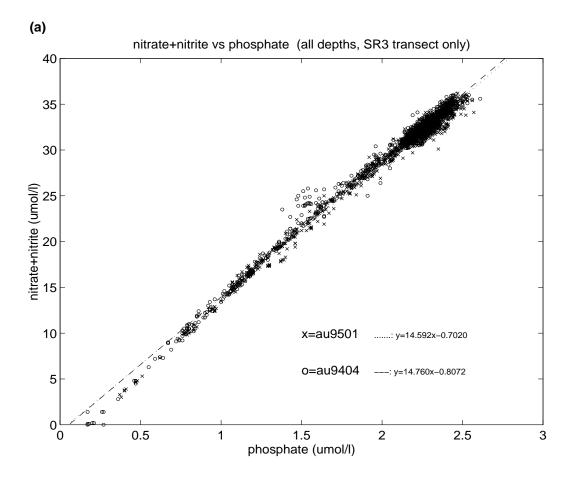


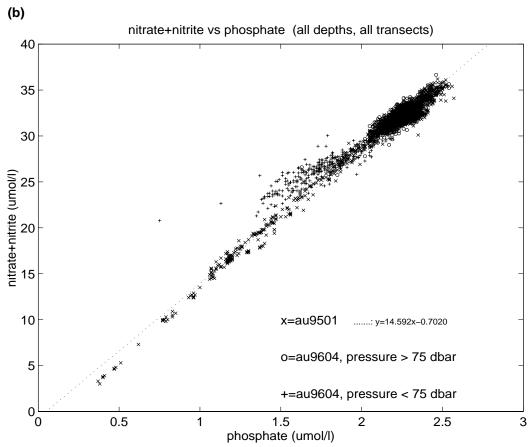
<u>Figure 4.5a:</u> Dissolved oxygen bottle data comparison for cruises au9404, au9407 and au9501, SR3 data only. Note that scale is expanded i.e. not all data are on the plot.





<u>Figure 4.5b:</u> Dissolved oxygen bottle data comparison for cruises au9404, au9604 and au9601, SR3 data only (except for au9604, where data from the longitude range 128 to 150  $^{\circ}$ E are plotted). Note that scale is expanded i.e. not all data are on the plot.





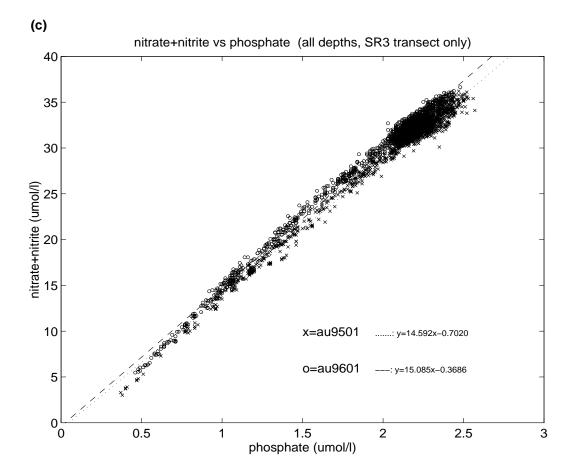
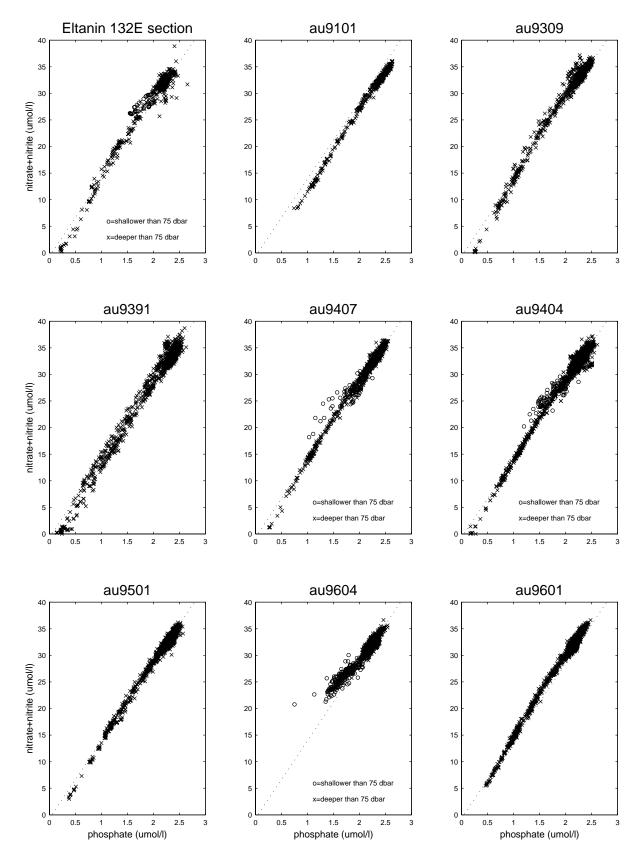
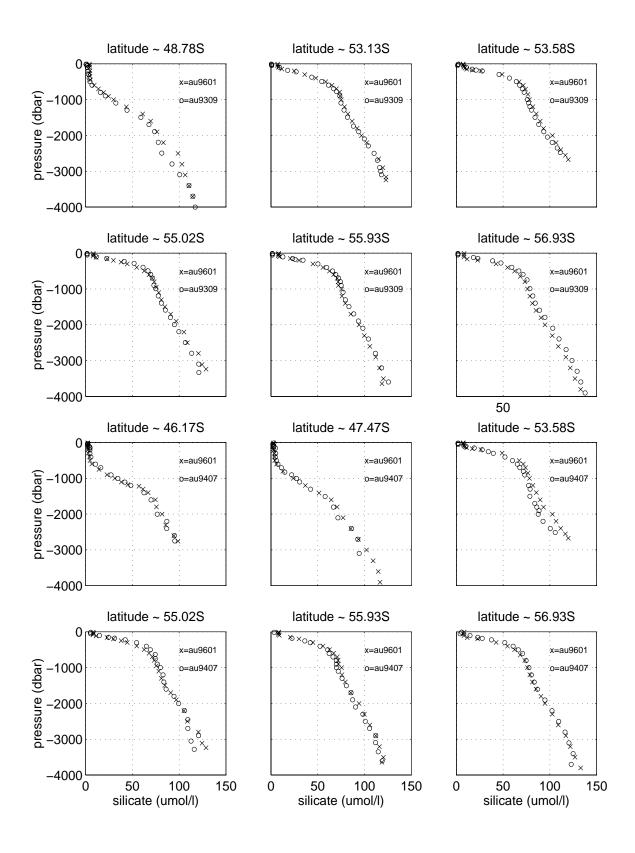


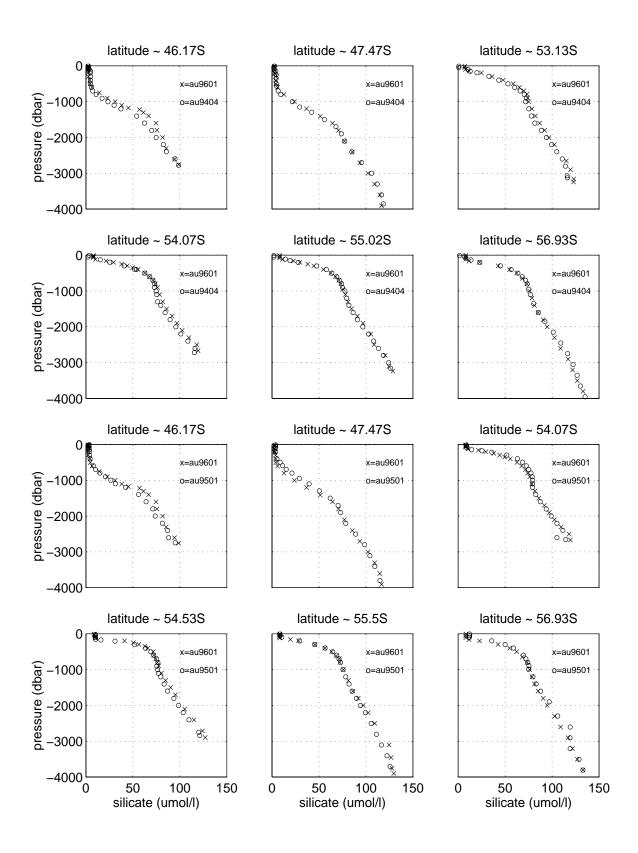
Figure 4.6 (previous page and this page): Bulk plot of nitrate+nitrite versus phosphate for: (a) all au9501 and au9404 data along the SR3 transect, together with linear best fit lines; (b) all au9501 and au9604 data along all transects, with linear best fit line for au9501; (c) all au9501 and au9601 data along the SR3 transect, together with linear best fit lines.



<u>Figure 4.7:</u> Nitrate+nitrite versus phosphate for Aurora Australis oceanographic cruises, plus Eltanin data from Gordon et al. (1982). The linear best fit line for cruise au9501 is included on each plot.



<u>Figure 4.8a:</u> Comparison of vertical silicate concentration profiles between cruises au9601 and au9309, and cruises au9601 and au9407, for selected stations along the SR3 transect. Note that data below 4000 dbar are not included in the plots.



<u>Figure 4.8b:</u> Comparison of vertical silicate concentration profiles between cruises au9601 and au9404, and cruises au9601 and au9501, for selected stations along the SR3 transect. Note that data below 4000 dbar are not included in the plots.

# Part 5 Data File Types and Formats

## 5.1 UNDERWAY MEASUREMENTS

The underway measurements for the cruise, as logged automatically by the ship's data logging system, and quality controlled by human operator (Ryan, 1995), are contained in column formatted ascii files. The two file types contain 10 sec digitised data, and 15 min averaged data. In both cases, missing data or data flagged as bad are replaced by the null value -999. The files are padded out to commence on the first digitising interval of the first day in the file, and ending at the last digitising interval on the last day in the file.

#### 5.1.1 10 second digitised underway measurement data

Data at the minimum digitised interval of 10 sec. are contained in files named \*.alf (Table 5.1), where the data filename prefix corresponds to the cruise acronym. A two line header is followed by the data as follows:

#### column parameter 1 decimal time (0.0=midnight on December 31st, therefore, for example, 1.5=midday on January 2nd) 2 day 3 month 4 year 5 hour 6 minute 7 second 8 latitude (decimal degrees, +ve=north, -ve=south) 9 longitude (decimal degrees, +ve=east, -ve=west) 10 depth (m) sea surface temperature (OC) (measured at the seawater inlet at 7 m depth) 11 air pressure (hPa) (included for cruises au9501, au9604 and au9601) 12 13 wind speed (knots) (included for cruise au9501 only) 14 wind direction (deg. true) (included for cruise au9501 only) 15 roll (included for cruise au9501 only) 16 pitch (included for cruise au9501 only)

Note that all times are UTC.

Table 5.1: Example 10 sec digitised underway measurement file (\*.alf file).

```
Aurora Australis data - GPS pos. (deg), depth (m), sea surface temp (deg C)
decimaltime day mn yr hr m s
                                    lat
                                             lon
                                                       depth SST
70.00000004 12 3 1993 0 0 0
                                  -999.0000 -999.0000
                                                       -999.0 -999.00
 70.00011578 12 3 1993 0 0 10
                                  -999.0000 -999.0000
                                                       -999.0 -999.00
 70.00023148 12 3 1993 0 0 20
                                   -44.0044 146.3534
                                                        284.6 15.20
 70.00034722 12 3 1993 0 0 30
                                   -44.0044 146.3529
                                                        -999.0 15.20
 70.00046296 12 3 1993 0 0 40
                                   -44.0044 146.3530
                                                        283.5 15.20
 70.00057870 12 3 1993 0 0 50
                                   -44.0044 146.3523
                                                        287.4 15.20
 70.00069444 12 3 1993 0 1 0
                                   -44.0043 146.3519
                                                        282.2 15.20
 70.00081019 12 3 1993 0 1 10
                                   -44.0044 146.3515
                                                        282.4
                                                               15.20
```

#### 5.1.2 15 minute averaged underway measurement data

15 minute averaged data are contained in files named \*.exp (Table 5.2), where the data filename prefix corresponds to the cruise acronym. Note that wind direction and ship's heading are instantaneous values. All times represent the *centre* of the averaging interval. A two line header is followed by the data as follows:

#### column parameter decimal time (as for 10 sec digitised files) 1 2 latitude (as for 10 sec digitised files) 3 longitude (as for 10 sec digitised files) 4 air pressure (hPa) 5 wind speed (knots) 6 wind direction (deg. true) 7 port air temperature (OC) starboard air temperature (OC) 8 9 port relative humidity (%) 10 starboard relative humidity (%) 11 quantum radiation (μmol/s/m<sup>2</sup>) ship speed (knots) (speed through the water) 12 13 ship heading (deg. true) 14 ship roll (deg.) 15 ship pitch (deg.) sea surface salinity (parts per thousand) (from seawater inlet at 7 m depth) 16 sea surface temperature (OC) (at seawater inlet, 7 m depth) 17 average fluorescence (arbitrary units) (from seawater inlet at 7 m depth) 18 19 seawater flow (I/min) (flow rate at seawater inlet)

Note that all times are UTC.

<u>Table 5.2:</u> Example 15 min averaged underway measurement file (\*.exp file).

#### 5.2 2 DBAR AVERAGED CTD DATA FILES

The final format in which CTD data is distributed is as 2 dbar averaged data, contained in column formatted ascii files, named \*.all (Table 5.3) (the file name prefix is discussed in Appendix 2 of Rosenberg et al., 1995b). Averaging bins are centered on even pressure values, starting at 2 dbar. A 15 line header is followed by the data, as follows:

```
column
                  parameter
         pressure (dbar)
 1
 2
         temperature (OC) (ITS-90)
 3
         salinity (PSS78)
 4
         \sigma_T = density-1000 (kg.m<sup>-3</sup>)
 5
         specific volume anomaly x 108(m3.kg-1)
 6
         geopotential anomaly (J.kg<sup>-1</sup>)
 7
         dissolved oxygen (µmol.l-1)
 8
         number of data points used in the 2 dbar averaging bin
 9
         standard deviation of temperature values in the 2 dbar bin
10
         standard deviation of conductivity values in the 2 dbar bin
11
         fluorescence (mg.m<sup>-3</sup>) (uncalibrated)
         photosynthetically active radiation (µmol.s<sup>-1</sup>.m<sup>2</sup>) (uncalibrated)
12
```

All files start at the 2 dbar pressure level, incrementing by 2 dbar for each new data line. Missing data are filled by blank characters (this most often applies to dissolved oxygen data).

Table 5.3: Example 2 dbar averaged CTD data file (\*.all file).

```
SHIP : R.V. Aurora Australis
```

STATION NUMBER : 4

DATE : 02-JAN-1994 (DAY NUMBER 2)

START TIME : 1020 UTC = ZBOTTOM TIME : 1100 UTC = ZFINISH TIME : 1222 UTC = Z

CRUISE : Au94/07

START POSITION : 44:07.03S 146:13.35E
BOTTOM POSITION : 44:07.14S 146:13.71E
FINISH POSITION : 44:06.61S 146:13.95E
MAXIMUM PRESSURE: 1038 DECIBARS
BOTTOM DEPTH : 1015 METRES

```
PRESS TEMP SAL SIGMA-T S.V.A. G.A. D.O. fluorescence p.a.r. (T-90)
```

```
2.0 11.899 34.773 26.432 158.69 0.032 277.6
                                                    30 0.001 0.007 0.95569E+01 -0.49498E+00
                                                    30 0.001 0.001 0.10817E+02 -0.63459E+00
4.0 11.899 34.778 26.436 158.41 0.063 280.3
6.0 11.903 34.779 26.436 158.46 0.095 281.1
                                                    45 0.001 0.002 0.90911E+01 -0.60488E+00
                                                    41 0.000 0.000 0.80700E+01 -0.58265E+00
8.0 11.903 34.778 26.435 158.55 0.127 278.0
10.0 11.903 34.778 26.435 158.60 0.159 278.6
                                                    32 0.001 0.001 0.75122E+01 -0.66496E+00
12.0 11.904 34.778 26.435 158.66 0.190 280.2
                                                    32 0.001 0.001 0.72758E+01 -0.55944E+00
14.0 11.905 34.778 26.435 158.72 0.222 281.5
                                                    40 0.000 0.000 0.73697E+01 -0.62194E+00
16.0 11.907 34.779 26.435 158.76 0.254 277.5
                                                    34 0.002 0.002 0.69932E+01 -0.56719E+00
18.0 11.908 34.780 26.435 158.77 0.286 275.7
                                                    25 0.002 0.002 0.68356E+01 -0.63807E+00
```

#### 5.3 HYDROLOGY DATA FILES

Files named \*.bot (where the filename prefix is the the cruise code e.g. a9407) are column formatted ascii files containing the hydrology data, together with CTD upcast burst data (Table 5.4). The columns contain the following values:

#### column parameter 1 station number 2 CTD pressure (dbar) 3 CTD temperature (OC) 4 reversing thermometer temperature (OC) 5 CTD conductivity (mS.cm<sup>-1</sup>) 6 CTD salinity (PSS78) 7 bottle salinity (PSS78) 8 ortho phosphate concentration (µmol.l<sup>-1</sup>) 9 nitrate + nitrite concentration (μmol.l<sup>-1</sup>) 10 reactive silicate concentration (µmol.l<sup>-1</sup>) bottle dissolved oxygen concentration (µmol.l<sup>-1</sup>) 11 12 bottle quality flag (-1=rejected, 0=suspect, 1=good) niskin bottle number 13

Missing data values are filled by a decimal point (surrounded by blank characters). Parameters 2,3,5 and 6 are mean values from the upcast CTD burst data at the time of bottle firing, where each burst contains the data 10 sec previous to the time of bottle firing. Parameters 7 to 11 are laboratory values for the hydrology analyses. Parameter 12, the bottle quality flag, is relevant to the calibration of CTD salinities - bottles flagged 1 and 0 are used for calibration, while those flagged -1 are rejected. Criteria for flagging of the bottle data are discussed elsewhere (Appendix 2 of Rosenberg et al., 1995b). Parameter 13, the niskin bottle number, is a unique identifier for each bottle. Note that the bottle number does not always correspond with rosette position.

Table 5.4: Example hydrology data file (\*.bot file).

```
11
2
      8.556 15.155 15.154 43.109 35.032 35.031 0.29
                                                          8.80
                                                                 7.7
                                                                       247.10 1
2
     25.593 15.111
                           43.076 35.034 35.035 0.28
                                                          0.20
                                                                 3.7
                                                                       248.50 1
                                                                                   9
2
     50.992 15.105
                           43.085 35.038 35.038 0.27
                                                          0.30
                                                                 2.2
                                                                       249.10 1
                                                                                   8
2
     73.718 14.188
                           42.227 35.068 35.077 0.48
                                                          4.40
                                                                 2.8
                                                                       228.70 -1
                                                                                   7
2
                           40.910 35.055 35.051 0.66
                                                          7.70
     98.376 12.840
                                                                 2.5
                                                                       227.60 -1
                                                                                   6
2
    123.524 12.490
                           40.618 35.089 35.081 0.76
                                                          9.60
                                                                 3.0
                                                                       223.10 -1
                                                                                   5
2
                           40.025 35.052 35.067 0.85
    148.516 11.904
                                                         11.10
                                                                 3.4
                                                                       223.30 -1
                                                                                   4
2
                                                                                   3
    200.278 11.085
                           39.174 34.963 34.965 0.90
                                                        13.30
                                                                 4.0
                                                                       226.40 -1
2
    247.807 10.678 10.691 38.758 34.914 34.914 1.02
                                                        13.90
                                                                 4.1
                                                                       230.40 0
                                                                                   2
2
    289.188 9.625
                           37.640 34.769 34.794 1.13
                                                        15.80
                                                                 4.8
                                                                       232.40 -1
3
      8.609 15.984 15.958 44.199 35.274 35.275
                                                          0.20
                                                                 1.6
                                                                       270.80 1
                                                                                  16
3
     21.504 15.975
                           44.198 35.276 35.275 0.25
                                                          0.20
                                                                 1.5
                                                                       266.60 1
                                                                                  15
3
     48.210 15.935
                           44.171 35.277 35.276 0.25
                                                          0.40
                                                                 0.7
                                                                       264.60 1
                                                                                  14
3
                           44.140 35.273 35.270 0.27
     73.795 15.897
                                                          0.80
                                                                 1.6
                                                                       238.30 -1
                                                                                  13
3
     98.905 14.011
                           42.238 35.229 35.236 0.63
                                                          7.50
                                                                 2.3
                                                                              -1
                                                                                  12
3
                           40.763 35.155 35.155 0.81
                                                                       216.00 0 11
    148.674 12.557
                                                         10.90
                                                                 4.1
3
    197.813 11.432
                           39.575 35.033 35.033 0.92
                                                        12.80
                                                                 3.9
                                                                       227.30 1
                                                                                  10
3
    298.658 10.110
                           38.158 34.828 34.831 1.10
                                                        15.40
                                                                       230.70 1
                                                                                   9
                                                                 4.6
3
    396.295 9.214
                           37.238 34.702 34.703 1.28
                                                        18.70
                                                                 6.0
                                                                       226.20 -1
                                                                                   8
3
                           36.405 34.604 34.603 1.52
                                                                                   7
    496.675 8.371
                                                        22.50
                                                                 9.3
                                                                       210.60 1
3
    597.207 7.385
                           35.469 34.524 34.524 1.71
                                                        25.90
                                                                14.6
                                                                       199.30 1
                                                                                   6
3
    697.115 6.587
                           34.751 34.487 34.486 1.90
                                                        28.30
                                                                20.6
                                                                       195.30 1
                                                                                   5
3
                           33.995 34.458 34.458 2.05
                                                                                   4
    778.707
             5.739
                                                        30.50
                                                                27.8
                                                                                   3
3
    900.509
             4.315
                           32.710 34.381 34.382 2.20
                                                        32.70
                                                                33.6
                                                                       198.50 1
3
             4.027
                     4.029 32.574 34.471 34.471 2.34
                                                        34.30
                                                                49.6
                                                                       171.00 1 302
   1000.091
                           32.110 34.517 34.522 2.42
   1113.395
             3.403
                                                        35.40
                                                                61.3
                                                                       169.90 -1
```

4	23.926	15.341	43.397	35.121	35.120	0.26	0.10	0.6	230.60 1 23
4	49.736	15.198	43.231	35.088	35.087	0.26	0.30	0.6	229.10 1 22
4	99.651	13.388	41.599	35.202	35.200	0.77	9.00	2.6	200.60 1 21
4	148.952	12.164	40.341	35.114	35.122	0.86	12.90	3.8	221.80 -1 20
4	196.847	11.114	39.222	34.985	34.980	0.95	11.40	3.6	233.30 -1 119
4	298.033	9.997	38.028	34.804	34.803	1.02	13.80		254.10 -1 118
4	384.198	9.235	37.228	34.676	34.677				256.20 -1 17
4	495.853	8.452	36.455	34.578	34.577	1.43	20.70	8.1	232.70 -1 16

## 5.4 STATION INFORMATION FILES

Station information files, named \*.sta (Table 5.5) (where the filename prefix is the cruise code), contain position, time, bottom depth and maximum pressure of cast for CTD stations. The CTD instrument number is specified in the file header. Position and time (UTC) are specified at the start, bottom and end of the cast, while the bottom depth is for the start of the cast. Note that small inconsistencies may exist between bottom depth and maximum pressure, due to drift of the vessel between the start and bottom of the cast. In addition, a single value is used for the sound velocity in seawater for echo sounder calculations (1498 m.s<sup>-1</sup>), which may cause small errors in water depth values.

<u>Table 5.5:</u> Example CTD station information file (\*.sta file).

RSV Aurora Australis		Cruise : Au93/09		CTD station list			(CTD unit 4)					
stat   no.	   time	date	sta latitude	art longitude	bottom depth(m)	max P  (dbar)	   time	bottom latitude	longitude	   time	end latitude	  longitude
	2032	11-MAR-93	44:06.73S	146:14.35E	1000	956	  2118	44:06.37S	146:14.35E	2154	44:06.198	146:14.60E
2	0027	12-MAR-93	44:00.06S	146:18.61E	300	   289	   0042	44:00.03S	146:18.77E	0115	43:59.97S	146:18.64E
3	0513	12-MAR-93	44:07.51S	146:14.89E	1100	   1115	   0549	44:07.48S	146:15.06E	0632	44:07.39S	146:15.23E
4	0854	12-MAR-93	44:27.89S	146:07.94E	2340	   2335	   0938	44:27.52S	146:07.30E	1028	44:27.32S	146:07.51E
5	1437	12-MAR-93	44:56.71S	145:56.67E	3380	   3465	  1606	44:56.10S	145:56.52E	1727	44:55.56S	145:56.36E
Ί	l					I	1		I			I

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#### 5.5 WOCE DATA FORMAT

This section is relevant only to data submitted to the WHP Office. For WOCE format data, file format descriptions as detailed above should be ignored. Data files submitted to the WHP Office are in the standard WOCE format as specified in Joyce and Corry (1994).

#### 5.5.1 CTD 2 dbar-averaged data files

- \* CTD 2 dbar-averaged file format is as per Table 4.7 of Joyce and Corry (1994), except that measurements are centered on even pressure bins (with first value at 2 dbar).
- \* CTD temperature and salinity are reported to the third decimal place only.
- \* Files are named as in the CTD methodology, except that for WOCE format data the suffix ".all" is replaced with ".ctd".
- \* The quality flags for CTD data are defined in Table 5.6. Data quality information is detailed in earlier sections of this report.

#### 5.5.2 Hydrology data files

- Hydrology data file format is as per Table 4.5 of Joyce and Corry (1994), with quality flags defined in Tables 5.7 and 5.8.
- \* Files are named as in the CTD methodology, except that for WOCE format data the suffix ".bot" is replaced by ".sea".
- \* The total value of nitrate+nitrite only is listed.
- \* Silicate and nitrate+nitrite are reported to the first decimal place only.
- \* CTD temperature (including theta), CTD salinity and bottle salinity are all reported to the third decimal place only.
- \* CTD temperature (including theta), CTD pressure and CTD salinity are all derived from upcast CTD burst data; CTD dissolved oxygen is derived from downcast 2 dbar-averaged data.
- Raw CTD pressure values are not reported.
- \* SAMPNO is equal to the rosette position of the Niskin bottle.
- \* Salinity samples rejected for conductivity calibration, as per eqn A2.20 in Rosenberg et al. (1995b), are not flagged in the .sea file.
- \* Dissolved oxygen samples rejected for CTD dissolved oxygen calibration, as per Tables 1.18, 2.19 and 3.18 in Parts 1, 2 and 3 respectively of this report, are not flagged in the .sea file.

#### 5.5.3 Conversion of units for dissolved oxygen and nutrients

#### 5.5.3.1 Dissolved oxygen

Niskin bottle data

For the WOCE format files, all Niskin bottle dissolved oxygen concentration values have been converted from volumetric units  $\mu$ mol/I to gravimetric units  $\mu$ mol/kg, as follows. Concentration  $C_k$  in  $\mu$ mol/kg is given by

$$C_k = 1000 C_1 / \rho(\theta, s, 0)$$
 (eqn 5.1)

where  $C_1$  is the concentration in  $\mu$ mol/I, 1000 is a conversion factor, and  $\rho(\theta,s,0)$  is the potential density at zero pressure and at the potential temperature  $\theta$ , where potential temperature is given by

$$\theta = \theta(\mathsf{T},\mathsf{s},\mathsf{p}) \tag{eqn 5.2}$$

for the *in situ* temperature T, salinity s and pressure p values at which the Niskin bottle was fired. Note that T, s and p are upcast CTD burst data averages.

In the WOCE format files, CTD dissolved oxygen data are converted to  $\mu$ mol/kg by the same method as above, except that T, s and p in eqns 5.1 and 5.2 are CTD 2 dbar-averaged data.

#### 5.5.3.2 Nutrients

For the WOCE format files, all Niskin bottle nutrient concentration values have been converted from volumetric units µmol/l to gravimetric units µmol/kg using

$$C_k = 1000 C_1 / \rho(T_1, s, 0)$$
 (eqn 5.3)

where 1000 is a conversion factor, and  $\rho(T_i,s,0)$  is the water density in the hydrology laboratory at the laboratory temperature  $T_i$  and at zero pressure. Note that the following values were used for  $T_i$ :

```
cruise au9501, T_i=18.0°C cruise au9604, T_i=19.6°C cruise au9601, T_i=20.0°C
```

Upcast CTD burst data averages are used for s.

<u>Table 5.6:</u> Definition of quality flags for CTD data (after Table 4.10 in Joyce and Corry, 1994). These flags apply both to CTD data in the 2 dbar-averaged \*.ctd files, and to upcast CTD burst data in the \*.sea files.

flag	definition
1	not calibrated with water samples
2	acceptable measurement
3	questionable measurement
4	bad measurement
5	measurement not reported
6	interpolated over >2 dbar interval
7	despiked
8	this flag not used
9	parameter not sampled

<u>Table 5.7:</u> Definition of quality flags for Niskin bottles (i.e. parameter BTLNBR in \*.sea files) (after Table 4.8 in Joyce and Corry, 1994).

flag	definition
1	this flag is not used
2	no problems noted
3	bottle leaking
4	bottle did not trip correctly
5	not reported
6,7,8	these flags are not used
9	samples not drawn from this bottle

<u>Table 5.8:</u> Definition of quality flags for water samples in \*.sea files (after Table 4.9 in Joyce and Corry, 1994).

flag	definition
1	this flag is not used
2	acceptable measurement
3	questionable measurement
4	bad measurement
5	measurement not reported
6	mean of replicate measurements
7	manual autoanalyser peak measurement
8	this flag not used
9	parameter not sampled

#### 5.5.4 Station information files

- \* File format is as per section 3.3 of Joyce and Corry (1994), and files are named as in the CTD methodology, except that for WOCE format data the suffix ".sta" is replaced by ".sum".
- \* All depths are calculated using a uniform speed of sound through the water column of 1498 ms<sup>-1</sup>. Reported depths are as measured from the water surface. Missing depths are due to interference of the ship's bow thrusters with the echo sounder signal.
- $^{\star}$  An altimeter attached to the base of the rosette frame (approximately at the same vertical position as the CTD sensors) measures the elevation (or height above the bottom) in metres. The elevation value at each station is recorded manually from the CTD data stream display at the bottom of each CTD downcast. Motion of the ship due to waves can cause an error in these manually recorded values of up to  $\pm 3$  m.
- \* Lineout (i.e. meter wheel readings of the CTD winch) were unavailable.

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